

TRAVERSE MOUNTAIN AREA PLAN STORM DRAIN



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TRAVERSE MOUNTAIN AREA PLAN

STORM DRAIN

12 June 2012

The Traverse Mountain development is comprised of two main drainage areas. These areas, as shown in Figure One, consist of the Fox Hollow Drainage and the SR-92 Drainage. The Fox Hollow Drainage flows westerly to an existing 60" culvert under I-15. The culvert has been extended and an energy dissipater constructed in the Jordan Narrows Regional Drainage Facility. The SR-92 Drainage flows westerly and southerly to a recently constructed 72" outfall storm drain for the Timpanogos Highway. The outfall terminal is the Jordan Narrows Facility.

Outfall Drainage

The drainage from the SR-92 basin discharges into the 72" storm drain. Traverse Mountain's by agreement between UDOT and Lehi City has the ability to connect to this storm drain and discharge at specified flow rates. Traverse Mountain participated in the project to construct the Jordan Narrows Regional Detention Facility at the end of the 72" SR-92 outfall line. By the agreement, Traverse Mountain has 8.1 acre feet of capacity in the 17.1 acre feet constructed in the first phase. This allows them to transfer the existing Pond "A" facility offsite. Traverse Mountain also has the right to construct a second pond consisting of an additional 20 acre feet at the same location. Traverse Mountain will have to disconnect the existing pond "A" detention and connect it to the 72" storm drain at the Adobe Way location. The existing 36" storm drain in Adobe Way will need to be connected to the existing Bull River Ditch crossing of I-15 which connects to the 36" storm drain in the west frontage road.

Drainage Analysis

The concept plan was modeled in WMS software using a hec-1 model to estimate drainage flow for the development. The rainfall data used is provided in the appendix. A rainfall depth of 2.52 inches for the 100 year event, 2.30 inches for the 50 year event and 1.79 inches for the 10 year event were used in the modeling.

The estimated peak flows for the development can be found on Figure 1. The analysis calculated the allowable discharge rates for the project. The discharge rates were determined to be 0.4 cfs/acre for residential and commercial for the SR-92 drainage area and the allowable discharge will be based upon a c-factor of 0.53 for a 50 year event for the Fox Hollow drainage basin, as seen in Figure 2. Onsite detention will be required for projects exceeding this discharge rate for a 100 year design event. The developer will be responsible for meeting the city's requirement for detention of 0.2 cfs/acre based upon the 100 year event. The detention will be provided in both onsite facilities and offsite facilities (Lambert and Jordan Narrows Ponds). The developer will construct the onsite detention determined from the difference on the allowable discharge rate and the city's 0.2 cfs/acre discharge. The developer will also construct the offsite detention as it is needed for the project.

The following is an example for East Canyon A1-A4:

Required detention based upon 0.2 cfs/acre: 76,248 cubic feet.
 Required detention based upon 0.4 cfs/acre: 58,176 cubic feet.
 Require offsite detention (Difference between 0.2 and 0.4): 18,072 cubic feet
 Offsite detention has been provided with the balance required onsite to hold to these flow rates.

An analysis of the proposed developable area was performed using the rational method to estimate the required detention volumes. Results are shown in the attached detention tables. The following c-factors were used:

<u>Land Use</u>	<u>C-Factor Range</u>	<u>C-Factor Used</u>	<u>Soil Group C</u>		<u>Soil Group D</u>	
			<u>CN Range</u>	<u>CN Used</u>	<u>CN Range</u>	<u>CN Used</u>
Native Open Space	.10	.10	55-59	57	61-65	63
Parks/Cut slopes/Landscaping	.20	.20	72-76	74	78-82	80
Low Density (1-4)	.34-.47	.41	79-83	81.0	84-87	85.5
Medium Density (4.1-6)	.47-.59	.53	83-88	85.5	87-90	88.5
High Density (6.1-20)	.59-.70	.64	88-91	89.5	90-93	91.5
Churches/Schools (70% imp.)	.69	.69	84-88	86	91-95	93
Commercial (85% imp.)	.80	.80	93-95	94	95	95
Roads/Impervious	.90	.90		95		95

The development will require approximately 75.49 acre-feet of detention. The following is an estimate of where it will be distributed.

