

**TRAVERSE MOUNTAIN AREA PLAN
STORM DRAIN**



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LEHI CITY

TRAVERSE MOUNTAIN AREA PLAN

STORM DRAIN

12 June 2012

The Traverse Mountain development is comprised of two main drainage areas. These areas, as shown in Figure One, consist of the Fox Hollow Drainage and the SR-92 Drainage. The Fox Hollow Drainage flows westerly to an existing 60" culvert under I-15. The culvert has been extended and an energy dissipater constructed in the Jordan Narrows Regional Drainage Facility. The SR-92 Drainage flows westerly and southerly to a recently constructed 72" outfall storm drain for the Timpanogos Highway. The outfall terminal is the Jordan Narrows Facility.

Outfall Drainage

The drainage from the SR-92 basin discharges into the 72" storm drain. Traverse Mountain's by agreement between UDOT and Lehi City has the ability to connect to this storm drain and discharge at specified flow rates. Traverse Mountain participated in the project to construct the Jordan Narrows Regional Detention Facility at the end of the 72" SR-92 outfall line. By the agreement, Traverse Mountain has 8.1 acre feet of capacity in the 17.1 acre feet constructed in the first phase. This allows them to transfer the existing Pond "A" facility offsite. Traverse Mountain also has the right to construct a second pond consisting of an additional 20 acre feet at the same location. Traverse Mountain will have to disconnect the existing pond "A" detention and connect it to the 72" storm drain at the Adobe Way location. The existing 36" storm drain in Adobe Way will need to be connected to the existing Bull River Ditch crossing of I-15 which connects to the 36" storm drain in the west frontage road.

Drainage Analysis

The concept plan was modeled in WMS software using a hec-1 model to estimate drainage flow for the development. The rainfall data used is provided in the appendix. A rainfall depth of 2.52 inches for the 100 year event, 2.30 inches for the 50 year event and 1.79 inches for the 10 year event were used in the modeling.

The estimated peak flows for the development can be found on Figure 1. The analysis calculated the allowable discharge rates for the project. The discharge rates were determined to be 0.4 cfs/acre for residential and commercial for the SR-92 drainage area and the allowable discharge will be based upon a c-factor of 0.53 for a 50 year event for the Fox Hollow drainage basin, as seen in Figure 2. Onsite detention will be required for projects exceeding this discharge rate for a 100 year design event. The developer will be responsible for meeting the city's requirement for detention of 0.2 cfs/acre based upon the 100 year event. The detention will be provided in both onsite facilities and offsite facilities (Lambert and Jordan Narrows Ponds). The developer will construct the onsite detention determined from the difference on the allowable discharge rate and the city's 0.2 cfs/acre discharge. The developer will also construct the offsite detention as it is needed for the project.

SD - 1



The following is an example for East Canyon A1-A4:

Required detention based upon 0.2 cfs/acre: 76,248 cubic feet.
 Required detention based upon 0.4 cfs/acre: 58,176 cubic feet.
 Require offsite detention (Difference between 0.2 and 0.4): 18,072 cubic feet
 Offsite detention has been provided with the balance required onsite to hold to these flow rates.

An analysis of the proposed developable area was performed using the rational method to estimate the required detention volumes. Results are shown in the attached detention tables. The following c-factors were used:

<u>Land Use</u>	<u>C-Factor Range</u>	<u>C-Factor Used</u>	<u>Soil Group C</u>		<u>Soil Group D</u>	
			<u>CN Range</u>	<u>CN Used</u>	<u>CN Range</u>	<u>CN Used</u>
Native Open Space	.10	.10	55-59	57	61-65	63
Parks/Cut slopes/Landscaping	.20	.20	72-76	74	78-82	80
Low Density (1-4)	.34-.47	.41	79-83	81.0	84-87	85.5
Medium Density (4.1-6)	.47-.59	.53	83-88	85.5	87-90	88.5
High Density (6.1-20)	.59-.70	.64	88-91	89.5	90-93	91.5
Churches/Schools (70% imp.)	.69	.69	84-88	86	91-95	93
Commercial (85% imp.)	.80	.80	93-95	94	95	95
Roads/Impervious	.90	.90		95		95

The development will require approximately 75.49 acre-feet of detention. The following is an estimate of where it will be distributed.

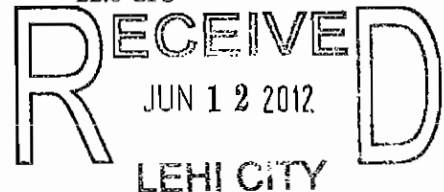
	<u>Total Req.</u>	<u>Constructed</u>	<u>Proposed</u>
Jordan Narrows	26.50 AF	8.10 AF	18.40 AF
Lambert	10.00 AF		10.00 AF
On Site Storage	35.22 AF	5.28 AF	29.94 AF
TOTAL	75.49 acre-feet		

Storm Drains

The SR-92 basin will have storm drains designed for the 10 year event as per Lehi City Standards. Pipes will meet the requirement of Section 9.07 of the Lehi Design Standards. The maximum 10 year event will not exceed the agreed discharge into the 72" storm drain. Detention will be required to control the flows from developments draining to the 72" storm drain. This will be done by the discharge rates as shown on Figure 1 and as follows:

Adobe (9C):	109 CFS	Murdock Canal (11C):	62.8 CFS
Rail Road (10C):	72.7 CFS	Perry (13C):	22.6 CFS
Existing Bull River Bore	50.0 CFS		

SD - 2



The master plan storm drains are shown in Figure 3. These storm drains must be installed with developments or as soon as the existing downstream capacity is exceeded. The schedule of when the storm drain lines need to be installed is shown on Figure 3. The plan requires several major pipes to be installed. The removal of pond "A" will require the installation of several storm drain lines as shown on Figure 3. A 36" line will need to be installed south of the Murdock Corridor and a 42" line (parallel in sections) will need to be installed under the canal along Cabella's Blvd. to the Adobe corridor.

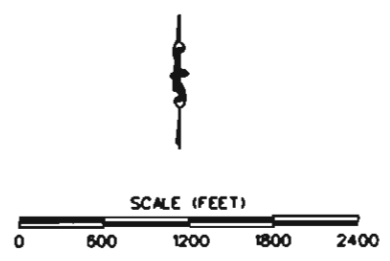
Central Canyon will have the main storm drain pipe designed for the 50 year event. The existing storm drain has a capacity of approximately 200 CFS. The outfall from the Lambert basin will be limited to 325 CFS maximum flow with discharge into the Jordan Narrows facility. A parallel storm drain construction of 48" and 60" pipe will be constructed along Traverse Mtn. Blvd. to the Lambert Detention Facility. A connection from Chapple Ridge to Fox Canyon will also be required to separate the Chapple Ridge system into parts.

Mass Grading

Mass grading operations will be detained to 0.1 CFS per acre of disturbed ground or higher as determined by the City Engineer during all construction phases to control erosion and sedimentation of downstream facilities. A complete Storm Water Pollution Prevention Plan (SWPPP) will also be developed to include Best Management Practices (BMPs), for erosion and revegetation of slopes and pads.

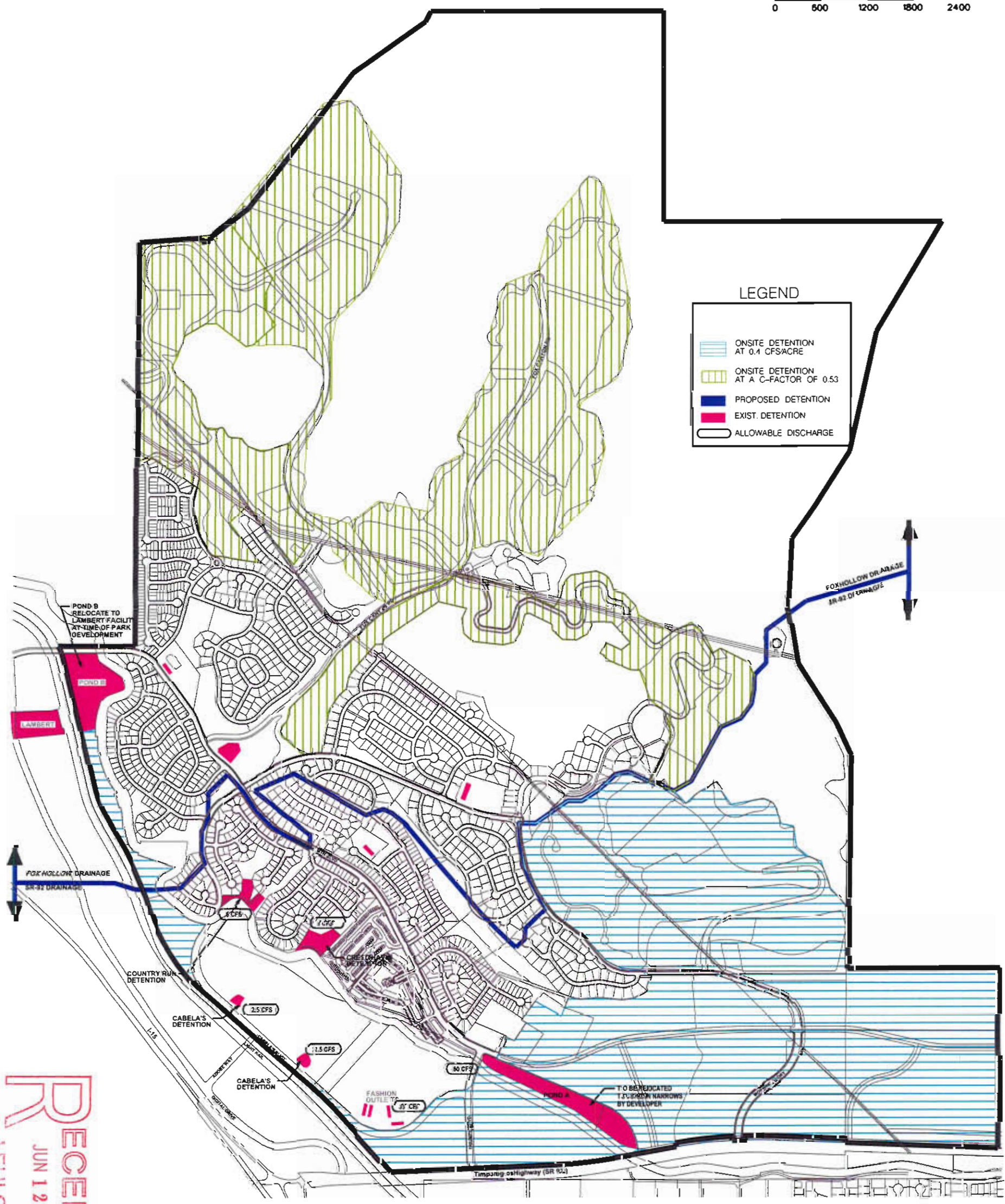
SD - 3





LEGEND

- ONSITE DETENTION AT 0.1 CFS/ACRE
- ONSITE DETENTION AT A C-FACTOR OF 0.53
- PROPOSED DETENTION
- EXIST. DETENTION
- ALLOWABLE DISCHARGE



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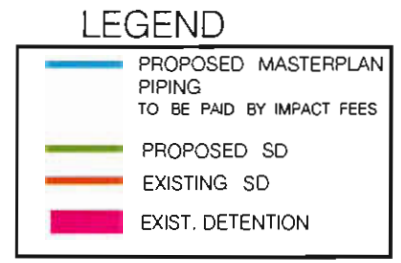
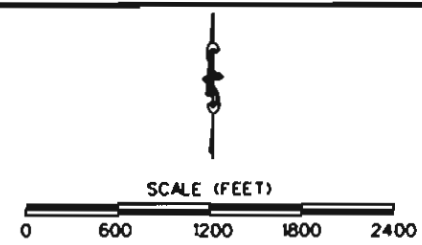
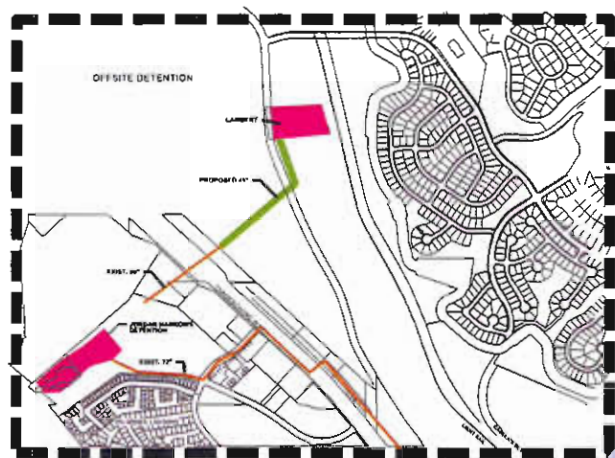
JUN 12 2012

MW BROWN

ENGINEERING, INC

Office: (801) 377-1790 Fax: (801) 377-1789
578 East 770 North, Orem UT 84097

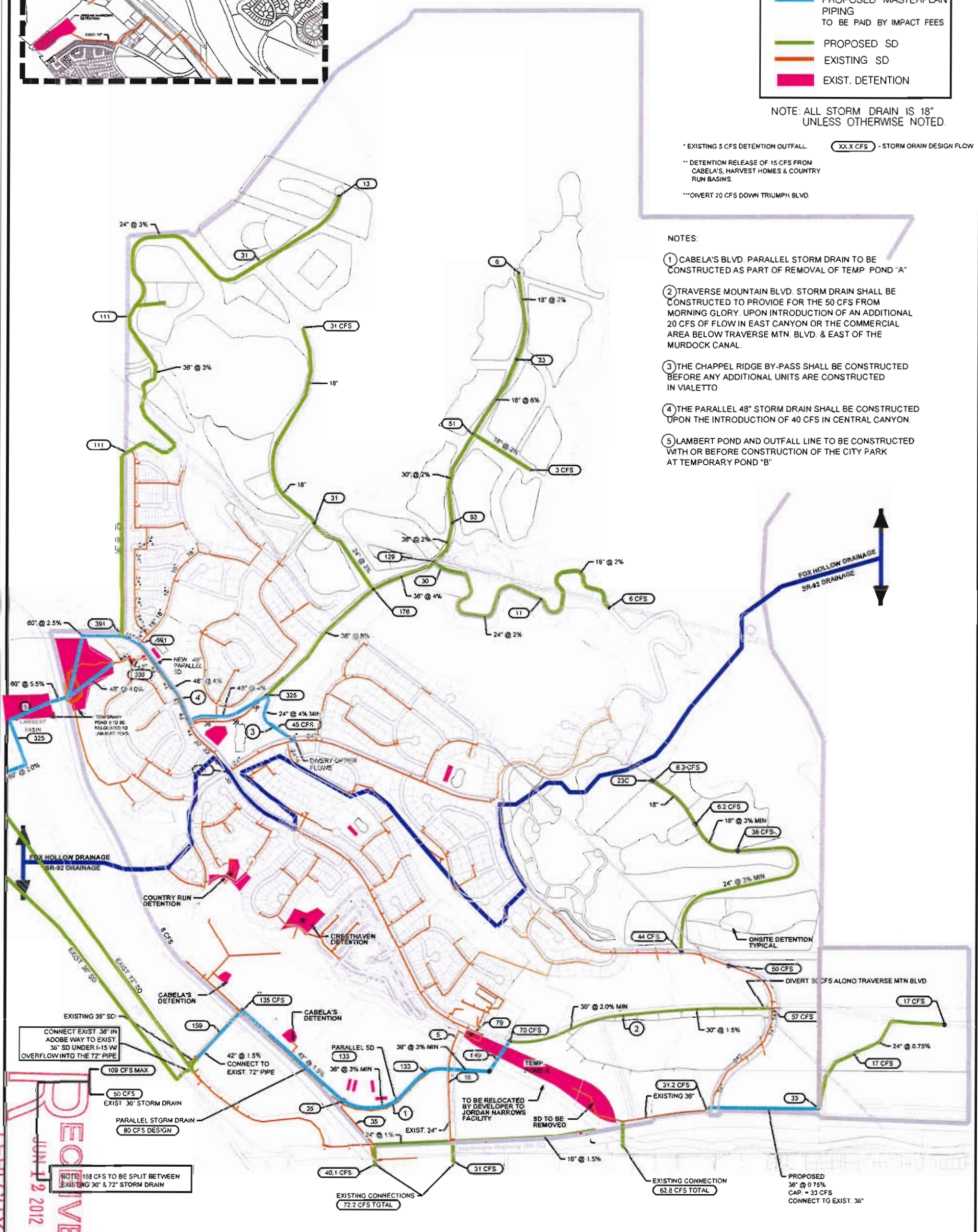
Title:		PROJECT NO. 2010.037.005
Client:	TRAVERSE MOUNTAIN, LEHI UTAH	
Drawing Name:	ALLOWABLE RELEASE RATE	FIGURE 2
		DATE: 6-12-12



NOTE: ALL STORM DRAIN IS 18" UNLESS OTHERWISE NOTED.

* EXISTING 5 CFS DETENTION OUTFALL. (XX) CFS - STORM DRAIN DESIGN FLOW
 ** DETENTION RELEASE OF 15 CFS FROM CABELA'S, HARVEST HOMES & COUNTRY RUN BASINS.
 *** OVERT 20 CFS DOWN TRIUMPH BLVD.