	<u>Total Req.</u>	<u>Constructed</u>	<u>Proposed</u>
Jordan Narrows	26.50 AF	8.10 AF	18.40 AF
Lambert	10.00 AF		10.00 AF
On Site Storage	35.22 AF	5.28 AF	29.94 AF
TOTAL	75.49 acre-feet		

Storm Drains

The SR-92 basin will have storm drains designed for the 10 year event as per Lehi City Standards. Pipes will meet the requirement of Section 9.07 of the Lehi Design Standards. The maximum 10 year event will not exceed the agreed discharge into the 72" storm drain. Detention will be required to control the flows from developments draining to the 72" storm drain. This will be done by the discharge rates as shown on Figure 1 and as follows:

Adobe (9C):	109 CFS	Murdock Canal (11C):	62.8 CFS
Rail Road (10C):	72.7 CFS	Perry (13C):	22.6 CFS
Existing Bull River Bore	50.0 CFS		

The master plan storm drains are shown in Figure 3. These storm drains must be installed with developments or as soon as the existing downstream capacity is exceeded. The schedule of when the storm drain lines need to be installed is shown on Figure 3. The plan requires several major pipes to be installed. The removal of pond "A" will require the installation of several storm drain lines as shown on Figure 3. A 36" line will need to be installed south of the Murdock Corridor and a 42" line (parallel in sections) will need to be installed under the canal along Cabella's Blvd. to the Adobe corridor.

Central Canyon will have the main storm drain pipe designed for the 50 year event. The existing storm drain has a capacity of approximately 200 CFS. The outfall from the Lambert basin will be limited to 325 CFS maximum flow with discharge into the Jordan Narrows facility. A parallel storm drain construction of 48" and 60" pipe will be constructed along Traverse Mtn. Blvd. to the Lambert Detention Facility. A connection from Chapple Ridge to Fox Canyon will also be required to separate the Chapple Ridge system into parts.

Mass Grading

Mass grading operations will be detained to 0.1 CFS per acre of disturbed ground or higher as determined by the City Engineer during all construction phases to control erosion and sedimentation of downstream facilities. A complete Storm Water Pollution Prevention Plan (SWPPP) will also be developed to include Best Management Practices (BMPs), for erosion and revegetation of slopes and pads.



Master Plan	Outfall	Master Plan	Outfall
3 C	591	29 R	13
4 C	85	30 C	31
7 C	129	31 R	31
8 C	11	32 C	111
9 C	159	37 C	80
10 R	40.1	38 R	31
11 C	72.7	41 C	176
12 C	25	43 C	325
13 C	22.3		
15 R	6		
16 C	51		
17 R	3		
18 C	57		
19 R	6		
20 C	93		
21 C	23		
22 C	30		
23 R	6.2		
24 C	11		
25 R	26		