- NOTES:
- 1 CABELA'S BLVD. PARALLEL STORM DRAIN TO BE CONSTRUCTED AS PART OF REMOVAL OF TEMP POND "A"
 - 2 TRAVERSE MOUNTAIN BLVD. STORM DRAIN SHALL BE CONSTRUCTED TO PROVIDE FOR THE 50 CFS FROM MORNING GLORY. UPON INTRODUCTION OF AN ADDITIONAL 20 CFS OF FLOW IN EAST CANYON OR THE COMMERCIAL AREA BELOW TRAVERSE MTN. BLVD. & EAST OF THE MURDOCK CANAL.
 - 3 THE CHAPPEL RIDGE BY-PASS SHALL BE CONSTRUCTED BEFORE ANY ADDITIONAL UNITS ARE CONSTRUCTED IN VIALETTO
 - 4 THE PARALLEL 48" STORM DRAIN SHALL BE CONSTRUCTED UPON THE INTRODUCTION OF 40 CFS IN CENTRAL CANYON.
 - 5 LAMBERT POND AND OUTFALL LINE TO BE CONSTRUCTED WITH OR BEFORE CONSTRUCTION OF THE CITY PARK AT TEMPORARY POND "B"



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Title:		PROJECT NO. 2010.037.005
Client:	TRAVERSE MOUNTAIN, LEHI UTAH	FIGURE 3 DATE: 6-12-12
Drawing Name:	STORM DRAIN PIPE SIZES	

DETENTION
SUMMARY

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Proposed Plats Required Detention

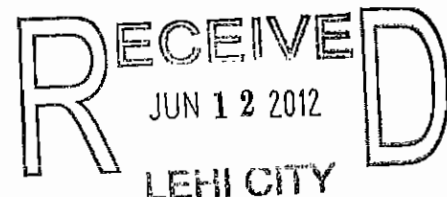
Traverse Mountain Overall System

May 25, 2012

West Canyon	Acres	Required Detention		Onsite Detention		Lambert	Jordan Landing
		CF	Acre-Ft	CF	Acre-Ft	Acre-Ft	Acre-Ft
A1-A3	16.0	44,280	1.02	8,784	0.20	0.00	0.81
B1-B2	5.1	12,888	0.30	0	0.00	0.00	0.30
C1-C2	15.8	42,768	0.98	8,712	0.20	0.00	0.78
D1	5.7	18,216	0.42	3,816	0.09	0.00	0.33
E1-E2	14.0	37,044	0.85	7,704	0.18	0.00	0.67
F1-F3	15.5	27,720	0.64	0	0.00	0.00	0.64
Total	72.1	182,916	4.20	29,016	0.67	0.00	3.53

Central Canyon	Acres	Required Detention		Onsite Detention		Lambert	Jordan Landing
		CF	Acre-Ft	CF	Acre-Ft	Acre-Ft	Acre-Ft
A1-A2	10.3	22,824	0.52	0	0.00	0.00	0.52
B	7.0	17,676	0.41	0	0.00	0.00	0.41
C	5.7	14,400	0.33	0	0.00	0.00	0.33
D1-D2	10.4	23,076	0.53	0	0.00	0.00	0.53
E1-E2	15.0	34,200	0.79	0	0.00	0.00	0.79
F1-F3	15.2	28,116	0.65	0	0.00	0.00	0.65
G1-G2	10.4	23,076	0.53	0	0.00	0.00	0.53
H1-H2	9.9	23,184	0.53	0	0.00	0.00	0.53
I1-I2	8.4	19,152	0.44	0	0.00	0.00	0.44
J1-J2	14.4	41,616	0.96	7,920	0.18	0.00	0.77
K1-K2	9.9	26,208	0.60	5,472	0.13	0.00	0.48
L2	14.5	41,040	0.94	8,892	0.20	0.00	0.74
M	4.0	12,780	0.29	2,700	0.06	0.00	0.23
N (Public Park)	1.2	756	0.02	0	0.00	0.00	0.02
Total	136.3	328,104	7.53	24,984	0.57	0.00	6.96

East Canyon	Acres	Required Detention		Onsite Detention		Lambert	Jordan Landing
		CF	Acre-Ft	CF	Acre-Ft	Acre-Ft	Acre-Ft
A1-A4	25.3	76,248	1.75	58,176	1.34	0.00	0.41
B1	9.0	28,764	0.66	22,284	0.51	0.00	0.15
C1-C2	19.3	38,088	0.87	28,134	0.65	0.00	0.23
D1-D6	59.4	109,908	2.52	80,730	1.85	0.00	0.67
Total	113.0	253,008	5.81	189,324	4.35	0.00	1.46



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Proposed Plats Required Detention

Traverse Mountain Overall System

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Perry Properties	Acres	Required Detention		Onsite Detention		Lambert	Jordan Landing
		CF	Acre-Ft	CF	Acre-Ft	Acre-Ft	Acre-Ft
A1-A2	34.9	83,808	1.92	62,982	1.45	0.00	0.48
B1-B2	28.4	66,456	1.53	49,842	1.14	0.00	0.38
C	69.7	222,804	5.11	172,620	3.96	0.00	1.15
D	25.6	81,828	1.88	63,396	1.46	0.00	0.42
Private Park	10.4	6,552	0.15	3,915	0.09	0.00	0.06
Total	169.0	461,448	10.59	352,755	8.10	0.00	2.50

River Bend	Acres	Required Detention		Onsite Detention		Lambert	Jordan Landing
		CF	Acre-Ft	CF	Acre-Ft	Acre-Ft	Acre-Ft
A	9.8	24,732	0.57	0	0.00	0.57	0.00
B	14.5	46,368	1.06	9,792	0.22	0.00	0.84
C	23.8	76,068	1.75	16,020	0.37	0.00	1.38
D	5.7	18,216	0.42	3,816	0.09	0.33	0.00
E	18.9	47,700	1.10	0	0.00	0.00	1.10
F	16.0	40,392	0.93	0	0.00	0.93	0.00
Total	88.7	253,476	5.82	29,628	0.68	1.83	3.31

Non-Canyon	Acres	Required Detention		Onsite Detention		Lambert	Jordan Landing
		CF	Acre-Ft	CF	Acre-Ft	Acre-Ft	Acre-Ft
Church	3.4	14,184	0.33	5,616	0.13	0.00	0.20
A	8.1	25,884	0.59	5,436	0.12	0.00	0.47
	6.5	20,772	0.48	4,356	0.10	0.00	0.38
	3.3	8,316	0.19	0	0.00	0.00	0.19
D	0.6	1,512	0.03	0	0.00	0.00	0.03
Total	21.9	70,668	1.62	15,408	0.35	0.00	1.27

Commercial	Acres	Required Detention		Onsite Detention		Lambert	Jordan Landing
		CF	Acre-Ft	CF	Acre-Ft	Acre-Ft	Acre-Ft
Public Park	9.6	6,048	0.14	3,609	0.08	0.00	0.06
Highway Comm.	9.4	39,240	0.90	32,472	0.75	0.00	0.16
Highway Comm.	7.3	30,492	0.70	25,236	0.58	0.00	0.12
Highway Comm.	6.7	27,972	0.64	23,140	0.53	0.00	0.11
Highway Comm.	7.8	32,580	0.75	26,964	0.62	0.00	0.13
Highway Comm.	14.8	61,812	1.42	51,156	1.17	0.00	0.24
Highway Comm.	2.5	10,440	0.24	8,640	0.20	0.00	0.04
Highway Comm.	114.6	478,584	10.99	396,072	9.09	0.00	1.89
Highway Comm.	27.3	114,012	2.62	94,356	2.17	0.00	0.45
HC	1.8	7,524	0.17	6,228	0.14	0.00	0.03
HC	3.1	12,960	0.30	10,728	0.25	0.00	0.05
Total	204.9	821,664	18.86	678,601	15.58	0.00	3.28

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DETECTION BASIN TOTALS

Traverse Mountain Overall System

May 25, 2012

EXISTING DEVELOPMENT	DETECTION		REQUIRED				CR	POND	HH	POND	Onsite	Lambert	JORDAN	NARROWS				
	Location	VOLUME (cubic feet)	POND A	POND B	HH	POND												
Recorded Plats																		
TM BLVD. NORTH	ROAD PLAT	6,100		6,100														
TM BLVD. SOUTH	ROAD PLAT	22,500		22,500														
MORNING GLORY ROAD	ROAD PLAT	25,285		25,285														
CHAPEL RIDGE	PHASES 1&2	20,285		20,285														
	PHASE 3	19,440		19,440														
COUNTRY RUN	CR BASIN	35,667																
HARVEST HOMES	PLAT ONE	33,000																
	PLAT TWO	0																
	PLAT THREE	0																
HEATHER MOORE	PLAT ONE	31,000		31,000														
HUNTER CHASE	PLAT ONE	15,000		15,000														
	PLAT TWO	14,000		14,000														
	PLAT THREE	2,000		2,000														
EAGLE SUMMIT	PHASES 1&2	74,558		74,558														
	PLAT THREE	870		870														
	PLAT FOUR	870		870														
	PLAT FIVE	870		870														
Eagle Summit Plat 6	Site Plan	0		0														
SHADOW RIDGE	PLAT ONE	28,920		28,920														
	PLAT TWO	26,950		26,950														
WINTERHAVEN	PHASES 1&2	42,274		42,274														
WOODHAVEN	PHASES 1-3	68,310		68,310														
VISTA RIDGE	PHASES 1&2	43,856		43,856														
	PHASE 3 & 4	22,908		22,908														
Traverse Mount Plat D & Challenger School	Plat D	11,909		11,909														
Violetto Recorded Plat	Pond B	39,350		39,350														
Cresthaven Townhomes	All	23,666		23,666														
Cresthaven Apartments	All	31,741		31,741														
FASHION OUTLET	JORDAN NARROWS/ HH	114,138		114,138														
TRAVERSE MOUNTAIN SALES CENTER	JORDAN NARROWS	3,973		3,973														
CABELAS-ON SITE		131,237		131,237														
CHURCH (TRaverse MOUNTAIN BLVD)		9,230		9,230														
CHURCH (CABEL RIDGE)		13,464		13,464														
CHURCH (FOX HILL DR.)		9,967		9,967														
TRANSFER FROM POND A TO JORDAN NARROWS AGREEMENT		0		-168,840														
Total Volumes Required for Existing Development (Cubic Feet)											923,318	0	352,368	69,296	35,667	229,857	0	236,130
Total Volumes Required for Existing Development (Acre Feet)											21.20	0.00	8.09	1.59	0.82	5.28	0.00	5.42

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DETENTION BASIN TOTALS

Traverse Mountain Overall System

May 25, 2012

EXISTING DETENTION BASINS	CONSTRUCTED	DETENTION					On Site	Lambert	JORDAN NARROWS
		VOLUME (cubic feet)	POND A	POND B	HH POND	CR POND			
Constructed Ponds									
TRAVERSE MOUNTAIN POND A	TRAV. PLAT 1	352,836	352,836						
TRAVERSE MOUNTAIN POND B*	CHAPEL BEND	196,020	196,020						
TRAVERSE MOUNTAIN POND B*	SHADOW RIDGE	60,984	60,984						
HARVEST HOMES	HARVEST HOME	33,000			33,000				
COUNTRY RUN	COUNTRY RUN	87,120				87,120			
CRESTHAVEN (constructed)	CRESTHAVEN	44,000			44,000				
JORDAN NARROWS (REPLACES POND A)	AGREEMENT	8,712	-352,836					361,548	
FASHION OUTLET		65,959						65,959	
CABELLAS ON SITE		131,237						131,237	
CHURCH (TRAVERSE MOUNTAIN BLVD)		9,230						9,230	
CHURCH (CHAPEL RIDGE)		13,464						13,464	
CHURCH (FOXTAIL DR.)		9,967						9,967	
Total Storage Provided (cubic feet)		1,012,529	0	257,004	77,000	87,120	0	361,548	
Total Storage Provided (Acre Feet)		23.24	0.00	5.90	1.77	2.00	0.00	8.30	
Percentage of storage used		91%	0%	137%	90%	41%	0%	65%	
Percentage Available		9%	0%	-37%	10%	58%	0%	33%	

*Note: Expansion of Pond B to be in the Lambert Parcel with Vialeto and Fox Canyon Subdivisions. Upon final build out of project, no pond will exceed 100% of capacity.



DETECTION BASIN TOTALS

Traverse Mountain Overall System

May 25, 2012

PROPOSED DEVELOPMENT

Proposed Plats	AREA PLAN	DETECTION					
		VOLUME (cubic feet)	POND A	POND B	HH POND	CR POND	On Site Lambert JORDAN NARROWS
TRANSFER FROM POND B TO LAMBERT		0		-352,368			352,368
West Canyon		182,916				29,016	0
Central Canyon		328,104				24,984	0
East Canyon		253,008				189,324	0
Perry Properties		451,448				352,755	0
Riverbend Properties		253,476				29,628	79,524
Commercial		821,664				678,601	0

Total Volumes Required for Proposed Development (Cubic Feet) 2,300,616 0 -352,368 0 0 1,304,308 431,892 916,784

Total Volumes Required for Proposed Development (Acre Feet) 52.81 0.00 -8.09 0.00 0.00 29.94 9.91 21.05

PROPOSED DETENTION BASINS

DETECTION

Proposed Pond Expansions	DETECTION					
	VOLUME (cubic feet)	POND A	POND B	HH POND	CR POND	On Site Lambert JORDAN NARROWS
Jordan Narrows Expansion	792,792					792,792
Lambert Pond	178,596		-257,004			435,600
West Canyon	29,016					29,016
Central Canyon	24,984					24,984
East Canyon	189,324					189,324
Perry Properties	352,755					352,755
Riverbend Properties	29,628					29,628
Commercial	678,601					678,601

Total Volumes Required for Proposed Development (Cubic Feet) 2,275,696 0 -257,004 0 0 1,304,308 435,600 792,792

Total Volumes Required for Proposed Development (Acre Feet) 52.24 0.00 -5.90 0.00 0.00 29.94 10.00 18.20

Percentage of storage used 101%

Percentage Available -1%



DETENTION BASIN TOTALS

Traverse Mountain Overall System
May 25, 2012

PROJECT TOTALS

DETENTION

Required Storage

	VOLUME	POND		HH		CR		On Site	Lambert	JORDAN	NARROWS
		A	B	POND	POND	POND	POND				
Storage Required For Existing Development	Cubic Feet 929,318	0	352,368	69,296	35,667	229,857	0	236,130	0	0	5.42
	Acre Feet 21.20	0.00	8.09	1.59	0.82	5.28	0.00	5.42	0.00	0.00	0.00
Storage Required For Proposed Development	Cubic Feet 2,300,616	0	-352,368	0	0	1,304,308	431,892	916,784	29.94	9.91	21.05
	Acre Feet 52.81	0.00	-8.09	0.00	0.00	29.94	9.91	21.05	0.00	0.00	0.00
Total Required Storage For Project (Cubic Feet)	3,223,934	0	0	69,296	35,667	1,534,165	431,892	1,152,914	35.22	9.91	26.47
Total Required Storage For Project (Acre Feet)	74.01	0.00	0.00	1.59	0.82	35.22	9.91	26.47	0.00	0.00	0.00

DETENTION

Provided Storage

	VOLUME (cubic feet)	POND		HH		CR		On Site	Lambert	JORDAN	NARROWS
		A	B	POND	POND	POND	POND				
Constructed Pond Total	Cubic Feet 1,012,529	0	257,004	77,000	87,120	229,857	0	361,546	0	0	8
	Acre Feet 23	0	6	2	2	5	0	8	0	0	0
Proposed Pond Expansion Total	Cubic Feet 2,275,696	0	-257,004	0	0	1,304,308	431,892	791,792	29.94	9.91	18.22
	Acre Feet 52.24	0.00	-5.90	0.00	0.00	29.94	10.00	18.22	0.00	0.00	0.00

Total Required Storage For Project (Cubic Feet)	3,223,934	0	0	77,000	87,120	1,534,165	431,892	1,154,340	35.22	10.00	26.50
Total Required Storage For Project (Acre Feet)	75.49	0.00	0.00	1.77	2.00	35.22	10.00	26.50	0.00	0.00	0.00
Percentage of storage used	98%	0%	0%	90%	41%	100%	99%	100%	0%	0%	0%
Percentage Available	2%	0%	0%	10%	59%	0%	1%	0%	0%	0%	0%

Note: Expansion of Pond B to be in the Lambert Parcel with Vialetto and Fox Canyon Subdivisions. Upon final build out of project, no pond will exceed 100% of capacity.

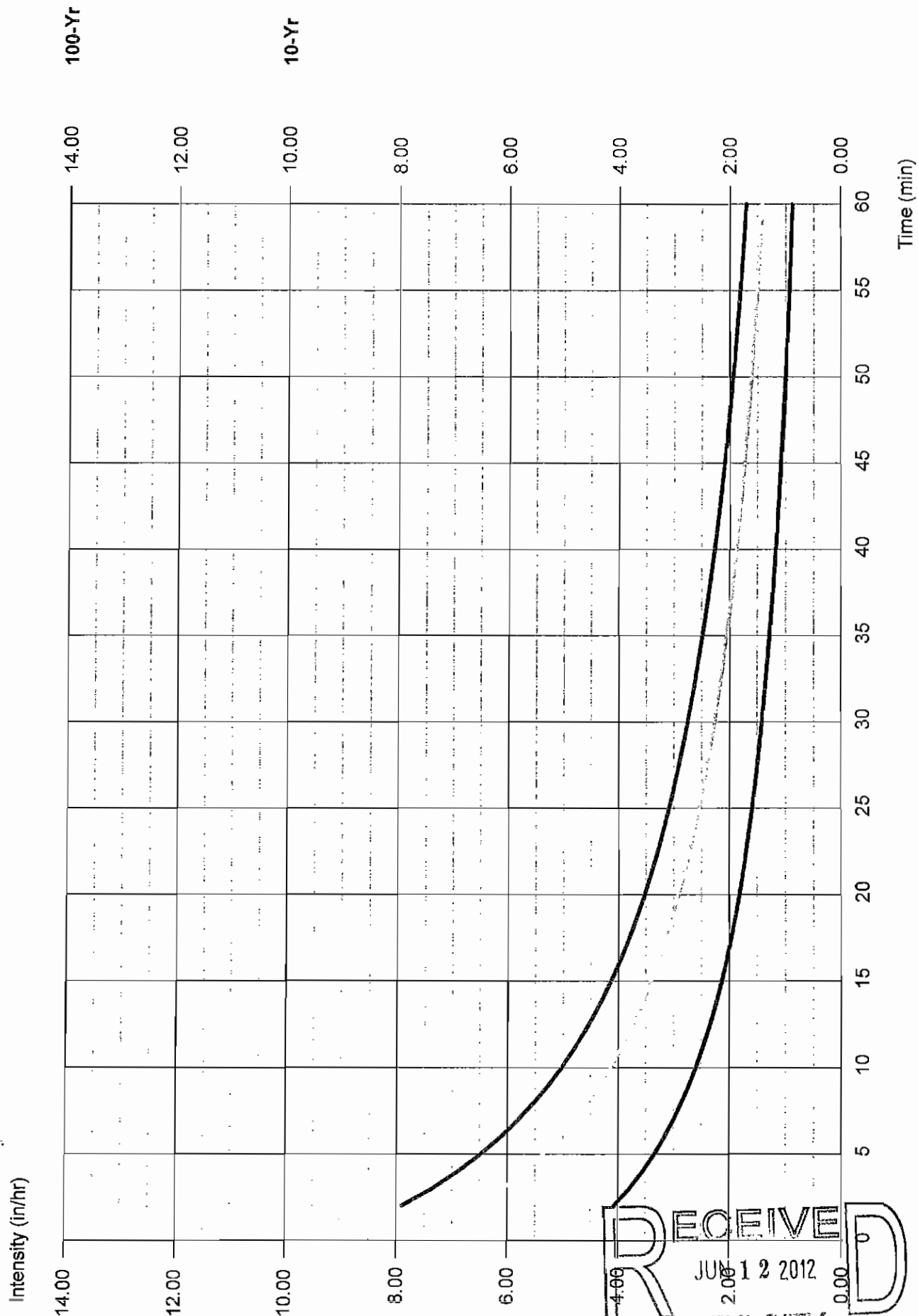


RAINFALL

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LEHI CITY

Hydrology IDF Curves

IDF file: ..average.IDF



RECEIVED
JUN 12 2012
LEHI CITY



NOAA Atlas 14, Volume 1, Version 6
 Location name: Lehi, Utah, US*
 Coordinates: 40.4373, -111.8674
 Elevation: 4978ft*
 * source: Google Maps



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Helm, Lillian Hiner, Kazungu Maitirika, Deborah Martin, Sandra Pavlovic, Ishant Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

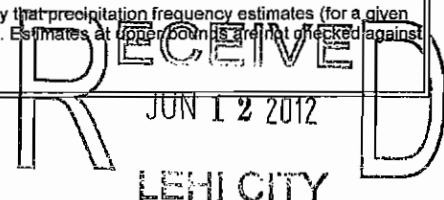
[PF tabular](#) | [PF graphical](#) | [Maps & aerials](#)

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches)¹										
Duration	Average recurrence interval(years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.128 (0.112-0.148)	0.162 (0.143-0.188)	0.223 (0.195-0.259)	0.279 (0.241-0.324)	0.366 (0.308-0.429)	0.447 (0.366-0.528)	0.541 (0.430-0.647)	0.652 (0.499-0.792)	0.830 (0.602-1.03)	0.992 (0.689-1.26)
10-min	0.195 (0.171-0.226)	0.247 (0.217-0.287)	0.339 (0.297-0.394)	0.424 (0.366-0.493)	0.557 (0.469-0.652)	0.681 (0.558-0.804)	0.824 (0.655-0.984)	0.993 (0.760-1.21)	1.26 (0.917-1.57)	1.51 (1.05-1.92)
15-min	0.242 (0.212-0.280)	0.306 (0.270-0.355)	0.421 (0.368-0.488)	0.526 (0.454-0.611)	0.690 (0.581-0.809)	0.844 (0.692-0.996)	1.02 (0.812-1.22)	1.23 (0.942-1.49)	1.57 (1.14-1.95)	1.87 (1.30-2.38)
30-min	0.325 (0.285-0.377)	0.413 (0.363-0.478)	0.567 (0.495-0.657)	0.708 (0.611-0.823)	0.929 (0.783-1.09)	1.14 (0.931-1.34)	1.38 (1.09-1.64)	1.66 (1.27-2.01)	2.11 (1.53-2.62)	2.52 (1.75-3.20)
60-min	0.403 (0.353-0.466)	0.511 (0.449-0.592)	0.701 (0.613-0.813)	0.876 (0.756-1.02)	1.15 (0.969-1.35)	1.41 (1.15-1.66)	1.70 (1.35-2.03)	2.05 (1.57-2.49)	2.61 (1.90-3.25)	3.12 (2.17-3.97)
2-hr	0.503 (0.456-0.571)	0.630 (0.566-0.712)	0.823 (0.735-0.932)	1.00 (0.887-1.14)	1.29 (1.12-1.48)	1.56 (1.31-1.79)	1.87 (1.53-2.16)	2.24 (1.76-2.66)	2.83 (2.11-3.46)	3.37 (2.40-4.21)
3-hr	0.582 (0.531-0.649)	0.720 (0.658-0.801)	0.912 (0.827-1.01)	1.09 (0.979-1.21)	1.37 (1.21-1.53)	1.61 (1.39-1.82)	1.91 (1.60-2.19)	2.26 (1.84-2.69)	2.85 (2.21-3.49)	3.38 (2.52-4.26)
6-hr	0.762 (0.706-0.829)	0.936 (0.866-1.02)	1.14 (1.05-1.25)	1.32 (1.22-1.45)	1.59 (1.44-1.75)	1.82 (1.61-2.01)	2.07 (1.81-2.32)	2.38 (2.03-2.71)	2.95 (2.44-3.53)	3.44 (2.77-4.30)
12-hr	0.967 (0.893-1.05)	1.18 (1.09-1.29)	1.43 (1.32-1.56)	1.64 (1.50-1.80)	1.95 (1.76-2.14)	2.20 (1.96-2.44)	2.46 (2.16-2.76)	2.76 (2.38-3.14)	3.23 (2.71-3.76)	3.62 (2.96-4.33)
24-hr	1.08 (1.01-1.16)	1.33 (1.24-1.43)	1.58 (1.48-1.70)	1.79 (1.68-1.92)	2.08 (1.94-2.23)	2.30 (2.13-2.46)	2.52 (2.33-2.79)	2.78 (2.53-3.17)	3.26 (2.78-3.79)	3.65 (2.99-4.37)
2-day	1.28 (1.20-1.37)	1.57 (1.47-1.68)	1.87 (1.75-2.00)	2.12 (1.98-2.26)	2.45 (2.29-2.62)	2.71 (2.52-2.69)	2.97 (2.75-3.17)	3.23 (2.97-3.46)	3.57 (3.26-3.86)	3.83 (3.48-4.42)
3-day	1.40 (1.30-1.50)	1.71 (1.59-1.84)	2.04 (1.90-2.20)	2.32 (2.16-2.49)	2.70 (2.51-2.90)	2.99 (2.77-3.22)	3.29 (3.03-3.54)	3.60 (3.29-3.88)	4.00 (3.63-4.35)	4.31 (3.89-4.83)
4-day	1.51 (1.40-1.64)	1.85 (1.72-2.01)	2.22 (2.06-2.39)	2.52 (2.34-2.72)	2.95 (2.72-3.18)	3.28 (3.02-3.54)	3.62 (3.32-3.92)	3.96 (3.61-4.30)	4.43 (4.00-4.83)	4.80 (4.30-5.25)
7-day	1.79 (1.65-1.94)	2.19 (2.03-2.36)	2.61 (2.42-2.83)	2.96 (2.74-3.20)	3.43 (3.17-3.71)	3.80 (3.50-4.10)	4.16 (3.82-4.50)	4.53 (4.14-4.91)	5.02 (4.54-5.46)	5.38 (4.85-5.88)
10-day	2.01 (1.86-2.17)	2.46 (2.28-2.66)	2.92 (2.72-3.15)	3.29 (3.06-3.54)	3.78 (3.50-4.08)	4.14 (3.82-4.45)	4.49 (4.14-4.84)	4.84 (4.45-5.22)	5.28 (4.83-5.72)	5.61 (5.10-6.09)
20-day	2.65 (2.45-2.85)	3.25 (3.00-3.50)	3.83 (3.55-4.13)	4.29 (3.98-4.61)	4.87 (4.50-5.23)	5.28 (4.89-5.68)	5.68 (5.25-6.11)	6.06 (5.58-6.52)	6.52 (5.99-7.03)	6.84 (6.26-7.40)
30-day	3.19 (2.95-3.43)	3.90 (3.62-4.20)	4.59 (4.26-4.94)	5.13 (4.76-5.51)	5.82 (5.40-6.25)	6.33 (5.85-6.80)	6.81 (6.29-7.34)	7.27 (6.70-7.85)	7.85 (7.20-8.50)	8.26 (7.55-8.97)
45-day	3.96 (3.69-4.26)	4.84 (4.51-5.21)	5.68 (5.30-6.10)	6.33 (5.90-6.79)	7.16 (6.67-7.67)	7.75 (7.21-8.30)	8.31 (7.72-8.91)	8.84 (8.19-9.49)	9.47 (8.76-10.2)	9.91 (9.13-10.7)
60-day	4.69 (4.37-5.04)	5.74 (5.34-6.17)	6.72 (6.26-7.20)	7.47 (6.97-8.01)	8.42 (7.84-9.03)	9.10 (8.48-9.75)	9.73 (9.04-10.4)	10.3 (9.57-11.1)	11.0 (10.2-11.9)	11.5 (10.6-12.4)

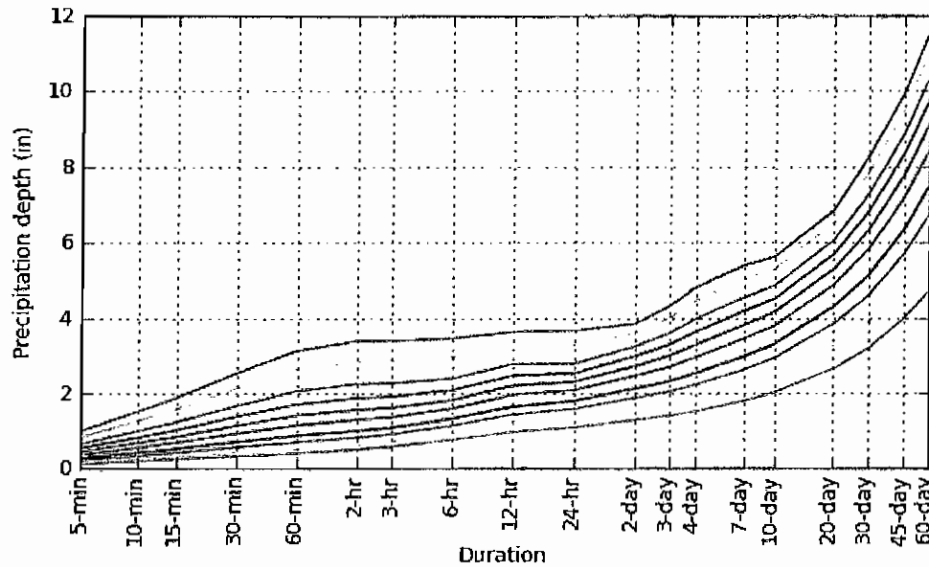
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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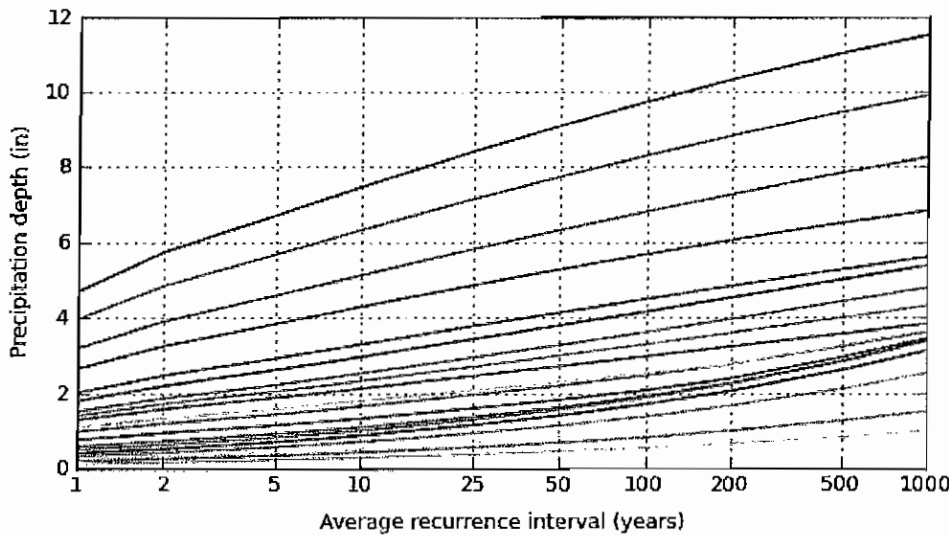


PF graphical

PDS-based depth-duration-frequency (DDF) curves
 Coordinates: 40.4373, -111.8674



Average recurrence interval (years)
1
2
5
10
25
50
100
200
500
1000



Duration	
5-min	2-day
10-min	3-day
15-min	4-day
30-min	7-day
60-min	10-day
2-hr	20-day
3-hr	30-day
6-hr	45-day
12-hr	60-day
24-hr	

NOAA/NWS/OHD/HDSC

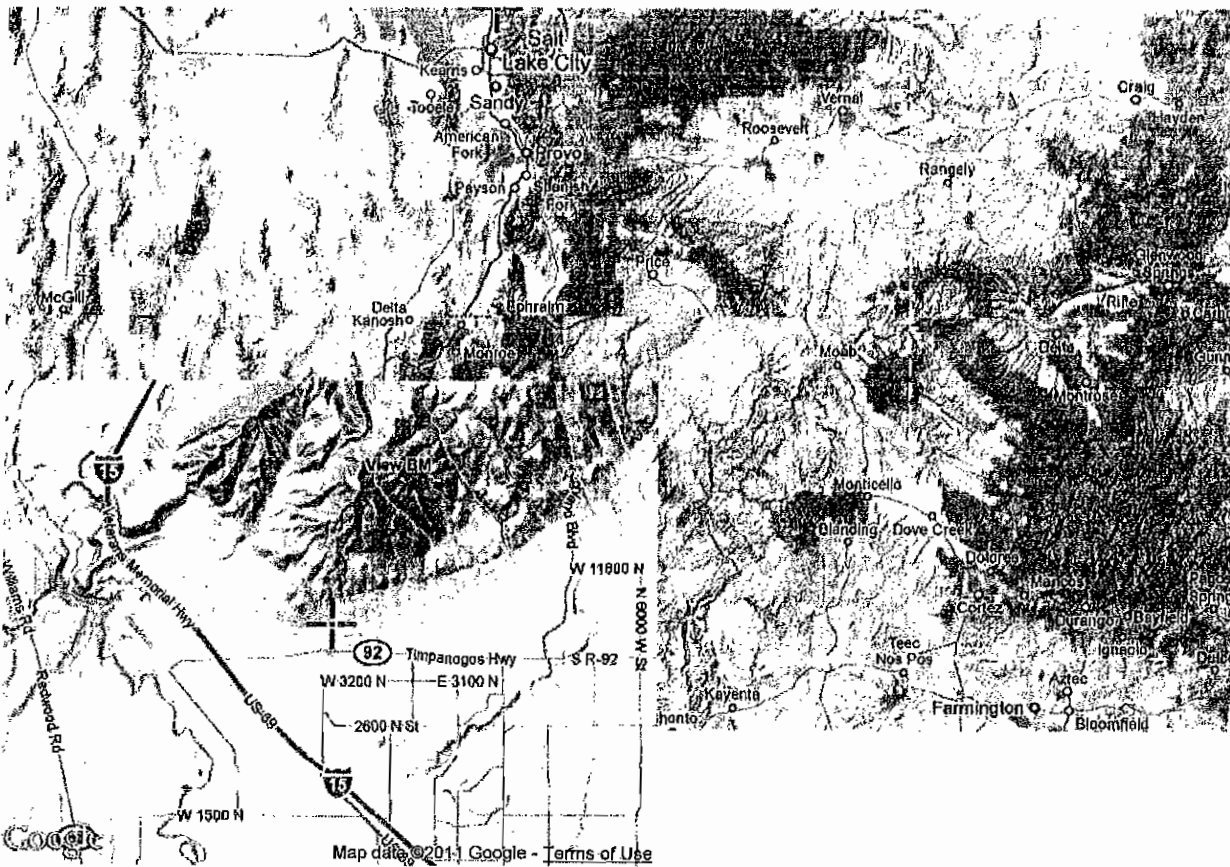
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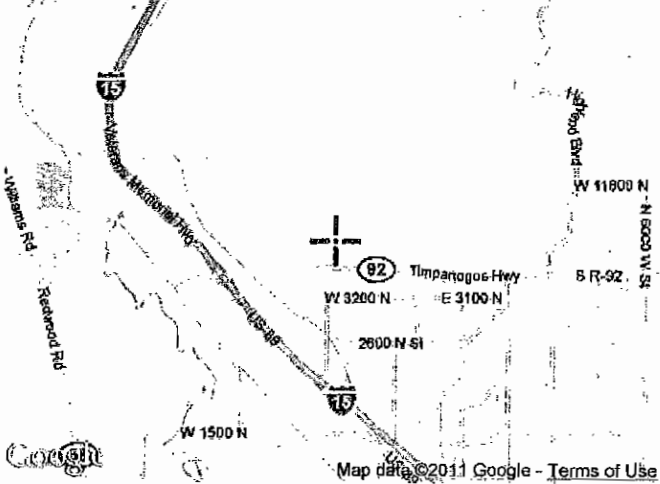
Maps & aeriels

Small scale terrain





Large scale map



Large scale aerial



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 LEHI CITY



NOAA Atlas 14, Volume 1, Version 5
 Location name: Lehi, Utah, US*
 Coordinates: 40.4373, -111.8674
 Elevation: 4978ft*
 * source: Google Maps



POINT PRECIPITATION FREQUENCY ESTIMATES

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NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aeriels](#)