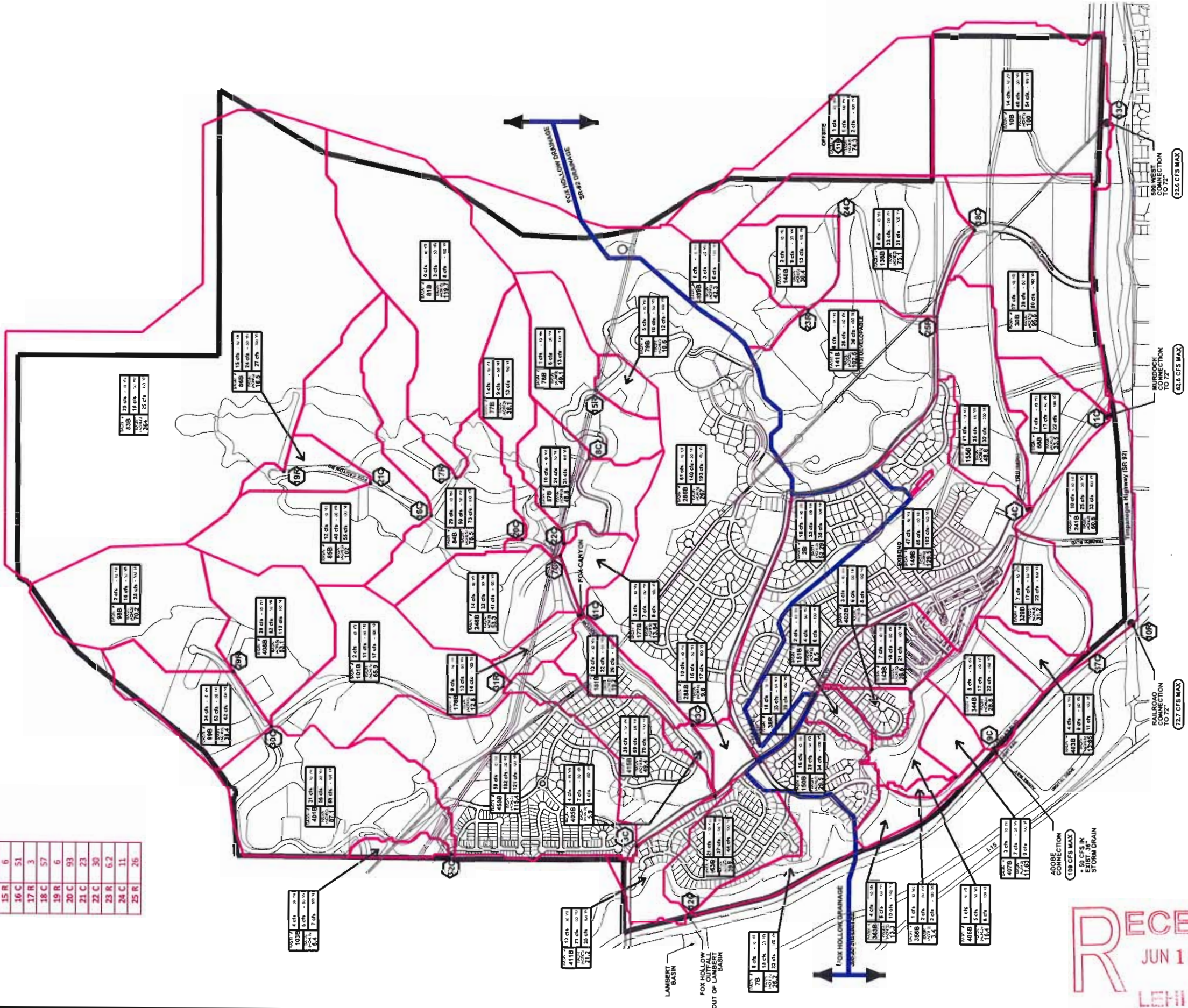
LEGEND

DRAINAGE BASIN

OUTFALLS

BASIN #	* - 10 YR
BASIN #/CFS	* - 50 YR
BASIN #/CFS	* - 100 YR

* ESTIMATED DISCHARGE FROM WMS MODEL 11-30-11



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Drawing Name:

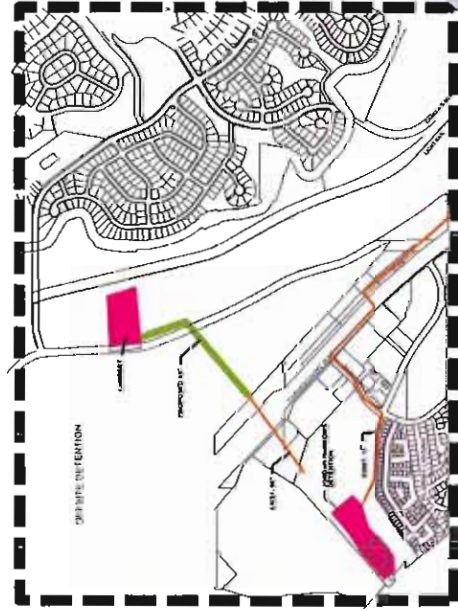
PROJECT NO.
2010.037.005

TRAVERSE MOUNTAIN, LEHI UTAH

DRAINAGE AREAS

FIGURE 1

DATE: 6-12-12



LEGEND

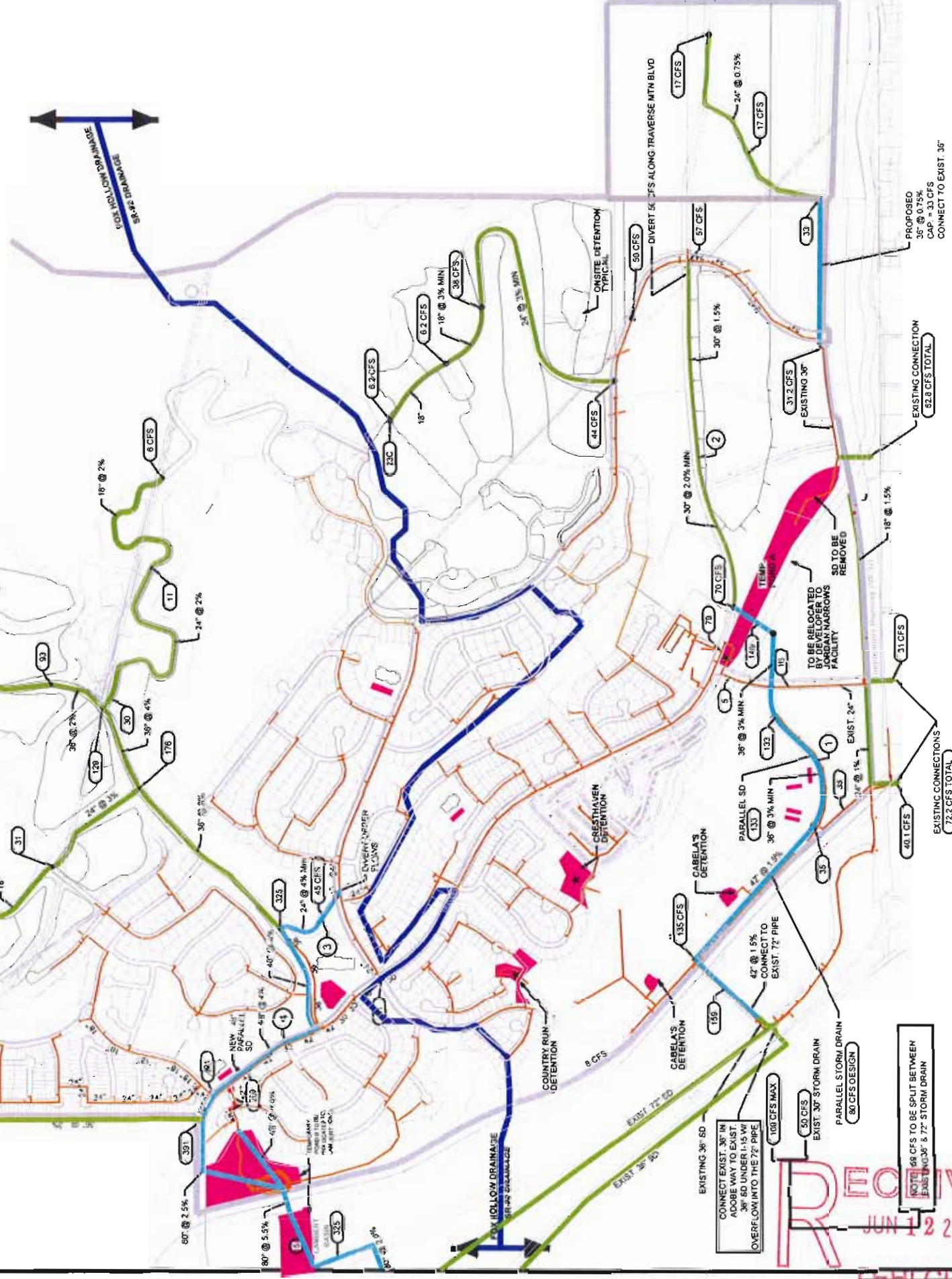
- PROPOSED MASTERPLAN PIPING TO BE PAID BY IMPACT FEES
- PROPOSED SD
- EXISTING SD
- EXIST. DETENTION

NOTE: ALL STORM DRAIN IS 18" UNLESS OTHERWISE NOTED.