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour) ¹										
Duration	Average recurrence interval(years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	1.54 (0.84-1.78)	1.94 (1.72-2.26)	2.68 (2.34-3.11)	3.35 (2.89-3.89)	4.39 (3.70-5.15)	5.36 (4.39-6.34)	6.49 (5.16-7.76)	7.82 (5.99-9.50)	9.96 (7.22-12.4)	11.9 (8.27-15.1)
10-min	1.17 (1.03-1.36)	1.48 (1.30-1.72)	2.03 (1.78-2.36)	2.54 (2.20-2.96)	3.34 (2.81-3.91)	4.09 (3.35-4.82)	4.94 (3.93-5.90)	5.96 (4.56-7.23)	7.58 (5.50-9.43)	9.06 (6.29-11.5)
15-min	0.968 (0.848-1.12)	1.22 (1.08-1.42)	1.68 (1.47-1.95)	2.10 (1.82-2.44)	2.76 (2.32-3.24)	3.38 (2.77-3.98)	4.09 (3.25-4.88)	4.92 (3.77-5.98)	6.26 (4.55-7.79)	7.49 (5.20-9.52)
30-min	0.650 (0.570-0.754)	0.826 (0.726-0.956)	1.13 (0.990-1.31)	1.42 (1.22-1.65)	1.86 (1.57-2.18)	2.27 (1.86-2.68)	2.75 (2.19-3.28)	3.32 (2.54-4.03)	4.22 (3.06-5.25)	5.04 (3.50-6.41)
60-min	0.403 (0.353-0.466)	0.511 (0.449-0.592)	0.701 (0.613-0.813)	0.876 (0.756-1.02)	1.15 (0.969-1.35)	1.41 (1.15-1.66)	1.70 (1.35-2.03)	2.05 (1.57-2.49)	2.61 (1.90-3.25)	3.12 (2.17-3.97)
2-hr	0.252 (0.228-0.286)	0.315 (0.283-0.356)	0.412 (0.368-0.466)	0.501 (0.444-0.569)	0.646 (0.558-0.738)	0.779 (0.656-0.897)	0.936 (0.762-1.09)	1.12 (0.876-1.33)	1.42 (1.05-1.73)	1.69 (1.20-2.11)
3-hr	0.194 (0.177-0.216)	0.240 (0.219-0.267)	0.304 (0.275-0.338)	0.362 (0.326-0.404)	0.455 (0.401-0.510)	0.536 (0.463-0.607)	0.636 (0.534-0.730)	0.763 (0.613-0.896)	0.947 (0.736-1.16)	1.13 (0.839-1.42)
6-hr	0.127 (0.118-0.138)	0.156 (0.145-0.171)	0.191 (0.176-0.208)	0.221 (0.203-0.241)	0.266 (0.240-0.292)	0.303 (0.270-0.335)	0.346 (0.302-0.388)	0.398 (0.340-0.452)	0.492 (0.407-0.589)	0.575 (0.463-0.718)
12-hr	0.080 (0.074-0.087)	0.098 (0.091-0.107)	0.119 (0.109-0.130)	0.136 (0.125-0.149)	0.162 (0.146-0.178)	0.182 (0.163-0.202)	0.204 (0.179-0.229)	0.229 (0.197-0.260)	0.268 (0.225-0.312)	0.300 (0.246-0.359)
24-hr	0.045 (0.042-0.048)	0.055 (0.052-0.059)	0.066 (0.062-0.071)	0.075 (0.070-0.080)	0.087 (0.081-0.093)	0.096 (0.089-0.103)	0.105 (0.097-0.116)	0.116 (0.105-0.132)	0.136 (0.116-0.158)	0.152 (0.124-0.182)
2-day	0.027 (0.025-0.029)	0.033 (0.031-0.035)	0.039 (0.036-0.042)	0.044 (0.041-0.047)	0.051 (0.048-0.055)	0.056 (0.052-0.060)	0.062 (0.057-0.066)	0.067 (0.062-0.072)	0.074 (0.068-0.080)	0.080 (0.072-0.092)
3-day	0.019 (0.018-0.021)	0.024 (0.022-0.026)	0.028 (0.026-0.031)	0.032 (0.030-0.035)	0.037 (0.035-0.040)	0.042 (0.038-0.045)	0.046 (0.042-0.049)	0.050 (0.046-0.054)	0.056 (0.050-0.060)	0.060 (0.054-0.067)
4-day	0.016 (0.015-0.017)	0.019 (0.018-0.021)	0.023 (0.021-0.025)	0.026 (0.024-0.028)	0.031 (0.028-0.033)	0.034 (0.031-0.037)	0.038 (0.035-0.041)	0.041 (0.038-0.045)	0.046 (0.042-0.050)	0.050 (0.045-0.055)
7-day	0.011 (0.010-0.012)	0.013 (0.012-0.014)	0.016 (0.014-0.017)	0.018 (0.016-0.019)	0.020 (0.019-0.022)	0.023 (0.021-0.024)	0.025 (0.023-0.027)	0.027 (0.025-0.029)	0.030 (0.027-0.032)	0.032 (0.029-0.035)
10-day	0.008 (0.008-0.009)	0.010 (0.010-0.011)	0.012 (0.011-0.013)	0.014 (0.013-0.015)	0.016 (0.015-0.017)	0.017 (0.016-0.019)	0.019 (0.017-0.020)	0.020 (0.019-0.022)	0.022 (0.020-0.024)	0.023 (0.021-0.025)
20-day	0.006 (0.005-0.006)	0.007 (0.006-0.007)	0.008 (0.007-0.009)	0.009 (0.008-0.010)	0.010 (0.009-0.011)	0.011 (0.010-0.012)	0.012 (0.011-0.013)	0.013 (0.012-0.014)	0.014 (0.012-0.015)	0.014 (0.013-0.015)
30-day	0.004 (0.004-0.005)	0.005 (0.005-0.006)	0.006 (0.006-0.007)	0.007 (0.007-0.008)	0.008 (0.007-0.009)	0.009 (0.008-0.009)	0.009 (0.009-0.010)	0.010 (0.009-0.011)	0.011 (0.010-0.012)	0.011 (0.010-0.012)
45-day	0.004 (0.003-0.004)	0.004 (0.004-0.005)	0.005 (0.005-0.006)	0.006 (0.005-0.006)	0.007 (0.006-0.007)	0.007 (0.007-0.008)	0.008 (0.007-0.008)	0.008 (0.008-0.009)	0.009 (0.008-0.009)	0.009 (0.008-0.010)
60-day	0.003 (0.003-0.003)	0.004 (0.004-0.004)	0.005 (0.004-0.005)	0.005 (0.005-0.006)	0.006 (0.005-0.006)	0.006 (0.006-0.007)	0.007 (0.006-0.007)	0.007 (0.007-0.008)	0.008 (0.007-0.008)	0.008 (0.007-0.009)

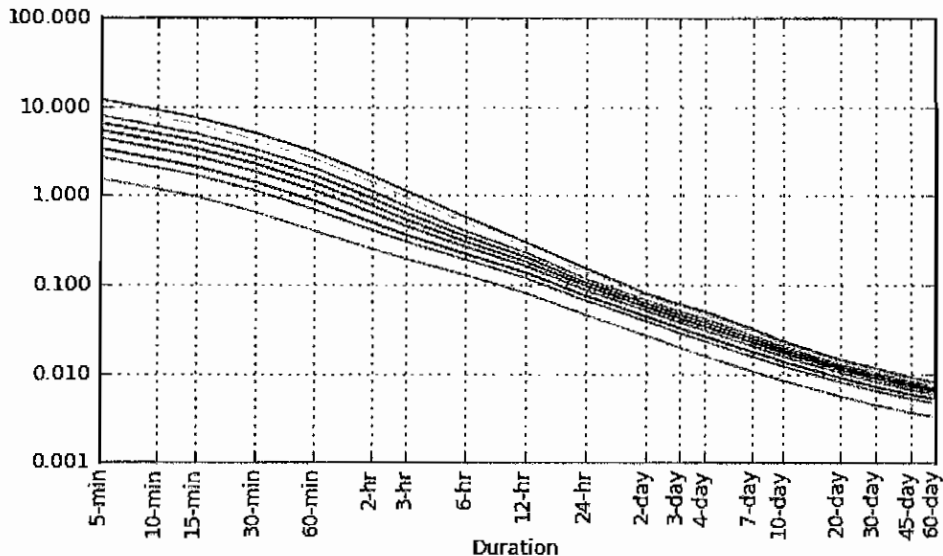
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS). Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

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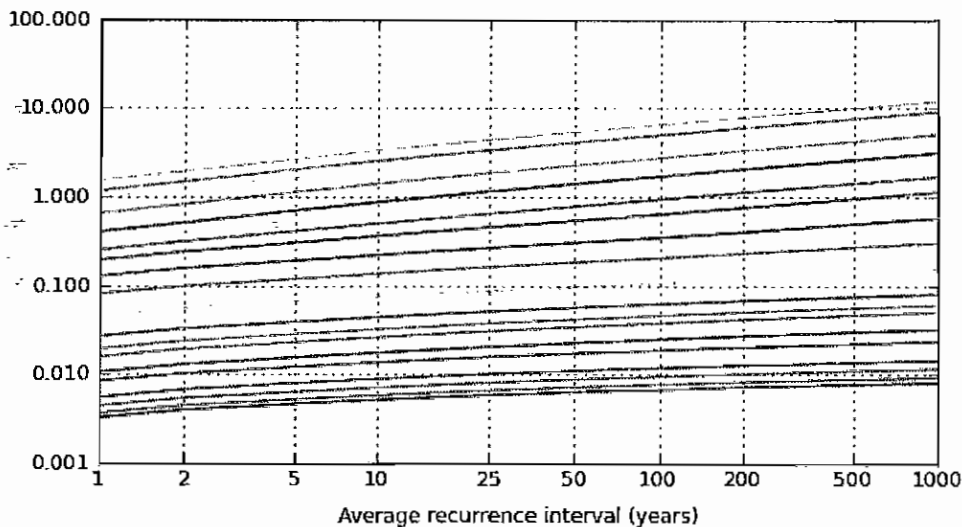
PF graphical

PDS-based intensity-duration-frequency (IDF) curves

Coordinates: 40.4373, -111.8674



Average recurrence interval (years)
1
2
5
10
25
50
100
200
500
1000



Duration
5-min
10-min
15-min
30-min
60-min
2-hr
3-hr
6-hr
12-hr
24-hr
2-day
3-day
4-day
7-day
10-day
20-day
30-day
45-day
60-day

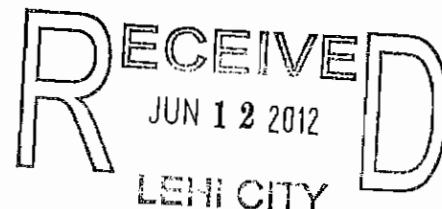
NOAA/NWS/OHD/HDSC

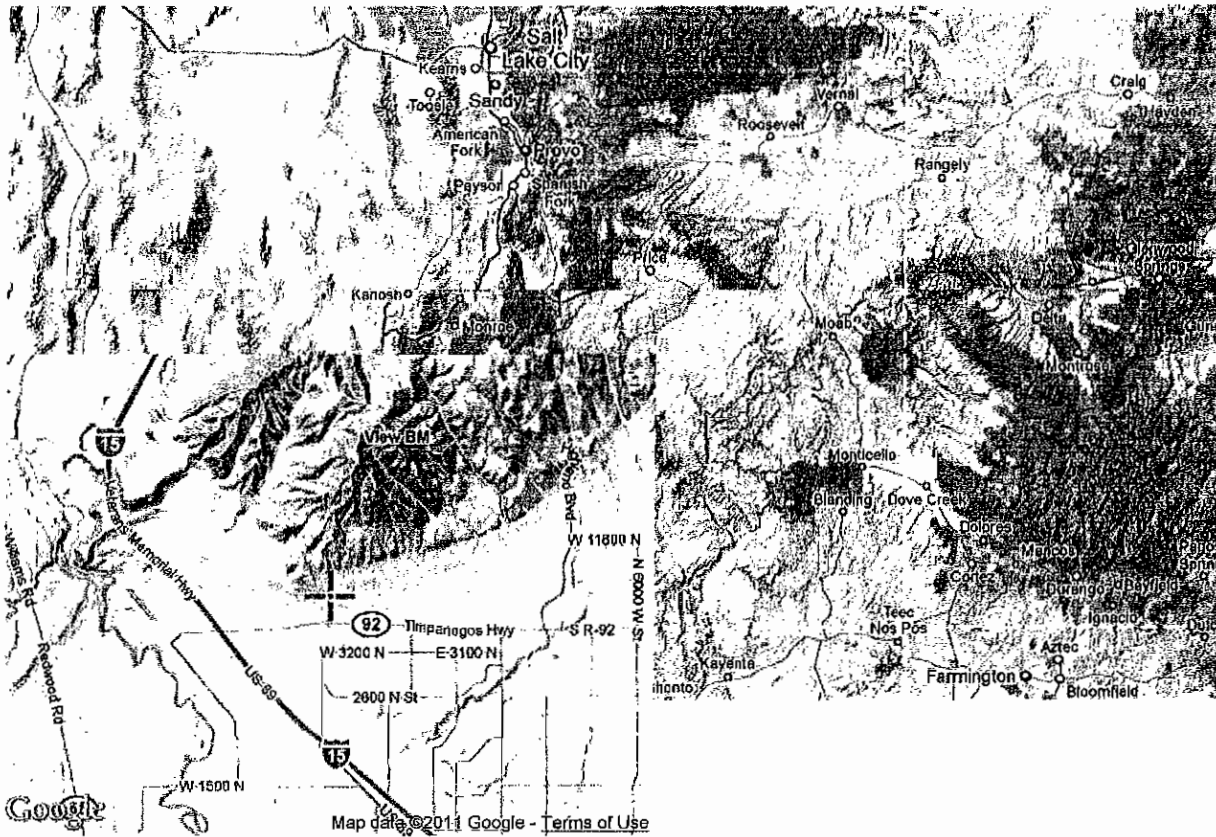
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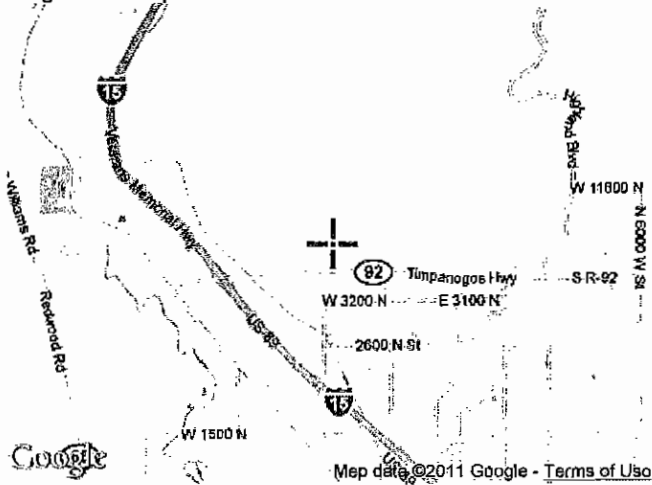
Maps & aeriels

Small scale terrain





Large scale map



Large scale aerial



LEHI CITY
AGREEMENT & UDOT
EXHIBITS

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LEHI CITY

AGREEMENT

For

LEHI CITY DETENTION & STORM DRAIN FACILITIES AT PILGRIM'S LANDING

Between

**LEHI CITY and PILGRIM'S LANDING, LLC and
MOUNTAIN HOME DEVELOPMENT CORPORATION**

WHEREAS, Lehi City owns an existing 8.10 acre foot detention basin (the "Traverse Mountain Detention Basin") on a 9.46 acre parcel located in the Traverse Mountain Development (Parcel No.: 53:257:0001) (the "Development Property");

WHEREAS, Lehi City owns and maintains an existing detention facility (the "Pilgrim's Landing Detention Basin") along the western edge of the Pilgrim's Landing, LLC property, and has already purchased an additional 1.15 acres of adjacent property from Pilgrim's Landing, LLC;

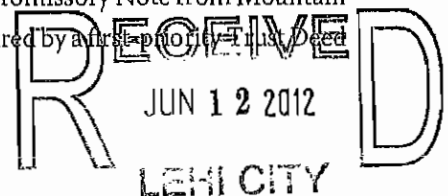
WHEREAS, Lehi City is currently in the process of designing and constructing a 72-inch storm drain and detention basin along and in property owned by Pilgrim's Landing, LLC;

WHEREAS, Lehi City desires to acquire additional land from Pilgrim's Landing, LLC to upgrade and increase the Pilgrim's Landing Detention Basin's capacity to serve the residents of Lehi City, drainage from I-15, SR-92, and Traverse Mountain Development (including replacement of the Traverse Mountain Detention Basin), and to provide a multi-use facility; and

WHEREAS, Mountain Home Development Corporation desires to acquire from Lehi City the Development Property for commercial development purposes, and Lehi City is willing to convey such property to Mountain Home Development Corporation on the terms and conditions set forth herein.

NOW THEREFORE, in consideration of the foregoing premises and the mutual promises contained herein, the Parties hereto agree as follows:

1. Pilgrim's Landing, LLC will sign a Special Warranty Deed to Lehi City for the property needed to increase the area of the Pilgrim's Landing Detention Basin to approximately 18.75 acres. (See attached Exhibit A.) The price of the sale will be \$2,890,000.00.
2. Lehi City will pay Pilgrim's Landing, LLC \$200,000.00 to be applied toward the total purchase price, reducing the amount owing to \$2,690,000.00. In consideration of Mountain Home Development Corporation being able to purchase the Development Property, it agrees to pay to Pilgrim's Landing, LLC the balance of the purchase price (\$2,690,000.00), to be evidenced by a Promissory Note from Mountain Home Development Corporation in favor of Pilgrim's Landing, LLC, secured by a first-priority Trust Deed on the Development Property in favor of Pilgrim's Landing, LLC.



3. Lehi City will construct a detention basin on the property purchased from Pilgrim's Landing, LLC with a capacity of 17.1 acre feet, and upon completion thereof Lehi City will decommission the detention basin on the Development Property.
4. Lehi City will sign a Special Warranty Deed to Mountain Home Development Corporation for the 9.46 acre parcel (County Parcel No.: 53:257:0001, see attached Exhibit B) per the Area Plan Note #4, page 1 on the concept plan approved by Lehi City on November 18, 2008 which shall be used for commercial purposes only as generally described in the Area Plan.
5. Mountain Home Development Corporation will execute a promissory note and a first-position trust deed on the 9.46 acre parcel in favor of Pilgrim's Landing, LLC with the following terms:
 - a. The promissory note shall be in the principal amount of \$2,690,000.00, plus interest at the rate of 7% per annum.
 - b. Annual interest payments of \$188,300.00 shall be due on each anniversary date of the Promissory Note, and all unpaid principal and accrued interest shall be due on the 3rd anniversary of the Promissory Note.
 - c. The Trust Deed on the Development Property shall be in the amount of \$2,690,000.00, plus accrued interest, with a 3-year maturity date.
 - d. Mountain Home Development Corporation's obligations under the trust deed will be recourse only to the property encumbered by the trust deed.
 - e. If Pilgrim's Landing, LLC and/or its successors and assigns forecloses on the trust deed and acquires ownership of the 9.46 acre parcel, all owners of the parcel will hold the parcel subject to the Traverse Mountain Area Plan and CC&R's, all as in effect from time to time.
6. Lehi City will own and agrees to diligently proceed to build and maintain the new storm drain and detention facility to be built on the property purchased from Pilgrim's Landing, LLC.
7. Mountain Home Development Corporation will expand at its own cost the new storm basin to 37 acre feet in the future as capacity is needed.
8. Mountain Home Development Corporation will provide the trust deed in form and substance acceptable to Pilgrim's Landing, LLC in its sole discretion.
9. Lehi City will provide all legal documents for the Special Warranty Deeds in form and substance acceptable to the grantees of such Special Warranty Deeds.
10. The grantors of the Special Warranty Deeds shall provide at their cost an ALTA standard owner's policy insuring title to the subject properties, respectively, with only such exceptions as may be approved by the grantees.



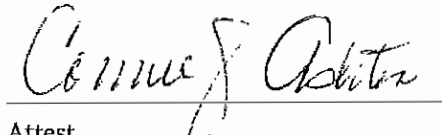
11. Lehi City, Pilgrim's Landing, LLC, and Mountain Home Development Corporation agree to close with Affiliated First Title Company, 321 East State Road, American Fork, UT 84003, Attention: Marnae Ballantyne.

Signed:


Lehi City

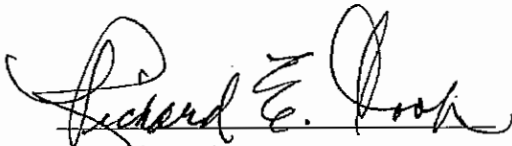
7-28-10
Date

Lehi City Mayor
Title


Attest

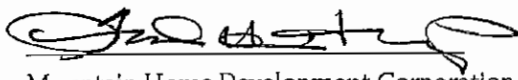
7/28/10
Date

City Recorder
Title


Pilgrim's Landing, LLC

7/28/10
Date

Manager
Title


Mountain Home Development Corporation
By Ted Heap, CEO

7/28/10
Date

CEO
Title

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Exhibit "B"

Lehi City to Traverse Mountain

Lot 1, Plat A, Traverse Mountain Subdivision.

Area = 9.455 acres

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10 YEAR HEC-1

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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* MAY 1991
* VERSION 4.0.1E
*
* RUN DATE TIME
*
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*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
*
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X X XXXXXXX XXXXX X
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XXXXXXX XXXX X XXXXX X
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X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	HEC-1 Analysis using WMS									
2	ID	10 year developed flow									
3	ID	MAY 2012									
4	IT	10	07MAY09	0	130						
5	IO	5									
6	IN	6	07MAY09	0							
7	JD	1.79	10.0								
8	* typeII-24hour										
9	PC	0.0	0.001	0.002	0.0031	0.0041	0.0051	0.0062	0.0073	0.0083	0.0094
10	PC	0.0105	0.0116	0.0127	0.0138	0.015	0.0161	0.0173	0.0185	0.0196	0.0208
11	PC	0.022	0.0232	0.0244	0.0256	0.0269	0.0281	0.0294	0.0307	0.0319	0.0332
12	PC	0.0345	0.0358	0.0371	0.0384	0.0398	0.0411	0.0425	0.0439	0.0452	0.0466
13	PC	0.048	0.0494	0.0508	0.0523	0.0538	0.0553	0.0568	0.0583	0.0598	0.0614
14	PC	0.063	0.0646	0.0662	0.0679	0.0696	0.0712	0.073	0.0747	0.0764	0.0782
15	PC	0.08	0.0818	0.0836	0.0855	0.0874	0.0892	0.0912	0.0931	0.095	0.097
16	PC	0.099	0.101	0.103	0.1051	0.1072	0.1093	0.1114	0.1135	0.1156	0.1178
17	PC	0.12	0.1223	0.1246	0.1271	0.1296	0.1323	0.135	0.1379	0.1408	0.1439
18	PC	0.147	0.1502	0.1534	0.1566	0.1598	0.163	0.1663	0.1697	0.1733	0.1771
19	PC	0.181	0.1851	0.1895	0.1941	0.1989	0.204	0.2094	0.2152	0.2214	0.228
20	PC	0.235	0.2427	0.2513	0.2609	0.2715	0.283	0.3068	0.3544	0.4308	0.5679
21	PC	0.663	0.682	0.6986	0.713	0.7252	0.735	0.7434	0.7514	0.7588	0.7656



LINE	ID	1	2	3	4	5	6	7	8	9	10
46	KK	37R	CNAME	37C							
47	KO	0	0	0.0	0	22					
48	RS	1	FLOW	0.0	0.0						
		* 37C Volume									
49	SV	0.00	1266630.253327	0.379990	5066530.633316	0.759980	8866431.0133061	1.39969			
50	SV	1.26661	3932961.5199591	6466221.7732861	8999492.0266122	1532752.2799392	406602				
		* 37C Elevation									
51	SE	4742.04742	4214742.8424743	2634743.6844744	1054744.5264744	9474745.3684745	789				
52	SE	4746.24746	6314747.0524747	4734747.8944748	3154748.7364749	1574749.578	4750.0				
		* 37C Discharge									
53	SQ	0.02	197453	8.3679616	4140423.1448215	9029218.6881421	1090223.2794925	26417			
54	SQ	27.10328	8264930.4517731	9946033.4663734	8761036.2310137	5370538.7991540	02147				
		* 37C Elevation									
55	SE	4742.04742	4214742.8424743	2634743.6844744	1054744.5264744	9474745.3684745	789				
56	SE	4746.24746	6314747.0524747	4734747.8944748	3154748.7364749	1574749.578	4750.0				
57	KK	11B									
58	KO	0	0	0.0	0	22					
59	BA	0.1161									
60	LS	0.0	57.0	0.0							
61	UD	0.0767									
62	KK	6R	CNAME	6C							
63	KO	0	0	0.0	0	22					
64	RN	6R									
65	KK	10B									
66	KO	0	0	0.0	0	22					
67	BA	0.1616									
68	LS	0.0	71.74	0.0							
69	UD	0.1283									
70	KK	13C	CNAME	13R							
71	KO	0	0	0.0	0	22					
72	HC	2									
73	KK	13R	CNAME	13C							
74	KO	0	0	0.0	0	22					
75	RS	1	FLOW	0.0	0.0						
		* 13C Volume									
	SV	0.00	9742581.9639382	969202	3.990215	0271236	0801017	1493058	2348969	337034	
	SV	10.45511	5915912.7443313	9142715	1015516	3063517	5288218	7691220	0274121	30386	
		* 13C Elevation									
	SE	4800.04800	5264801.0524801	5784802.1054802	6314803	1574803	6844804	2104804	736		
	SE	4805.24805	7894806.3154806	8424807.3684807	8944808	4214808	9474809	473	4810.0		
		* 13C Discharge									
	SQ	0.03	42952912.3279421	8209515	9029219	3218222	2207724	7829127	1039229	24128	
	SQ	31.23233	1045734.8761036	5618938	1733239	7194241	2075542	6437844	0331945	38008	
		* 13C Elevation									
	SE	4800.04800	5264801.0524801	5784802.1054802	6314803	1574803	6844804	2104804	736		
	SE	4805.24805	7894806.3154806	8424807.3684807	8944808	4214808	9474809	473	4810.0		

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LINE	ID	1	2	3	4	5	6	7	8	9	10
126	KK	83B									
127	KO	0	0	0.0	0	22					
128	BA	0.5686									
129	LS	0.0	58.07	0.0							
130	UD	0.0556									
131	KK	19R	CNAME	19C							
132	KO	0	0	0.0	0	22					
133	RN	19R									
134	KK	86B									
135	KO	0	0	0.0	0	22					
136	BA	0.0259									
137	LS	0.0	73.61	0.0							
138	UD	0.0556									
139	KK	21C	CNAME	21R							
140	KO	0	0	0.0	0	22					
141	HC	2									
142	KK	85B									
143	KO	0	0	0.0	0	22					
144	BA	0.1593									
145	LS	0.0	63.35	0.0							
146	UD	0.0556									
147	KK	16C	CNAME	16R							
148	KO	0	0	0.0	0	22					
149	HC	2									
150	KK	81B									
151	KO	0	0	0.0	0	22					
152	BA	0.1869									
153	LS	0.0	58.02	0.0							
154	UD	0.0556									
155	KK	17R	CNAME	17C							
156	KO	0	0	0.0	0	22					
157	RN	17R									
158	KK	84B									
159	KO	0	0	0.0	0	22					
160	BA	0.1198									
161	LS	0.0	67.12	0.0							
162	UD	0.0556									
163	KK	20C	CNAME	20R							
164	KO	0	0	0.0	0	22					
165	HC	3									

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LINE	ID	1	2	3	4	5	6	7	8	9	10
208	KK	176B									
209	KO	0	0	0.0	0	22					
210	BA	0.0174									
211	LS	0.0	75.39	0.0							
212	UD	0.1412									
213	KK	41C	CNAME	41R							
214	KO	0	0	0.0	0	22					
215	HC	5									
216	KK	286B									
217	KO	0	0	0.0	1	22					
218	BA	0.4184									
219	LS	0.0	70.78	0.0							
220	UD	0.0268									
221	KK	181B									
222	KO	0	0	0.0	1	22					
223	BA	0.0313									
224	LS	0.0	77.05	0.0							
225	UD	0.0991									
226	KK	43C	CNAME	43R							
227	KO	0	0	0.0	0	22					
228	HC	3									
229	KK	2B									
230	KO	0	0	0.0	1	22					
231	BA	0.0817									
232	LS	0.0	81.16	0.0							
233	UD	0.3103									
234	KK	38R	CNAME	38C							
235	KO	0	0	0.0	0	22					
236	RN	38R									
237	KK	405B									
238	KO	0	0	0.0	1	22					
239	BA	0.0092									
240	LS	0.0	80.21	0.0							
241	UD	0.0730									
242	KK	288B									
243	KO	0	0	0.0	1	22					
244	BA	0.0149									
245	LS	0.0	78.34	0.0							
246	UD	0.0664									
247	KK	44C	CNAME	44R							
248	KO	0	0	0.0	0	22					
249	HC	4									

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LINE	ID	1	2	3	4	5	6	7	8	9	10
250	KK	415B									
251	KO	0	0	0.0	1	22					
252	BA	0.0771									
253	LS	0.0	80.26	0.0							
254	UD	0.0921									
255	KK	459B									
256	KO	0	0	0.0	1	22					
257	BA	0.1803									
258	LS	0.0	79.85	0.0							
259	UD	0.1662									
260	KK	3C	CNAME	3R							
261	KO	0	0	0.0	0	22					
262	HC	4									
263	KK	163B									
264	KO	0	0	0.0	1	22					
265	BA	0.0618									
266	LS	0.0	80.62	0.0							
267	UD	0.1138									
268	KK	7B									
269	KO	0	0	0.0	1	22					
270	BA	0.0408									
271	LS	0.0	67.23	0.0							
272	UD	0.0556									
273	KK	411B									
274	KO	0	0	0.0	1	22					
275	BA	0.0331									
276	LS	0.0	79.74	0.0							
277	UD	0.0892									
278	KK	12C	CNAME	12R							
279	KO	0	0	0.0	0	22					
280	HC	4									
281	KK	12R	CNAME	12C							
282	KO	0	0	0.0	0	22					
283	RN	12R									
284	KK	141B									
285	KO	0	0	0.0	1	22					
286	BA	0.1600									
287	LS	0.0	69.57	0.0							
288	UD	0.1866									
289	KK	25R	CNAME	25C							
290	KO	0	0	0.0	0	22					
291	RD	1297.6	0.07153	0.013		CIRC	2.0	0.0			

LINE	ID	1	2	3	4	5	6	7	8	9	10
292	KK	139B									
293	KO	0	0	0.0	0	22					
294	BA	0.0660									
295	LS	0.0	61.27	0.0							
296	UD	0.0702									
297	KK	23R	CNAME	23C							
298	KO	0	0	0.0	0	22					
299	RD	1357.8	0.04276	0.013		CIRC	2.0	0.0			
300	KK	140B									
301	KO	0	0	0.0	0	22					
302	BA	0.0475									
303	LS	0.0	67.54	0.0							
304	UD	0.0616									
305	KK	24C	CNAME	24R							
306	KO	0	0	0.0	0	22					
307	HC	2									
308	KK	24R	CNAME	24C							
309	KO	0	0	0.0	0	22					
310	RD	3765.7	0.06856	0.013		CIRC	2.0	0.0			
311	KK	138B									
312	KO	0	0	0.0	0	22					
313	BA	0.1174									
314	LS	0.0	71.23	0.0							
315	UD	0.2069									
316	KK	18C	CNAME	18R							
317	KO	0	0	0.0	0	22					
318	HC	3									
319	KK	18R	CNAME	18C							
320	KO	0	0	0.0	0	22					
321	RD	3528.0	0.04879	0.013		TRAP	2.0	0.0			
322	KK	155B									
323	KO	0	0	0.0	0	22					
324	BA	0.0758									
325	LS	0.0	75.21	0.0							
326	UD	0.1458									
327	KK	149B									
328	KO	0	0	0.0	0	22					
329	BA	0.2020									
330	LS	0.0	80.17	0.0							
331	UD	0.2477									

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LINE	ID	1	2	3	4	5	6	7	8	9	10
370	KK	151B									
371	KO	0	0	0.0	0	22					
372	BA	0.0132									
373	LS	0.0	72.23	0.0							
374	UD	0.0337									
375	KK	150B									
376	KO	0	0	0.0	0	22					
377	BA	0.0461									
378	LS	0.0	79.46	0.0							
379	UD	0.0407									
380	KK	35C	CNAME	35R							
381	KO	0	0	0.0	0	22					
382	HC	2									
383	KK	35R	CNAME	35C							
384	KO	0	0	0.0	0	22					
385	RS	1	FLOW	0.0	0.0						
		* 35C Volume									
386	SV	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0
		* 35C Elevation									
387	SE	4815.0	4816.0	4817.0	4818.0	4819.0	4820.0	4821.0	4822.0	4823.0	4824.0
		* 35C Discharge									
388	SQ	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0
		* 35C Elevation									
389	SE	4815.0	4816.0	4817.0	4818.0	4819.0	4820.0	4821.0	4822.0	4823.0	4824.0
390	KK	143B									
391	KO	0	0	0.0	0	22					
392	BA	0.0414									
393	LS	0.0	74.0	0.0							
394	UD	0.0120									
395	KK	402B									
396	KO	0	0	0.0	0	22					
397	BA	0.0153									
398	LS	0.0	74.0	0.0							
399	UD	0.0514									
400	KK	33C	CNAME	33R							
401	KO	0	0	0.0	0	22					
402	HC	2									
403	KK	33R	CNAME	33C							
404	KO	0	0	0.0	0	22					
405	RS	1	FLOW	0.0	0.0						
		* 33C Volume									
406	SV	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0
		* 33C Elevation									
407	SE	4810.0	4811.0	4812.0	4813.0	4814.0	4815.0	4816.0	4817.0	4818.0	4819.0
		* 33C Discharge									
408	SQ	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0
		* 33C Elevation									

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RUNOFF SUMMARY

FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

+	OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
					6-HOUR	24-HOUR	72-HOUR			
+	HYDROGRAPH AT	329B	7.	12.00	1.	0.	0.	0.05		
+	HYDROGRAPH AT	403B	4.	12.00	1.	0.	0.	0.02		
+	2 COMBINED AT	37C	11.	12.00	2.	1.	1.	0.07		
+	ROUTED TO	37R	5.	12.33	2.	1.	1.	0.07	4742.62	12.33
+	HYDROGRAPH AT	11B	0.	18.33	0.	0.	0.	0.12		
+	ROUTED TO	6R	0.	18.33	0.	0.	0.	0.12		
+	HYDROGRAPH AT	10B	14.	12.00	3.	1.	1.	0.16		
+	2 COMBINED AT	13C	14.	12.00	3.	1.	1.	0.28		
+	ROUTED TO	13R	2.	14.00	2.	1.	1.	0.28	4800.34	14.00
+	HYDROGRAPH AT	98B	1.	12.33	1.	0.	0.	0.11		
+	ROUTED TO	29R	1.	12.33	1.	0.	0.	0.11		
+	HYDROGRAPH AT	408B	2.	12.00	1.	0.	0.	0.08		
+	HYDROGRAPH AT	99B	19.	12.00	2.	1.	1.	0.06		
+	3 COMBINED AT	30C	21.	12.00	3.	1.	1.	0.25		
+	HYDROGRAPH AT	103B	4.	12.17	1.	0.	0.	0.01		
+	HYDROGRAPH AT	401B	18.	12.17	3.	1.	1.	0.14		



+	3 COMBINED AT	32C	37.	12.00	7.	3.	3.	0.40
+	HYDROGRAPH AT	101B	1.	12.33	1.	0.	0.	0.11
+	ROUTED TO	31R	1.	12.33	1.	0.	0.	0.11
+	HYDROGRAPH AT	83B	1.	17.83	1.	0.	0.	0.57
+	ROUTED TO	19R	1.	17.83	1.	0.	0.	0.57
+	HYDROGRAPH AT	86B	4.	12.00	1.	0.	0.	0.03
+	2 COMBINED AT	21C	4.	12.00	1.	0.	0.	0.59
+	HYDROGRAPH AT	85B	1.	12.50	1.	0.	0.	0.16
+	2 COMBINED AT	16C	5.	12.00	2.	1.	1.	0.75
+	HYDROGRAPH AT	81B	0.	17.83	0.	0.	0.	0.19
+	ROUTED TO	17R	0.	17.83	0.	0.	0.	0.19
+	HYDROGRAPH AT	84B	4.	12.00	1.	0.	0.	0.12
+	3 COMBINED AT	20C	9.	12.00	3.	1.	1.	1.06
+	HYDROGRAPH AT	79B	1.	12.00	0.	0.	0.	0.02
+	ROUTED TO	15R	1.	12.00	0.	0.	0.	0.02
+	HYDROGRAPH AT	78B	0.	13.50	0.	0.	0.	0.08
+	2 COMBINED AT	8C	1.	12.00	0.	0.	0.	0.09
+	HYDROGRAPH AT	87B	1.	12.00	1.	0.	0.	0.06
+	2 COMBINED AT	22C	2.	12.00	1.	0.	0.	0.16
+	HYDROGRAPH AT	77B	0.	12.83	0.	0.	0.	0.06

+	3 COMBINED AT	7C	11.	12.00	4.	2.	2.	1.27
+	HYDROGRAPH AT	177B	0.	12.33	0.	0.	0.	0.02
+	HYDROGRAPH AT	248B	2.	12.00	1.	0.	0.	0.08
+	HYDROGRAPH AT	176B	3.	12.00	0.	0.	0.	0.02
+	5 COMBINED AT	41C	16.	12.00	6.	2.	2.	1.51
+	HYDROGRAPH AT	286B	41.	12.00	7.	2.	2.	0.42
+	HYDROGRAPH AT	181B	8.	12.00	1.	0.	0.	0.03
+	3 COMBINED AT	43C	65.	12.00	14.	5.	5.	1.96
+	HYDROGRAPH AT	2B	18.	12.17	4.	1.	1.	0.08
+	ROUTED TO	38R	18.	12.17	4.	1.	1.	0.08
+	HYDROGRAPH AT	405B	3.	12.00	0.	0.	0.	0.01
+	HYDROGRAPH AT	288B	5.	12.00	1.	0.	0.	0.01
+	4 COMBINED AT	44C	83.	12.00	18.	6.	6.	2.06
+	HYDROGRAPH AT	415B	27.	12.00	3.	1.	1.	0.08
+	HYDROGRAPH AT	459B	42.	12.00	7.	2.	2.	0.18
+	4 COMBINED AT	3C	190.	12.00	36.	12.	12.	2.72
+	HYDROGRAPH AT	163B	21.	12.00	3.	1.	1.	0.06
+	HYDROGRAPH AT	7B	1.	12.00	0.	0.	0.	0.04
+	HYDROGRAPH AT	411B	11.	12.00	1.	0.	0.	0.03
+	4 COMBINED AT							