- * EXISTING 5 CFS DETENTION OUTFALL
- ** DETENTION RELEASE OF 15 CFS FROM CABELA'S, HARVEST HOMES & COUNTRY RUN BASINS.
- ***OVERT 20 CFS DOWN TRIUMPH BLVD.

NOTES:

- 1) CABELA'S BLVD. PARALLEL STORM DRAIN TO BE CONSTRUCTED AS PART OF REMOVAL OF TEMP. POND "A"
- 2) TRAVERSE MOUNTAIN BLVD. STORM DRAIN SHALL BE CONSTRUCTED TO PROVIDE FOR THE 50 CFS FROM MORNING GLORY. UPON INTRODUCTION OF AN ADDITIONAL 20 CFS OF FLOW IN EAST CANYON OR THE COMMERCIAL AREA BELOW TRAVERSE MTN. BLVD. & EAST OF THE MURDOCK CANAL
- 3) THE CHAPPEL RIDGE BY-PASS SHALL BE CONSTRUCTED BEFORE ANY ADDITIONAL UNITS ARE CONSTRUCTED IN VIALETTA.
- 4) THE PARALLEL 48" STORM DRAIN SHALL BE CONSTRUCTED UPON THE INTRODUCTION OF 40 CFS IN CENTRAL CANYON.
- 5) LAMBERT POND AND OUTFALL LINE TO BE CONSTRUCTED WITH OR BEFORE CONSTRUCTION OF THE CITY PARK AT TEMPORARY POND "B"



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TRAVERSE MOUNTAIN, LEHI UTAH

STORM DRAIN PIPE SIZES

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FIGURE 3

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DETENTION
SUMMARY

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Proposed Plats Required Detention

Traverse Mountain Overall System

May 25, 2012

West Canyon	Acres	Required Detention		Onsite Detention		Lambert	Jordan Landing
		CF	Acre-Ft	CF	Acre-Ft	Acre-Ft	Acre-Ft
A1-A3	16.0	44,280	1.02	8,784	0.20	0.00	0.81
B1-B2	5.1	12,888	0.30	0	0.00	0.00	0.30
C1-C2	15.8	42,768	0.98	8,712	0.20	0.00	0.78
D1	5.7	18,216	0.42	3,816	0.09	0.00	0.33
E1-E2	14.0	37,044	0.85	7,704	0.18	0.00	0.67
F1-F3	15.5	27,720	0.64	0	0.00	0.00	0.64
Total	72.1	182,916	4.20	29,016	0.67	0.00	3.53

Central Canyon	Acres	Required Detention		Onsite Detention		Lambert	Jordan Landing
		CF	Acre-Ft	CF	Acre-Ft	Acre-Ft	Acre-Ft
A1-A2	10.3	22,824	0.52	0	0.00	0.00	0.52
B	7.0	17,676	0.41	0	0.00	0.00	0.41
C	5.7	14,400	0.33	0	0.00	0.00	0.33
D1-D2	10.4	23,076	0.53	0	0.00	0.00	0.53
E1-E2	15.0	34,200	0.79	0	0.00	0.00	0.79
F1-F3	15.2	28,116	0.65	0	0.00	0.00	0.65
G1-G2	10.4	23,076	0.53	0	0.00	0.00	0.53
H1-H2	9.9	23,184	0.53	0	0.00	0.00	0.53
I1-I2	8.4	19,152	0.44	0	0.00	0.00	0.44
J1-J2	14.4	41,616	0.96	7,920	0.18	0.00	0.77
K1-K2	9.9	26,208	0.60	5,472	0.13	0.00	0.48
L2	14.5	41,040	0.94	8,892	0.20	0.00	0.74
M1	4.0	12,780	0.29	2,700	0.06	0.00	0.23
N (Public Park)	1.2	756	0.02	0	0.00	0.00	0.02
Total	136.3	328,104	7.53	24,984	0.57	0.00	6.96

East Canyon	Acres	Required Detention		Onsite Detention		Lambert	Jordan Landing
		CF	Acre-Ft	CF	Acre-Ft	Acre-Ft	Acre-Ft
A1-A4	25.3	76,248	1.75	58,176	1.34	0.00	0.41
B1	9.0	28,764	0.66	22,284	0.51	0.00	0.15
C1-C2	19.3	38,088	0.87	28,134	0.65	0.00	0.23
D1-D6	59.4	109,908	2.52	80,730	1.85	0.00	0.67
Total	113.0	253,008	5.81	189,324	4.35	0.00	1.46

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Proposed Plats Required Detention

Traverse Mountain Overall System

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Perry Properties	Acres	Required Detention		Onsite Detention		Lambert	Jordan Landing
		CF	Acre-Ft	CF	Acre-Ft	Acre-Ft	Acre-Ft
A1-A2	34.9	83,808	1.92	62,982	1.45	0.00	0.48
B1-B2	28.4	66,456	1.53	49,842	1.14	0.00	0.38
C	69.7	222,804	5.11	172,620	3.96	0.00	1.15
D	25.6	81,828	1.88	63,396	1.46	0.00	0.42
Private Park	10.4	6,552	0.15	3,915	0.09	0.00	0.06
Total	169.0	461,448	10.59	352,755	8.10	0.00	2.50

River Bend	Acres	Required Detention		Onsite Detention		Lambert	Jordan Landing
		CF	Acre-Ft	CF	Acre-Ft	Acre-Ft	Acre-Ft
A	9.8	24,732	0.57	0	0.00	0.57	0.00
B	14.5	46,368	1.06	9,792	0.22	0.00	0.84
C	23.8	76,068	1.75	16,020	0.37	0.00	1.38
D	5.7	18,216	0.42	3,816	0.09	0.33	0.00
E	18.9	47,700	1.10	0	0.00	0.00	1.10
F	16.0	40,392	0.93	0	0.00	0.93	0.00
Total	88.7	253,476	5.82	29,628	0.68	1.83	3.31

Non-Canyon	Acres	Required Detention		Onsite Detention		Lambert	Jordan Landing
		CF	Acre-Ft	CF	Acre-Ft	Acre-Ft	Acre-Ft
Church	3.4	14,184	0.33	5,616	0.13	0.00	0.20
A	8.1	25,884	0.59	5,436	0.12	0.00	0.47
	6.5	20,772	0.48	4,356	0.10	0.00	0.38
	3.3	8,316	0.19	0	0.00	0.00	0.19
D	0.6	1,512	0.03	0	0.00	0.00	0.03
Total	21.9	70,668	1.62	15,408	0.35	0.00	1.27

Commercial	Acres	Required Detention		Onsite Detention		Lambert	Jordan Landing
		CF	Acre-Ft	CF	Acre-Ft	Acre-Ft	Acre-Ft
Public Park	9.6	6,048	0.14	3,609	0.08	0.00	0.06
Highway Comm.	9.4	39,240	0.90	32,472	0.75	0.00	0.16
Highway Comm.	7.3	30,492	0.70	25,236	0.58	0.00	0.12
Highway Comm.	6.7	27,972	0.64	23,140	0.53	0.00	0.11
Highway Comm.	7.8	32,580	0.75	26,964	0.62	0.00	0.13
Highway Comm.	14.8	61,812	1.42	51,156	1.17	0.00	0.24
Highway Comm.	2.5	10,440	0.24	8,640	0.20	0.00	0.04
Highway Comm.	114.6	478,584	10.99	396,072	9.09	0.00	1.89
Highway Comm.	27.3	114,012	2.62	94,356	2.17	0.00	0.45
HC	1.8	7,524	0.17	6,228	0.14	0.00	0.03
HC	3.1	12,960	0.30	10,728	0.25	0.00	0.05
Total	204.9	821,664	18.86	678,601	15.58	0.00	3.28