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+		12C	224.	12.00	40.	14.	14.	2.86		
	ROUTED TO									
+		12R	224.	12.00	40.	14.	14.	2.86		
	HYDROGRAPH AT									
+		141B	8.	12.17	2.	1.	1.	0.16		
	ROUTED TO									
+		25R	8.	12.17	2.	1.	1.	0.16		
	HYDROGRAPH AT									
+		139B	0.	13.33	0.	0.	0.	0.07		
	ROUTED TO									
+		23R	0.	13.33	0.	0.	0.	0.07		
	HYDROGRAPH AT									
+		140B	2.	12.00	0.	0.	0.	0.05		
	2 COMBINED AT									
+		24C	2.	12.00	1.	0.	0.	0.11		
	ROUTED TO									
+		24R	2.	12.17	1.	0.	0.	0.11		
	HYDROGRAPH AT									
+		138B	8.	12.17	2.	1.	1.	0.12		
	3 COMBINED AT									
+		18C	18.	12.17	5.	2.	2.	0.39		
	ROUTED TO									
+		18R	16.	12.17	5.	2.	2.	0.39		
	HYDROGRAPH AT									
+		155B	11.	12.00	2.	1.	1.	0.08		
	HYDROGRAPH AT									
+		149B	46.	12.17	8.	3.	3.	0.20		
	2 COMBINED AT									
+		4C	57.	12.17	10.	3.	3.	0.28		
	ROUTED TO									
+		4R	16.	12.83	14.	13.	13.	0.28	4812.09	12.83
+										
	HYDROGRAPH AT									
+		30B	17.	12.17	3.	1.	1.	0.15		
	HYDROGRAPH AT									
+		66B	7.	12.00	1.	0.	0.	0.05		
	4 COMBINED AT									
+		11C	50.	12.17	23.	16.	16.	0.87		
	ROUTED TO									
+		11R	50.	12.17	23.	16.	16.	0.87		

+	HYDROGRAPH AT	241B	10.	12.17	2.	1.	1.	0.09		
+	ROUTED TO	10R	10.	12.17	2.	1.	1.	0.09		
+	HYDROGRAPH AT	151B	2.	12.00	0.	0.	0.	0.01		
+	HYDROGRAPH AT	150B	16.	12.00	2.	1.	1.	0.05		
+	2 COMBINED AT	35C	17.	12.00	2.	1.	1.	0.06		
+	ROUTED TO	35R	5.	0.17	5.	5.	5.	0.06	4815.00	0.00
+	HYDROGRAPH AT	143B	7.	12.00	1.	0.	0.	0.04		
+	HYDROGRAPH AT	402B	3.	12.00	0.	0.	0.	0.02		
+	2 COMBINED AT	33C	10.	12.00	1.	0.	0.	0.06		
+	ROUTED TO	33R	5.	0.17	5.	5.	5.	0.06	4810.01	12.17
+	HYDROGRAPH AT	407B	3.	12.00	0.	0.	0.	0.02		
+	HYDROGRAPH AT	406B	1.	12.00	0.	0.	0.	0.03		
+	HYDROGRAPH AT	358B	1.	12.00	0.	0.	0.	0.01		
+	5 COMBINED AT	54C	15.	12.00	11.	10.	10.	0.17		
+	HYDROGRAPH AT	344B	8.	12.00	1.	0.	0.	0.04		
+	HYDROGRAPH AT	363B	4.	12.00	1.	0.	0.	0.02		
+	3 COMBINED AT	9C	26.	12.00	12.	11.	11.	0.23		
+	ROUTED TO	9R	26.	12.00	12.	11.	11.	0.23		

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)



ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	INTERPOLATED TO COMPUTATION INTERVAL		VOLUME	
						PEAK	TIME TO PEAK		
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
FOR STORM = 1	STORM AREA (SQ MI) =			10.00					
25R MANE	1.26	8.21	731.71	0.16	10.00	7.92	730.00	0.16	
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1336E+01 EXCESS=0.0000E+00 OUTFLOW=0.1334E+01 BASIN STORAGE=0.2259E-02 PERCENT ERROR= 0.0									
FOR STORM = 1	STORM AREA (SQ MI) =			10.00					
23R MANE	3.29	0.24	806.43	0.04	10.00	0.24	810.00	0.04	
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1403E+00 EXCESS=0.0000E+00 OUTFLOW=0.1395E+00 BASIN STORAGE=0.7757E-03 PERCENT ERROR= 0.0									
FOR STORM = 1	STORM AREA (SQ MI) =			10.00					
24R MANE	0.50	1.83	725.50	0.07	10.00	1.56	730.00	0.07	
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4467E+00 EXCESS=0.0000E+00 OUTFLOW=0.4434E+00 BASIN STORAGE=0.3500E-02 PERCENT ERROR= 0.0									
FOR STORM = 1	STORM AREA (SQ MI) =			10.00					
18R MANE	2.00	17.70	734.00	0.14	10.00	16.22	730.00	0.14	
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2969E+01 EXCESS=0.0000E+00 OUTFLOW=0.2956E+01 BASIN STORAGE=0.2097E-01 PERCENT ERROR= -0.2									

*** NORMAL END OF HEC-1 ***

50 YEAR HEC-1

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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* MAY 1991
* VERSION 4.0.1E
*
* RUN DATE TIME
*
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*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
*
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	HEC-1 Analysis using WMS									
2	ID	50 year developed flow									
3	ID	MAY 2012									
4	IT	10	07MAY09	0	130						
5	IO	5									
6	IN	6	07MAY09	0							
7	JD	2.3	10.0								
		* typeII-24hour									
8	PC	0.0	0.001	0.002	0.0031	0.0041	0.0051	0.0062	0.0073	0.0083	0.0094
9	PC	0.0105	0.0116	0.0127	0.0138	0.015	0.0161	0.0173	0.0185	0.0196	0.0208
10	PC	0.022	0.0232	0.0244	0.0256	0.0269	0.0281	0.0294	0.0307	0.0319	0.0332
11	PC	0.0345	0.0358	0.0371	0.0384	0.0398	0.0411	0.0425	0.0439	0.0452	0.0466



HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
46	KK	37R	CNAME	37C							
47	KO	0	0	0.0	0	22					
48	RS	1	FLOW	0.0	0.0						
		* 37C Volume									
49	SV	0.00.1266630.253327	0.379990.5066530.633316	0.759980.8866431.0133061.139969							
50	SV	1.26661.3932961.5199591.6466221.7732861.8999492.0266122.1532752.2799392.406602									
		* 37C Elevation									
51	SE	4742.04742.4214742.8424743.2634743.6844744.1054744.5264744.9474745.3684745.789									
52	SE	4746.24746.6314747.0524747.4734747.8944748.3154748.7364749.1574749.578	4750.0								
		* 37C Discharge									
53	SQ	0.02.197453	8.3679616.4140423.1448215.9029218.6881421.1090223.2794925.26417								
54	SQ	27.10328.8264930.4517731.9946033.4663734.8761036.2310137.5370538.7991540.02147									
		* 37C Elevation									
55	SE	4742.04742.4214742.8424743.2634743.6844744.1054744.5264744.9474745.3684745.789									
56	SE	4746.24746.6314747.0524747.4734747.8944748.3154748.7364749.1574749.578	4750.0								
57	KK	11B									
58	KO	0	0	0.0	0	22					
59	BA	0.1161									
60	LS	0.0	57.0	0.0							
61	UD	0.0767									
62	KK	6R	CNAME	6C							
63	KO	0	0	0.0	0	22					
64	RN	6R									
65	KK	10B									
66	KO	0	0	0.0	0	22					
67	BA	0.1616									
68	LS	0.0	71.74	0.0							
69	UD	0.1283									
70	KK	13C	CNAME	13R							
71	KO	0	0	0.0	0	22					
72	HC	2									
73	KK	13R	CNAME	13C							
74	KO	0	0	0.0	0	22					
75	RS	1	FLOW	0.0	0.0						
		* 13C Volume									
76	SV	0.00.9742581.9639382.969202	3.990215.0271236.0801017.1493058.2348969.337034								
77	SV	10.45511.5915912.7443313.9142715.1015516.3063517.5288218.7691220.0274121.30386									
		* 13C Elevation									
78	SE	4800.04800.5264801.0524801.5784802.1054802.6314803.1574803.6844804.2104804.736									
79	SE	4805.24805.7894806.3154806.8424807.3684807.8944808.4214808.9474809.473	4810.0								

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* 13C Discharge
80 SQ 0.03.42952912.3279421.8209515.9029219.3218222.2207724.7829127.1039229.24128
81 SQ 31.23233.1045734.8761036.5618938.1733239.7194241.2075542.6437844.0331945.38008
* 13C Elevation
82 SE 4800.04800.5264801.0524801.5784802.1054802.6314803.1574803.6844804.2104804.736
83 SE 4805.24805.7894806.3154806.6424807.3684807.8944808.4214808.9474809.473 4810.0

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
84	KK	98B									
85	KO	0	0	0.0	0	22					
86	BA	0.1097									
87	LS	0.0	64.48	0.0							
88	UD	0.0812									
89	KK	29R	CNAME	29C							
90	KO	0	0	0.0	0	22					
91	RN	29R									
92	KK	408B									
93	KO	0	0	0.0	0	22					
94	BA	0.0830									
95	LS	0.0	66.25	0.0							
96	UD	0.1008									
97	KK	99B									
98	KO	0	0	0.0	0	22					
99	BA	0.0594									
100	LS	0.0	78.61	0.0							
101	UD	0.0694									
102	KK	30C	CNAME	30R							
103	KO	0	0	0.0	0	22					
104	HC	3									
105	KK	103B									
106	KO	0	0	0.0	0	22					
107	BA	0.0102									
108	LS	0.0	84.1	0.0							
109	UD	0.1933									
110	KK	401B									
111	KO	0	0	0.0	0	22					
112	BA	0.1360									
113	LS	0.0	74.82	0.0							
114	UD	0.1917									
115	KK	32C	CNAME	32R							
116	KO	0	0	0.0	0	22					
117	HC	3									
118	KK	101B									
119	KO	0	0	0.0	0	22					
120	BA	0.1138									

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121	LS	0.0	64.94	0.0		
122	UD	0.1459				
123	KK	31R	CNAME	31C		
124	KO	0	0	0.0	0	22
125	RN	31R				

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
126	KK	83B									
127	KO	0	0	0.0	0	22					
128	BA	0.5686									
129	LS	0.0	58.07	0.0							
130	UD	0.0556									
131	KK	19R	CNAME	19C							
132	KO	0	0	0.0	0	22					
133	RN	19R									
134	KK	86B									
135	KO	0	0	0.0	0	22					
136	BA	0.0259									
137	LS	0.0	73.61	0.0							
138	UD	0.0556									
139	KK	21C	CNAME	21R							
140	KO	0	0	0.0	0	22					
141	HC	2									
142	KK	85B									
143	KO	0	0	0.0	0	22					
144	BA	0.1593									
145	LS	0.0	63.35	0.0							
146	UD	0.0556									
147	KK	16C	CNAME	16R							
148	KO	0	0	0.0	0	22					
149	HC	2									
150	KK	81B									
151	KO	0	0	0.0	0	22					
152	BA	0.1869									
153	LS	0.0	58.02	0.0							
154	UD	0.0556									
155	KK	17R	CNAME	17C							
156	KO	0	0	0.0	0	22					
157	RN	17R									
158	KK	84B									
159	KO	0	0	0.0	0	22					
160	BA	0.1198									
161	LS	0.0	67.12	0.0							
162	UD	0.0556									

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163	KK	20C	CNAME	20R		
164	KO	0	0	0.0	0	22
165	HC	3				

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
166	KK	79B									
167	KO	0	0	0.0	0	22					
168	BA	0.0165									
169	LS	0.0	68.61	0.0							
170	UD	0.0556									
171	KK	15R	CNAME	15C							
172	KO	0	0	0.0	0	22					
173	RN	15R									
174	KK	78B									
175	KO	0	0	0.0	0	22					
176	BA	0.0764									
177	LS	0.0	61.01	0.0							
178	UD	0.0556									
179	KK	8C	CNAME	8R							
180	KO	0	0	0.0	0	22					
181	HC	2									
182	KK	87B									
183	KO	0	0	0.0	0	22					
184	BA	0.0637									
185	LS	0.0	66.31	0.0							
186	UD	0.0556									
187	KK	22C	CNAME	22R							
188	KO	0	0	0.0	0	22					
189	HC	2									
190	KK	77B									
191	KO	0	0	0.0	0	22					
192	BA	0.0564									
193	LS	0.0	62.17	0.0							
194	UD	0.0556									
195	KK	7C	CNAME	7R							
196	KO	0	0	0.0	0	22					
197	HC	3									
198	KK	177B									
199	KO	0	0	0.0	0	22					
200	BA	0.0215									
201	LS	0.0	64.7	0.0							
202	UD	0.0320									

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203	KK	248B					
204	KO	0	0	0.0	0	22	
205	BA	0.0832					
206	LS	0.0	66.07	0.0			
207	UD	0.0813					

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
208	KK	176B									
209	KO	0	0	0.0	0	22					
210	BA	0.0174									
211	LS	0.0	75.39	0.0							
212	UD	0.1412									
213	KK	41C	CNAME	41R							
214	KO	0	0	0.0	0	22					
215	HC	5									
216	KK	286B									
217	KO	0	0	0.0	1	22					
218	BA	0.4184									
219	LS	0.0	70.78	0.0							
220	UD	0.0268									
221	KK	181B									
222	KO	0	0	0.0	1	22					
223	BA	0.0313									
224	LS	0.0	77.05	0.0							
225	UD	0.0991									
226	KK	43C	CNAME	43R							
227	KO	0	0	0.0	0	22					
228	HC	3									
229	KK	2B									
230	KO	0	0	0.0	1	22					
231	BA	0.0817									
232	LS	0.0	81.16	0.0							
233	UD	0.3103									
234	KK	38R	CNAME	38C							
235	KO	0	0	0.0	0	22					
236	RN	38R									
237	KK	405B									
238	KO	0	0	0.0	1	22					
239	BA	0.0092									
240	LS	0.0	80.21	0.0							
241	UD	0.0730									
242	KK	288B									
243	KO	0	0	0.0	1	22					
244	BA	0.0149									



245	IS	0.0	78.34	0.0		
246	UD	0.0664				
247	KK	44C	CNAME	44R		
248	KO	0	0	0.0	0	22
249	HC	4				

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
250	KK	415B									
251	KO	0	0	0.0	1	22					
252	BA	0.0771									
253	LS	0.0	80.26	0.0							
254	UD	0.0921									
255	KK	459B									
256	KO	0	0	0.0	1	22					
257	BA	0.1803									
258	LS	0.0	79.85	0.0							
259	UD	0.1662									
260	KK	3C	CNAME	3R							
261	KO	0	0	0.0	0	22					
262	HC	4									
263	KK	163B									
264	KO	0	0	0.0	1	22					
265	BA	0.0618									
266	LS	0.0	80.62	0.0							
267	UD	0.1138									
268	KK	7B									
269	KO	0	0	0.0	1	22					
270	BA	0.0408									
271	LS	0.0	67.23	0.0							
272	UD	0.0556									
273	KK	411B									
274	KO	0	0	0.0	1	22					
275	BA	0.0331									
276	LS	0.0	79.74	0.0							
277	UD	0.0892									
278	KK	12C	CNAME	12R							
279	KO	0	0	0.0	0	22					
280	HC	4									
281	KK	12R	CNAME	12C							
282	KO	0	0	0.0	0	22					
283	RN	12R									
284	KK	141B									
285	KO	0	0	0.0	1	22					
286	BA	0.1600									

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287	LS	0.0	69.57	0.0				
288	UD	0.1866						
289	KK	25R	CNAME	25C				
290	KO	0	0	0.0	0	22		
291	RD	1297.6	0.07153	0.013		CIRC	2.0	0.0

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
292	KK	139B									
293	KO	0	0	0.0	0	22					
294	BA	0.0660									
295	LS	0.0	61.27	0.0							
296	UD	0.0702									
297	KK	23R	CNAME	23C							
298	KO	0	0	0.0	0	22					
299	RD	1357.8	0.04276	0.013		CIRC	2.0	0.0			
300	KK	140B									
301	KO	0	0	0.0	0	22					
302	BA	0.0475									
303	LS	0.0	67.54	0.0							
304	UD	0.0616									
305	KK	24C	CNAME	24R							
306	KO	0	0	0.0	0	22					
307	HC	2									
308	KK	24R	CNAME	24C							
309	KO	0	0	0.0	0	22					
310	RD	3765.7	0.06856	0.013		CIRC	2.0	0.0			
311	KK	138B									
312	KO	0	0	0.0	0	22					
313	BA	0.1174									
314	LS	0.0	71.23	0.0							
315	UD	0.2069									
316	KK	18C	CNAME	18R							
317	KO	0	0	0.0	0	22					
318	HC	3									
319	KK	18R	CNAME	18C							
320	KO	0	0	0.0	0	22					
321	RD	3528.0	0.04879	0.013		TRAP	2.0	0.0			
322	KK	155B									
323	KO	0	0	0.0	0	22					
324	BA	0.0758									
325	LS	0.0	75.21	0.0							
326	UD	0.1458									
327	KK	149B									

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328	KO	0	0	0.0	0	22
329	BA	0.2020				
330	LS	0.0	80.17	0.0		
331	UD	0.2477				

LINE	ID	1	2	3	4	5	6	7	8	9	10
332	KK	4C	CNAME	4R							
333	KO	0	0	0.0	0	22					
334	HC	2									
335	KK	4R	CNAME	4C							
336	KO	0	0	0.0	0	22					
337	RS	1	FLOW	0.0	0.0						
		* 4C Volume									
338	SV	0.00.2728530.5501420.8319091.118195 1.409041.7044872.0045762.3093492.618846									
339	SV	2.93313.2521783.5760963.9049024.2386384.5773464.921066 5.269845.6237085.982713									
		* 4C Elevation									
340	SE	4811.04811.2104811.4214811.6314811.8424812.0524812.2634812.4734812.6844812.894									
341	SE	4813.14813.3154813.5264813.7364813.9474814.1574814.3684814.5784814.789 4815.0									
		* 4C Discharge									
342	SQ	12.76313.3469013.9061714.4438114.9621415.4631015.9483316.4192316.8770017.32267									
343	SQ	17.75718.1812818.7378822.8393729.3622537.5566847.1173257.86315 69.670582.44792									
		* 4C Elevation									
344	SE	4811.04811.2104811.4214811.6314811.8424812.0524812.2634812.4734812.6844812.894									
345	SE	4813.14813.3154813.5264813.7364813.9474814.1574814.3684814.5784814.789 4815.0									
346	KK	30B									
347	KO	0	0	0.0	0	22					
348	BA	0.1491									
349	LS	0.0	74.12	0.0							
350	UD	0.2306									
351	KK	66B									
352	KO	0	0	0.0	0	22					
353	BA	0.0522									
354	LS	0.0	72.0	0.0							
355	UD	0.0556									
356	KK	11C	CNAME	11R							
357	KO	0	0	0.0	0	22					
358	HC	4									
359	KK	11R	CNAME	11C							
360	KO	0	0	0.0	0	22					
361	RN	11R									
362	KK	241B									
363	KO	0	0	0.0	0	22					
364	BA	0.0949									
365	LS	0.0	73.24	0.0							
366	UD	0.1459									

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367	KK	10R	CNAME	10C		
368	KO	0	0	0.0	0	22
369	RN	10R				

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
370	KK	151B									
371	KO	0	0	0.0	0	22					
372	BA	0.0132									
373	LS	0.0	72.23	0.0							
374	UD	0.0337									
375	KK	150B									
376	KO	0	0	0.0	0	22					
377	BA	0.0461									
378	LS	0.0	79.46	0.0							
379	UD	0.0407									
380	KK	35C	CNAME	35R							
381	KO	0	0	0.0	0	22					
382	HC	2									
383	KK	35R	CNAME	35C							
384	KO	0	0	0.0	0	22					
385	RS	1	FLOW	0.0	0.0						
		* 35C Volume									
386	SV	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0
		* 35C Elevation									
387	SE	4815.0	4816.0	4817.0	4818.0	4819.0	4820.0	4821.0	4822.0	4823.0	4824.0
		* 35C Discharge									
388	SQ	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0
		* 35C Elevation									
389	SE	4815.0	4816.0	4817.0	4818.0	4819.0	4820.0	4821.0	4822.0	4823.0	4824.0
390	KK	143B									
391	KO	0	0	0.0	0	22					
392	BA	0.0414									
393	LS	0.0	74.0	0.0							
394	UD	0.0120									
395	KK	402B									
396	KO	0	0	0.0	0	22					
397	BA	0.0153									
398	LS	0.0	74.0	0.0							
399	UD	0.0514									
400	KK	33C	CNAME	33R							
401	KO	0	0	0.0	0	22					
402	HC	2									
403	KK	33R	CNAME	33C							

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404	KO	0	0	0.0	0	22						
405	RS	1	FLOW	0.0	0.0							
	* 33C Volume											
406	SV	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	
	* 33C Elevation											
407	SE	4810.0	4811.0	4812.0	4813.0	4814.0	4815.0	4816.0	4817.0	4818.0	4819.0	
	* 33C Discharge											
408	SQ	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	
	* 33C Elevation											

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
409	SE	4810.0	4811.0	4812.0	4813.0	4814.0	4815.0	4816.0	4817.0	4818.0	4819.0
410	KK	407B									
411	KO	0	0	0.0	0	22					
412	BA	0.0182									
413	LS	0.0	74.0	0.0							
414	UD	0.0532									
415	KK	406B									
416	KO	0	0	0.0	0	22					
417	BA	0.0256									
418	LS	0.0	68.46	0.0							
419	UD	0.0717									
420	KK	358B									
421	KO	0	0	0.0	0	22					
422	BA	0.0053									
423	LS	0.0	72.0	0.0							
424	UD	0.0822									
425	KK	54C	CNAME	54R							
426	KO	0	0	0.0	0	22					
427	HC	5									
428	KK	344B									
429	KO	0	0	0.0	0	22					
430	BA	0.0449									
431	LS	0.0	73.99	0.0							
432	UD	0.0895									
433	KK	363B									
434	KO	0	0	0.0	0	22					
435	BA	0.0208									
436	LS	0.0	75.76	0.0							
437	UD	0.1262									
438	KK	9C	CNAME	9R							
439	KO	0	0	0.0	0	22					
440	HC	3									
441	KK	9R	CNAME	9C							
442	KO	0	0	0.0	0	22					
443	RN	9R									
444	ZZ										

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+		30C	57.	12.00	8.	3.	3.	0.25
	HYDROGRAPH AT							
+		103B	6.	12.17	1.	0.	0.	0.01
	HYDROGRAPH AT							
+		401B	39.	12.17	7.	2.	2.	0.14
	3 COMBINED AT							
+		32C	96.	12.00	15.	5.	5.	0.40
	HYDROGRAPH AT							
+		101B	9.	12.17	2.	1.	1.	0.11
	ROUTED TO							
+		31R	9.	12.17	2.	1.	1.	0.11
	HYDROGRAPH AT							
+		83B	7.	12.33	4.	2.	2.	0.57
	ROUTED TO							
+		19R	7.	12.33	4.	2.	2.	0.57
	HYDROGRAPH AT							
+		86B	10.	12.00	1.	0.	0.	0.03
	2 COMBINED AT							
+		21C	13.	12.00	5.	2.	2.	0.59
	HYDROGRAPH AT							
+		85B	13.	12.00	3.	1.	1.	0.16
	2 COMBINED AT							
+		16C	26.	12.00	8.	3.	3.	0.75
	HYDROGRAPH AT							
+		81B	2.	12.33	1.	1.	1.	0.19
	ROUTED TO							
+		17R	2.	12.33	1.	1.	1.	0.19
	HYDROGRAPH AT							
+		84B	21.	12.00	3.	1.	1.	0.12
	3 COMBINED AT							
+		20C	48.	12.00	12.	4.	4.	1.06
	HYDROGRAPH AT							
+		79B	4.	12.00	0.	0.	0.	0.02

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+	ROUTED TO	15R	4.	12.00	0.	0.	0.	0.02
+	HYDROGRAPH AT	78B	3.	12.00	1.	0.	0.	0.08
+	2 COMBINED AT	8C	6.	12.00	1.	0.	0.	0.09
+	HYDROGRAPH AT	87B	10.	12.00	1.	0.	0.	0.06
+	2 COMBINED AT	22C	16.	12.00	3.	1.	1.	0.16
+	HYDROGRAPH AT	77B	3.	12.00	1.	0.	0.	0.06
+	3 COMBINED AT	7C	67.	12.00	16.	6.	6.	1.27
+	HYDROGRAPH AT	177B	2.	12.00	0.	0.	0.	0.02
+	HYDROGRAPH AT	248B	12.	12.00	2.	1.	1.	0.08
+	HYDROGRAPH AT	176B	6.	12.00	1.	0.	0.	0.02
+	5 COMBINED AT	41C	96.	12.00	21.	7.	7.	1.51
+	HYDROGRAPH AT	286B	119.	12.00	15.	5.	5.	0.42
+	HYDROGRAPH AT	181B	15.	12.00	2.	1.	1.	0.03
+	3 COMBINED AT	43C	230.	12.00	37.	13.	13.	1.96
+	HYDROGRAPH AT	2B	32.	12.17	6.	2.	2.	0.08
+	ROUTED TO	38R	32.	12.17	6.	2.	2.	0.08
+	HYDROGRAPH AT	405B	6.	12.00	1.	0.	0.	0.01

+	HYDROGRAPH AT	288B	8.	12.00	1.	0.	0.	0.01
+	4 COMBINED AT	44C	265.	12.00	45.	15.	15.	2.06
+	HYDROGRAPH AT	415B	49.	12.00	5.	2.	2.	0.08
+	HYDROGRAPH AT	459B	80.	12.00	12.	4.	4.	0.18
+	4 COMBINED AT	3C	489.	12.00	78.	26.	26.	2.72
+	HYDROGRAPH AT	163B	37.	12.00	4.	1.	1.	0.06
+	HYDROGRAPH AT	7B	7.	12.00	1.	0.	0.	0.04
+	HYDROGRAPH AT	411B	20.	12.00	2.	1.	1.	0.03
+	4 COMBINED AT	12C	553.	12.00	86.	29.	29.	2.86
+	ROUTED TO	12R	553.	12.00	86.	29.	29.	2.86
+	HYDROGRAPH AT	141B	26.	12.17	5.	2.	2.	0.16
+	ROUTED TO	25R	26.	12.17	5.	2.	2.	0.16
+	HYDROGRAPH AT	139B	3.	12.00	1.	0.	0.	0.07
+	ROUTED TO	23R	2.	12.17	1.	0.	0.	0.07
+	HYDROGRAPH AT	140B	9.	12.00	1.	0.	0.	0.05
+	2 COMBINED AT	24C	11.	12.00	2.	1.	1.	0.11
+	ROUTED TO							

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+		24R	8.	12.17	2.	1.	1.	0.11		
	HYDROGRAPH AT									
+		138B	23.	12.17	4.	1.	1.	0.12		
	3 COMBINED AT									
+		18C	57.	12.17	11.	4.	4.	0.39		
	ROUTED TO									
+		18R	55.	12.17	11.	4.	4.	0.39		
	HYDROGRAPH AT									
+		155B	25.	12.00	4.	1.	1.	0.08		
	HYDROGRAPH AT									
+		149B	85.	12.17	14.	5.	5.	0.20		
	2 COMBINED AT									
+		4C	106.	12.17	18.	6.	6.	0.28		
	ROUTED TO									
+		4R	21.	13.00	17.	14.	14.	0.28		
+									4813.64	13.00
	HYDROGRAPH AT									
+		30B	38.	12.17	7.	2.	2.	0.15		
	HYDROGRAPH AT									
+		66B	17.	12.00	2.	1.	1.	0.05		
	4 COMBINED AT									
+		11C	117.	12.17	37.	21.	21.	0.87		
	ROUTED TO									
+		11R	117.	12.17	37.	21.	21.	0.87		
	HYDROGRAPH AT									
+		241B	25.	12.00	4.	1.	1.	0.09		
	ROUTED TO									
+		10R	25.	12.00	4.	1.	1.	0.09		
	HYDROGRAPH AT									
+		151B	4.	12.00	1.	0.	0.	0.01		
	HYDROGRAPH AT									
+		150B	28.	12.00	3.	1.	1.	0.05		
	2 COMBINED AT									
+		35C	33.	12.00	4.	1.	1.	0.06		

+	ROUTED TO	35R	5.	0.17	5.	5.	5.	0.06	4815.00	0.00
+	HYDROGRAPH AT	143B	16.	12.00	2.	1.	1.	0.04		
+	HYDROGRAPH AT	402B	6.	12.00	1.	0.	0.	0.02		
+	2 COMBINED AT	33C	23.	12.00	3.	1.	1.	0.06		
+	ROUTED TO	33R	5.	0.17	5.	5.	5.	0.06	4810.30	12.50
+	HYDROGRAPH AT	407B	7.	12.00	1.	0.	0.	0.02		
+	HYDROGRAPH AT	406B	5.	12.00	1.	0.	0.	0.03		
+	HYDROGRAPH AT	358B	2.	12.00	0.	0.	0.	0.01		
+	5 COMBINED AT	54C	24.	12.00	12.	11.	11.	0.17		
+	HYDROGRAPH AT	344B	17.	12.00	2.	1.	1.	0.04		
+	HYDROGRAPH AT	363B	8.	12.00	1.	0.	0.	0.02		
+	3 COMBINED AT	9C	50.	12.00	15.	12.	12.	0.23		
+	ROUTED TO	9R	50.	12.00	15.	12.	12.	0.23		

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

INTERPOLATED TO
COMPUTATION INTERVAL

STAG	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	PEAK	TIME TO PEAK	VOLUME
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)

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FOR STORM = 1 STORM AREA (SQ MI) = 10.00
25R MANE 1.00 25.99 730.49 0.35 10.00 25.72 730.00 0.35

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2960E+01 EXCESS=0.0000E+00 OUTFLOW=0.2957E+01 BASIN STORAGE=0.3543E-02 PERCENT ERROR= 0.0

FOR STORM = 1 STORM AREA (SQ MI) = 10.00
23R MANE 0.50 2.68 722.00 0.14 10.00 2.21 730.00 0.14

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5098E+00 EXCESS=0.0000E+00 OUTFLOW=0.5084E+00 BASIN STORAGE=0.1490E-02 PERCENT ERROR= 0.0

FOR STORM = 1 STORM AREA (SQ MI) = 10.00
24R MANE 1.00 10.99 724.00 0.20 10.00 8.20 730.00 0.21

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1245E+01 EXCESS=0.0000E+00 OUTFLOW=0.1240E+01 BASIN STORAGE=0.6146E-02 PERCENT ERROR= 0.0

FOR STORM = 1 STORM AREA (SQ MI) = 10.00
18R MANE 1.50 56.03 732.00 0.32 10.00 54.90 730.00 0.32

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.6707E+01 EXCESS=0.0000E+00 OUTFLOW=0.6693E+01 BASIN STORAGE=0.2973E-01 PERCENT ERROR= -0.2

*** NORMAL END OF HEC-1 ***

100 YEAR HEC-1

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LEHI CITY



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1*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* MAY 1991
* VERSION 4.0.1E
*
* RUN DATE TIME
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
*
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	HEC-1 Analysis using WMS									
2	ID	100 year developed flow									
3	ID	MAY 2012									
4	IT	10	07MAY09	0	130						
5	IO	5									
6	IN	6	07MAY09	0							
	JD	2.52	10.0								
	* typeII-24hour										
PC	0.0	0.001	0.002	0.0031	0.0041	0.0051	0.0062	0.0073	0.0083	0.0094	
PC	0.0105	0.0116	0.0127	0.0138	0.015	0.0161	0.0173	0.0185	0.0196	0.0208	
PC	0.022	0.0232	0.0244	0.0256	0.0269	0.0281	0.0294	0.0307	0.0319	0.0332	
PC	0.0345	0.0358	0.0371	0.0384	0.0398	0.0411	0.0425	0.0439	0.0452	0.0466	
PC	0.048	0.0494	0.0508	0.0523	0.0538	0.0553	0.0568	0.0583	0.0598	0.0614	
PC	0.063	0.0646	0.0662	0.0679	0.0696	0.0712	0.073	0.0747	0.0764	0.0782	
PC	0.08	0.0818	0.0836	0.0855	0.0874	0.0892	0.0912	0.0931	0.095	0.097	
PC	0.099	0.101	0.103	0.1051	0.1072	0.1093	0.1114	0.1135	0.1156	0.1178	
PC	0.12	0.1223	0.1246	0.1271	0.1296	0.1323	0.135	0.1379	0.1408	0.1439	
PC	0.147	0.1502	0.1534	0.1566	0.1598	0.163	0.1663	0.1697	0.1733	0.1771	
PC	0.181	0.1851	0.1895	0.1941	0.1989	0.204	0.2094	0.2152	0.2214	0.228	
PC	0.235	0.2427	0.2513	0.2609	0.2715	0.283	0.3068	0.3544	0.4308	0.5679	
PC	0.663	0.682	0.6986	0.713	0.7252	0.735	0.7434	0.7514	0.7588	0.7656	

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

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46 KK      37R  CNAME      37C
47 KO        0      0.0      0      22
48 RS        1  FLOW      0.0      0.0
* 37C Volume
49 SV      0.00.1266630.253327 0.379990.5066530.633316 0.759980.8866431.0133061.139969
50 SV      1.26661.3932961.5199591.6466221.7732861.8999492.0266122.1532752.2799392.406602
* 37C Elevation
51 SE      4742.04742.4214742.8424743.2634743.6844744.1054744.5264744.9474745.3684745.789
52 SE      4746.24746.6314747.0524747.4734747.8944748.3154748.7364749.1574749.578 4750.0
* 37C Discharge
53 SQ      0.02.197453 8.3679616.4140423.1448215.9029218.6881421.1090223.2794925.26417
54 SQ      27.10328.8264930.4517731.9946033.4663734.8761036.2310137.5370538.7991540.02147
* 37C Elevation
55 SE      4742.04742.4214742.8424743.2634743.6844744.1054744.5264744.9474745.3684745.789
56 SE      4746.24746.6314747.0524747.4734747.8944748.3154748.7364749.1574749.578 4750.0

57 KK      11B
58 KO        0      0      0.0      0      22
59 BA      0.1161
60 LS        0.0      57.0      0.0
61 UD      0.0767

62 KK      6R  CNAME      6C
63 KO        0      0      0.0      0      22
64 RN        6R

65 KK      10B
66 KO        0      0      0.0      0      22
67 BA      0.1616
68 LS        0.0      71.74      0.0
69 UD      0.1283

70 KK      13C  CNAME      13R
71 KO        0      0      0.0      0      22
72 HC        2

73 KK      13R  CNAME      13C
74 KO        0      0      0.0      0      22
75 RS        1  FLOW      0.0      0.0
* 13C Volume
SV      0.00.9742581.9639382.969202 3.990215.0271236.0801017.1493058.2348969.337034
SV      10.45511.5915912.7443313.9142715.1015516.3063517.5288218.7691220.0274121.30386
* 13C Elevation
SE      4800.04800.5264801.0524801.5784802.1054802.6314803.1574803.6844804.2104804.736
SE      4805.24805.7894806.3154806.8424807.3684807.8944808.4214808.9474809.473 4810.0
* 13C Discharge
SQ      0.03.42952912.3279421.8209515.9029219.3218222.2207724.7829127.1039229.24128
SQ      31.23233.1045734.8761036.5618938.1733239.7194241.2075542.6437844.0331945.38008
* 13C Elevation
SE      4800.04800.5264801.0524801.5784802.1054802.6314803.1574803.6844804.2104804.736
SE      4805.24805.7894806.3154806.8424807.3684807.8944808.4214808.9474809.473 4810.0