DETENTION BASIN TOTALS

Traverse Mountain Overall System

May 25, 2012

EXISTING DEVELOPMENT

Recorded Plots	DETENTION Location	REQUIRED VOLUME (cubic feet)	POND A	POND B	HH POND	CR POND	Onsite	Lambert	JORDAN NARROWS
TM BLVD. NORTH	ROAD PLAT	6,100		6,100					
TM BLVD. SOUTH	ROAD PLAT	22,500	22,500						
MORNING GLORY ROAD	ROAD PLAT	25,265	25,265						
CHAPEL RIDGE	PHASES 1&2	20,285	20,285						
	PHASE 3	19,440		19,440					
COUNTRY RUN	ALL PHASES	35,667							
HARVEST HOMES	PLAT ONE	33,000			33,000				
	PLAT TWO	0							
	PLAT THREE	0							
HEATHER MOORE	PLAT ONE	31,000	31,000						
HUNTER CHASE	PLAT ONE	15,000	15,000						
	PLAT TWO	14,000	14,000						
	PLAT THREE	2,000	2,000						
EAGLE SUMMIT	PHASES 1&2	74,558		74,558					
	PLAT THREE	870		870					
	PLAT FOUR	870		870					
	PLAT FIVE	870		870					
Eagle Summit Plat 6	Site Plan	0							
SHADOW RIDGE	PLAT ONE	28,920	28,920						
	PLAT TWO	26,950	26,950						
WINTERHAVEN	PHASES 1&2	42,274	42,274						
WOODHAVEN	PHASES 1-3	68,310	68,310						
VISTA RIDGE	PHASES 1&2	43,856	43,856						
	PHASE 3 & 4	22,908	22,908						
Traverse Mount Plat D & Challenger School	Plat D	11,909	11,909						
Violetto Recorded Plat	Plat A	39,350		39,350					
Cresthaven Townhomes	All	23,666			23,666				
Cresthaven Apartments	All	31,741			12,630				
FASHION-OUTLET	JORDAN NARROWS/ HH	114,138							
TRAVERSE MOUNTAIN SALES CENTER	JORDAN NARROWS	3,973							
CABELLAS-ON SITE	SITE PLAN	131,237	3,973						
CHURCH (TRAVERSE MOUNTAIN BLVD)		9,230							
CHURCH (CHAPEL RIDGE)		13,464							
CHURCH (FOX HILL DR.)		9,967							
TRANSFER FROM POND A TO JORDAN NARROWS AGREEMENT		0	-168,840						
Total Volumes Required for Existing Development (Cubic Feet)			0	352,368	69,296	35,667	229,857	0	236,130
Total Volumes Required for Existing Development (Acre Feet)			0.00	8.09	1.59	0.82	5.28	0.00	5.42

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DETENTION BASIN TOTALS											
Traverse Mountain Overall System											
May 25, 2012											
EXISTING DETENTION BASINS		DETENTION									
Constructed Ponds	CONSTRUCTED	VOLUME (cubic feet)	POND A	POND B	HH POND	CR POND	On Site	Lambert	JORDAN NARROWS		
TRAVERSE MOUNTAIN POND A	TRAV. PLAT 1	352,836	352,836								
TRAVERSE MOUNTAIN POND B*	CHAPEL BEND	196,020		196,020							
TRAVERSE MOUNTAIN POND B*	SHADOW RIDGE	60,984		60,984							
HARVEST HOMES	HARVEST HOME	33,000			33,000						
COUNTRY RUN	COUNTRY RUN	87,120				87,120					
CRESTHAVEN (constructed)	CRESTHAVEN	44,000				44,000					
JORDAN NARROWS (REPLACES POND A)	AGREEMENT	8,712	-352,836								
FASHION OUTLET		65,959					65,959				65,959
CABELLAS ON SITE		131,237					131,237				
CHURCH (TRAVERSE MOUNTAIN BLVD)		9,230					9,230				
CHURCH (CHAPEL RIDGE)		13,464					13,464				
CHURCH (FOXTAIL DR.)		9,967					9,967				
Total Storage Provided (cubic feet)		1,012,529	0	257,004	77,000	87,120	229,857	0		351,548	
Total Storage Provided (Acre Feet)		23.24	0.00	5.90	1.77	2.00	5.28	0.00		8.30	
Percentage of storage used		91%	0	137%	90%	41%	100%	0		65%	
Percentage Available		9%	0%	-37%	10%	59%	0%	0%		35%	
*Note: Expansion of Pond B to be in the Lambert Parcel with Vialeto and Fox Canyon Subdivisions. Upon final build out of project, no pond will exceed 100% of capacity.											