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

126	KK	83B							
127	KO	0	0	0.0	0	22			
128	BA	0.5686							
129	LS	0.0	58.07	0.0					
130	UD	0.0556							

131	KK	19R	CNAME	19C					
132	KO	0	0	0.0	0	22			
133	RN	19R							

134	KK	86B							
135	KO	0	0	0.0	0	22			
136	BA	0.0259							
137	LS	0.0	73.61	0.0					
138	UD	0.0556							

139	KK	21C	CNAME	21R					
140	KO	0	0	0.0	0	22			
141	HC	2							

142	KK	85B							
143	KO	0	0	0.0	0	22			
144	BA	0.1593							
145	LS	0.0	63.35	0.0					
146	UD	0.0556							

147	KK	16C	CNAME	16R					
148	KO	0	0	0.0	0	22			
149	HC	2							

150	KK	81B							
151	KO	0	0	0.0	0	22			
152	BA	0.1869							
153	LS	0.0	58.02	0.0					
154	UD	0.0556							

155	KK	17R	CNAME	17C					
156	KO	0	0	0.0	0	22			
157	RN	17R							

158	KK	84B							
159	KO	0	0	0.0	0	22			
160	BA	0.1198							
161	LS	0.0	67.12	0.0					
162	UD	0.0556							

163	KK	20C	CNAME	20R					
164	KO	0	0	0.0	0	22			
165	HC	3							

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

208	KK	176B							
209	KO	0	0	0.0	0	22			
210	BA	0.0174							
211	LS	0.0	75.39	0.0					
212	UD	0.1412							
213	KK	41C	CNAME	41R					
214	KO	0	0	0.0	0	22			
215	HC	5							
216	KK	286B							
217	KO	0	0	0.0	1	22			
218	BA	0.4184							
219	LS	0.0	70.78	0.0					
220	UD	0.0268							
221	KK	181B							
222	KO	0	0	0.0	1	22			
223	BA	0.0313							
224	LS	0.0	77.05	0.0					
225	UD	0.0991							
226	KK	43C	CNAME	43R					
227	KO	0	0	0.0	0	22			
228	HC	3							
229	KK	2B							
230	KO	0	0	0.0	1	22			
231	BA	0.0817							
232	LS	0.0	81.16	0.0					
233	UD	0.3103							
234	KK	38R	CNAME	38C					
235	KO	0	0	0.0	0	22			
236	RN	38R							
237	KK	405B							
238	KO	0	0	0.0	1	22			
239	BA	0.0092							
240	LS	0.0	80.21	0.0					
241	UD	0.0730							
242	KK	288B							
243	KO	0	0	0.0	1	22			
244	BA	0.0149							
245	LS	0.0	78.34	0.0					
246	UD	0.0664							
247	KK	44C	CNAME	44R					
248	KO	0	0	0.0	0	22			
249	HC	4							

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LINE	ID	1	2	3	4	5	6	7	8	9	10
250	KK	415B									
251	KO	0	0	0.0	1	22					
252	BA	0.0771									
253	LS	0.0	80.26	0.0							
254	UD	0.0921									
255	KK	459B									
256	KO	0	0	0.0	1	22					
257	BA	0.1803									
258	LS	0.0	79.85	0.0							
259	UD	0.1662									
260	KK	3C	CNAME	3R							
261	KO	0	0	0.0	0	22					
262	HC	4									
263	KK	163B									
264	KO	0	0	0.0	1	22					
265	BA	0.0618									
266	LS	0.0	80.62	0.0							
267	UD	0.1138									
268	KK	7B									
269	KO	0	0	0.0	1	22					
270	BA	0.0408									
271	LS	0.0	67.23	0.0							
272	UD	0.0556									
273	KK	411B									
274	KO	0	0	0.0	1	22					
275	BA	0.0331									
276	LS	0.0	79.74	0.0							
277	UD	0.0892									
278	KK	12C	CNAME	12R							
279	KO	0	0	0.0	0	22					
280	HC	4									
281	KK	12R	CNAME	12C							
282	KO	0	0	0.0	0	22					
283	RN	12R									
284	KK	141B									
285	KO	0	0	0.0	1	22					
286	BA	0.1600									
287	LS	0.0	69.57	0.0							
288	UD	0.1866									
289	KK	25R	CNAME	25C							
290	KO	0	0	0.0	0	22					
291	RD	1297.6	0.07153	0.013		CIRC	2.0	0.0			

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

292	KK	139B							
293	KO	0	0	0.0	0	22			
294	BA	0.0660							
295	LS	0.0	61.27	0.0					
296	UD	0.0702							
297	KK	23R	CNAME	23C					
298	KO	0	0	0.0	0	22			
299	RD	1357.8	0.04276	0.013		CIRC	2.0	0.0	
300	KK	140B							
301	KO	0	0	0.0	0	22			
302	BA	0.0475							
303	LS	0.0	67.54	0.0					
304	UD	0.0616							
305	KK	24C	CNAME	24R					
306	KO	0	0	0.0	0	22			
307	HC	2							
308	KK	24R	CNAME	24C					
309	KO	0	0	0.0	0	22			
310	RD	3765.7	0.06856	0.013		CIRC	2.0	0.0	
311	KK	138B							
312	KO	0	0	0.0	0	22			
313	BA	0.1174							
314	LS	0.0	71.23	0.0					
315	UD	0.2069							
316	KK	18C	CNAME	18R					
317	KO	0	0	0.0	0	22			
318	HC	3							
319	KK	18R	CNAME	18C					
320	KO	0	0	0.0	0	22			
321	RD	3528.0	0.04879	0.013		TRAP	2.0	0.0	
322	KK	155B							
323	KO	0	0	0.0	0	22			
324	BA	0.0758							
325	LS	0.0	75.21	0.0					
326	UD	0.1458							
327	KK	149B							
328	KO	0	0	0.0	0	22			
329	BA	0.2020							
330	LS	0.0	80.17	0.0					
331	UD	0.2477							

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LINE	ID	1	2	3	4	5	6	7	8	9	10
370	KK	151B									
371	KO	0	0	0.0	0	22					
372	BA	0.0132									
373	LS	0.0	72.23	0.0							
374	UD	0.0337									
375	KK	150B									
376	KO	0	0	0.0	0	22					
377	BA	0.0461									
378	LS	0.0	79.46	0.0							
379	UD	0.0407									
380	KK	35C	CNAME	35R							
381	KO	0	0	0.0	0	22					
382	HC	2									
383	KK	35R	CNAME	35C							
384	KO	0	0	0.0	0	22					
385	RS	1	FLOW	0.0	0.0						
		* 35C Volume									
386	SV	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0
		* 35C Elevation									
387	SE	4815.0	4816.0	4817.0	4818.0	4819.0	4820.0	4821.0	4822.0	4823.0	4824.0
		* 35C Discharge									
388	SQ	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0
		* 35C Elevation									
389	SE	4815.0	4816.0	4817.0	4818.0	4819.0	4820.0	4821.0	4822.0	4823.0	4824.0
390	KK	143B									
391	KO	0	0	0.0	0	22					
392	BA	0.0414									
393	LS	0.0	74.0	0.0							
394	UD	0.0120									
395	KK	402B									
396	KO	0	0	0.0	0	22					
397	BA	0.0153									
398	LS	0.0	74.0	0.0							
399	UD	0.0514									
400	KK	33C	CNAME	33R							
401	KO	0	0	0.0	0	22					
402	HC	2									
403	KK	33R	CNAME	33C							
404	KO	0	0	0.0	0	22					
405	RS	1	FLOW	0.0	0.0						
		* 33C Volume									
406	SV	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0
		* 33C Elevation									
407	SE	4810.0	4811.0	4812.0	4813.0	4814.0	4815.0	4816.0	4817.0	4818.0	4819.0
		* 33C Discharge									
408	SQ	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0
		* 33C Elevation									

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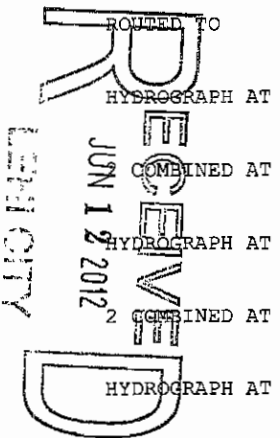


HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
409	SE	4810.0	4811.0	4812.0	4813.0	4814.0	4815.0	4816.0	4817.0	4818.0	4819.0
410	KK	407B									
411	KO	0	0	0.0	0	22					
412	BA	0.0182									
413	LS	0.0	74.0	0.0							
414	UD	0.0532									
415	KK	406B									
416	KO	0	0	0.0	0	22					
417	BA	0.0256									
418	LS	0.0	68.46	0.0							
419	UD	0.0717									
420	KK	358B									
421	KO	0	0	0.0	0	22					
422	BA	0.0053									
423	LS	0.0	72.0	0.0							
424	UD	0.0822									
425	KK	54C	CNAME	54R							
426	KO	0	0	0.0	0	22					
427	HC	5									
428	KK	344B									
429	KO	0	0	0.0	0	22					
430	BA	0.0449									
431	LS	0.0	73.99	0.0							
432	UD	0.0895									
433	KK	363B									
434	KO	0	0	0.0	0	22					
435	BA	0.0208									
436	LS	0.0	75.76	0.0							
437	UD	0.1262									
438	KK	9C	CNAME	9R							
439	KO	0	0	0.0	0	22					
440	HC	3									
441	KK	9R	CNAME	9C							
442	KO	0	0	0.0	0	22					
443	RN	9R									
444	ZZ										

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+		32C	128.	12.00	19.	6.	6.	0.40
+	HYDROGRAPH AT							
+		101B	14.	12.17	3.	1.	1.	0.11
+	ROUTED TO							
+		31R	14.	12.17	3.	1.	1.	0.11
+	HYDROGRAPH AT							
+		83B	17.	12.00	7.	2.	2.	0.57
+	ROUTED TO							
+		19R	17.	12.00	7.	2.	2.	0.57
+	HYDROGRAPH AT							
+		86B	13.	12.00	1.	0.	0.	0.03
+	2 COMBINED AT							
+		21C	29.	12.00	8.	3.	3.	0.59
+	HYDROGRAPH AT							
+		85B	23.	12.00	4.	1.	1.	0.16
+	2 COMBINED AT							
+		16C	52.	12.00	12.	4.	4.	0.75
+	HYDROGRAPH AT							
+		81B	5.	12.00	2.	1.	1.	0.19
+	ROUTED TO							
+		17R	5.	12.00	2.	1.	1.	0.19
+	HYDROGRAPH AT							
+		84B	30.	12.00	4.	1.	1.	0.12
+	3 COMBINED AT							
+		20C	88.	12.00	18.	6.	6.	1.06
+	HYDROGRAPH AT							
+		79B	5.	12.00	1.	0.	0.	0.02
+	ROUTED TO							
+		15R	5.	12.00	1.	0.	0.	0.02
+	HYDROGRAPH AT							
+		78B	6.	12.00	1.	0.	0.	0.08
+	COMBINED AT							
+		8C	11.	12.00	2.	1.	1.	0.09
+	HYDROGRAPH AT							
+		87B	15.	12.00	2.	1.	1.	0.06
+	2 COMBINED AT							
+		22C	26.	12.00	4.	1.	1.	0.16
+	HYDROGRAPH AT							
+		77B	6.	12.00	1.	0.	0.	0.06

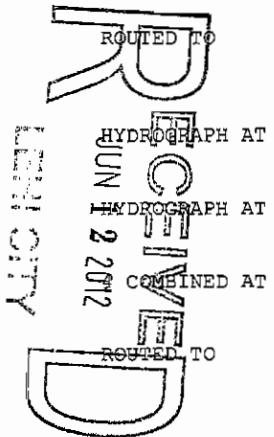


+	3 COMBINED AT	7C	120.	12.00	23.	8.	8.	1.27
	HYDROGRAPH AT							
+		177B	4.	12.00	1.	0.	0.	0.02
	HYDROGRAPH AT							
+		248B	18.	12.00	2.	1.	1.	0.08
	HYDROGRAPH AT							
+		176B	8.	12.00	1.	0.	0.	0.02
	5 COMBINED AT							
+		41C	163.	12.00	30.	10.	10.	1.51
	HYDROGRAPH AT							
+		286B	160.	12.00	19.	6.	6.	0.42
	HYDROGRAPH AT							
+		181B	19.	12.00	2.	1.	1.	0.03
	3 COMBINED AT							
+		43C	341.	12.00	51.	17.	17.	1.96
	HYDROGRAPH AT							
+		2B	39.	12.17	7.	2.	2.	0.08
	ROUTED TO							
+		38R	39.	12.17	7.	2.	2.	0.08
	HYDROGRAPH AT							
+		405B	7.	12.00	1.	0.	0.	0.01
	HYDROGRAPH AT							
+		288B	10.	12.00	1.	0.	0.	0.01
	4 COMBINED AT							
+		44C	384.	12.00	60.	20.	20.	2.06
	HYDROGRAPH AT							
+		415B	59.	12.00	7.	2.	2.	0.08
	HYDROGRAPH AT							
+		459B	98.	12.00	15.	5.	5.	0.18
	4 COMBINED AT							
+		3C	668.	12.00	100.	33.	33.	2.72
	HYDROGRAPH AT							
+		163B	44.	12.00	5.	2.	2.	0.06
	HYDROGRAPH AT							
+		7B	10.	12.00	1.	0.	0.	0.04
	HYDROGRAPH AT							
+		411B	25.	12.00	3.	1.	1.	0.03
	4 COMBINED AT							
+		12C	747.	12.00	110.	36.	36.	2.86

+	ROUTED TO	12R	747.	12.00	110.	36.	36.	2.86		
+	HYDROGRAPH AT	141B	36.	12.17	6.	2.	2.	0.16		
+	ROUTED TO	25R	35.	12.17	6.	2.	2.	0.16		
+	HYDROGRAPH AT	139B	6.	12.00	1.	0.	0.	0.07		
+	ROUTED TO	23R	5.	12.00	1.	0.	0.	0.07		
+	HYDROGRAPH AT	140B	13.	12.00	2.	1.	1.	0.05		
+	2 COMBINED AT	24C	18.	12.00	3.	1.	1.	0.11		
+	ROUTED TO	24R	13.	12.00	3.	1.	1.	0.11		
+	HYDROGRAPH AT	138B	31.	12.17	5.	2.	2.	0.12		
+	3 COMBINED AT	18C	79.	12.17	15.	5.	5.	0.39		
+	ROUTED TO	18R	77.	12.17	15.	5.	5.	0.39		
+	HYDROGRAPH AT	155B	32.	12.00	5.	2.	2.	0.08		
+	HYDROGRAPH AT	149B	103.	12.17	17.	5.	5.	0.20		
+	2 COMBINED AT	4C	129.	12.17	22.	7.	7.	0.28		
+	ROUTED TO	4R	35.	12.67	20.	15.	15.	0.28	4814.08	12.67
+	HYDROGRAPH AT	30B	49.	12.17	9.	3.	3.	0.15		
+	HYDROGRAPH AT	66B	22.	12.00	3.	1.	1.	0.05		
+	COMBINED AT	11C	154.	12.17	45.	23.	23.	0.87		
+	ROUTED TO	11R	154.	12.17	45.	23.	23.	0.87		

4814.08

12.67



+	HYDROGRAPH AT	241B	33.	12.00	5.	2.	2.	0.09		
	ROUTED TO									
+		10R	33.	12.00	5.	2.	2.	0.09		
+	HYDROGRAPH AT	151B	6.	12.00	1.	0.	0.	0.01		
+	HYDROGRAPH AT	150B	34.	12.00	4.	1.	1.	0.05		
+	2 COMBINED AT	35C	40.	12.00	4.	1.	1.	0.06		
+	ROUTED TO	35R	5.	0.17	5.	5.	5.	0.06		
+									4815.00	0.00
+	HYDROGRAPH AT	143B	21.	12.00	2.	1.	1.	0.04		
+	HYDROGRAPH AT	402B	8.	12.00	1.	0.	0.	0.02		
+	2 COMBINED AT	33C	29.	12.00	3.	1.	1.	0.06		
+	ROUTED TO	33R	5.	0.17	5.	5.	5.	0.06		
+									4810.49	12.50
+	HYDROGRAPH AT	407B	9.	12.00	1.	0.	0.	0.02		
+	HYDROGRAPH AT	406B	8.	12.00	1.	0.	0.	0.03		
+	HYDROGRAPH AT	358B	2.	12.00	0.	0.	0.	0.01		
+	5 COMBINED AT	54C	29.	12.00	12.	11.	11.	0.17		
+	HYDROGRAPH AT	344B	22.	12.00	3.	1.	1.	0.04		
+	HYDROGRAPH AT	363B	10.	12.00	1.	0.	0.	0.02		
+	3 COMBINED AT	9C	61.	12.00	16.	12.	12.	0.23		
+	ROUTED TO	9R	61.	12.00	16.	12.	12.	0.23		

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SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)
INTERPOLATED TO

ISTAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	DT (MIN)	COMPUTATION PEAK (CFS)	INTERVAL TIME TO PEAK (MIN)	VOLUME (IN)
FOR STORM = 1	STORM AREA (SQ MI) =			10.00					
25R	MANE	0.94	35.56	730.30	0.45	10.00	35.38	730.00	0.45

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3804E+01 EXCESS=0.0000E+00 OUTFLOW=0.3801E+01 BASIN STORAGE=0.4098E-02 PERCENT ERROR= 0.0

FOR STORM = 1	STORM AREA (SQ MI) =			10.00					
23R	MANE	0.50	5.82	722.00	0.21	10.00	4.93	720.00	0.21

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.7282E+00 EXCESS=0.0000E+00 OUTFLOW=0.7265E+00 BASIN STORAGE=0.1807E-02 PERCENT ERROR= 0.0

FOR STORM = 1	STORM AREA (SQ MI) =			10.00					
24R	MANE	1.00	17.38	723.00	0.28	10.00	12.90	720.00	0.28

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1692E+01 EXCESS=0.0000E+00 OUTFLOW=0.1686E+01 BASIN STORAGE=0.7309E-02 PERCENT ERROR= 0.0

FOR STORM = 1	STORM AREA (SQ MI) =			10.00					
18R	MANE	1.54	77.93	731.22	0.41	10.00	76.86	730.00	0.42

CONTINUITY SUMMARY (AC-FT) - INFLOW=0.8656E+01 EXCESS=0.0000E+00 OUTFLOW=0.8640E+01 BASIN STORAGE=0.3327E-01 PERCENT ERROR= -0.2

*** NORMAL END OF HEC-1 ***

RECEIVED
 JUN 12 2012
 LHM CITY