*Note: Expansion of Pond B to be in the Lambert Parcel with Vialetto and Fox Canyon Subdivisions. Upon final build out of project, no pond will exceed 100% of capacity.



DETENTION BASIN TOTALS

Traverse Mountain Overall System

May 25, 2012

PROPOSED DEVELOPMENT

Proposed Plots	AREA PLAN	DETENTION					Lambert	JORDAN NARROWS
		VOLUME (cubic feet)	POND A	POND B	HH POND	CR POND		
TRANSFER FROM POND B TO LAMBERT		0		-352,368			352,368	0
West Canyon		182,916					0	153,900
Central Canyon		328,104					0	303,110
East Canyon		253,008					0	53,684
Perry Properties		461,448					0	109,693
Riverbend Properties		253,476					79,524	144,314
Commercial		821,664					0	149,363

Total Volumes Required for Proposed Development (Cubic Feet)

2,300,616

Total Volumes Required for Proposed Development (Acre Feet)

52.81

PROPOSED DETENTION BASINS

Proposed Pond Expansions	DETENTION VOLUME (cubic feet)	POND A	POND B	HH POND	CR POND	On Site	Lambert	JORDAN NARROWS
Jordan Narrows Expansion	792,792							792,792
Lambert Pond	178,596		-257,004			29,015	435,600	
West Canyon	29,016					24,984		
Central Canyon	24,984					189,324		
East Canyon	189,324					352,755		
Perry Properties	352,755					29,523		
Riverbend Properties	29,523					678,601		
Commercial	678,601							

Total Volumes Required for Proposed Development (Cubic Feet)

2,275,696

Total Volumes Required for Proposed Development (Acre Feet)

52.24

Percentage of storage used

101%

Percentage Available

-1%



DETENTION BASIN TOTALS

Traverse Mountain Overall System

May 25, 2012

PROJECT TOTALS

	DETENTION		POND	POND	POND	HH	CR	On Site	Lambert	JORDAN
	VOLUME		A	B		POND	POND			NARROWS
Required Storage										
Storage Required For Existing Development	Cubic Feet	923,318	0	352,368	69,296	35,667	229,657	0	236,130	
	Acre Feet	21.20	0.00	8.09	1.59	0.82	5.28	0.00	5.42	
Storage Required For Proposed Development	Cubic Feet	2,300,616	0	-352,368	0	0	1,304,308	431,892	916,784	
	Acre Feet	52.81	0.00	-8.09	0.00	0.00	29.94	9.91	21.05	
Total Required Storage For Project (Cubic Feet)		3,223,934	0	0	69,296	35,667	1,534,165	431,892	1,152,914	
Total Required Storage For Project (Acre Feet)		74.01	0.00	0.00	1.59	0.82	35.22	9.91	26.47	

DETENTION

	DETENTION		POND	POND	POND	HH	CR	On Site	Lambert	JORDAN
	VOLUME		A	B		POND	POND			NARROWS
Provided Storage										
Constructed Pond Total	Cubic Feet	1,012,529	0	237,004	77,000	87,120	229,657	0	321,545	
	Acre Feet	23	0	5	2	2	5	0	8	
Proposed Pond Expansion Total	Cubic Feet	2,275,696	0	-237,004	0	0	1,304,308	431,892	792,732	
	Acre Feet	52.24	0.00	-5.90	0.00	0.00	29.94	10.00	18.10	
Total Required Storage For Project (Cubic Feet)		3,288,225	0	0	77,000	87,120	1,534,165	431,892	1,154,340	
Total Required Storage For Project (Acre Feet)		75.49	0.00	0.00	1.77	2.00	35.22	10.00	26.50	
Percentage of storage used		58%	0%	0%	90%	41%	100%	99%	100%	
Percentage Available		2%	0%	0%	10%	59%	0%	1%	0%	

Note: Expansion of Pond B to be in the Lambert Parcel with Vialto and Fox Canyon Subdivisions. Upon final build out of project, no pond will exceed 100% of capacity.



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LEHI CITY

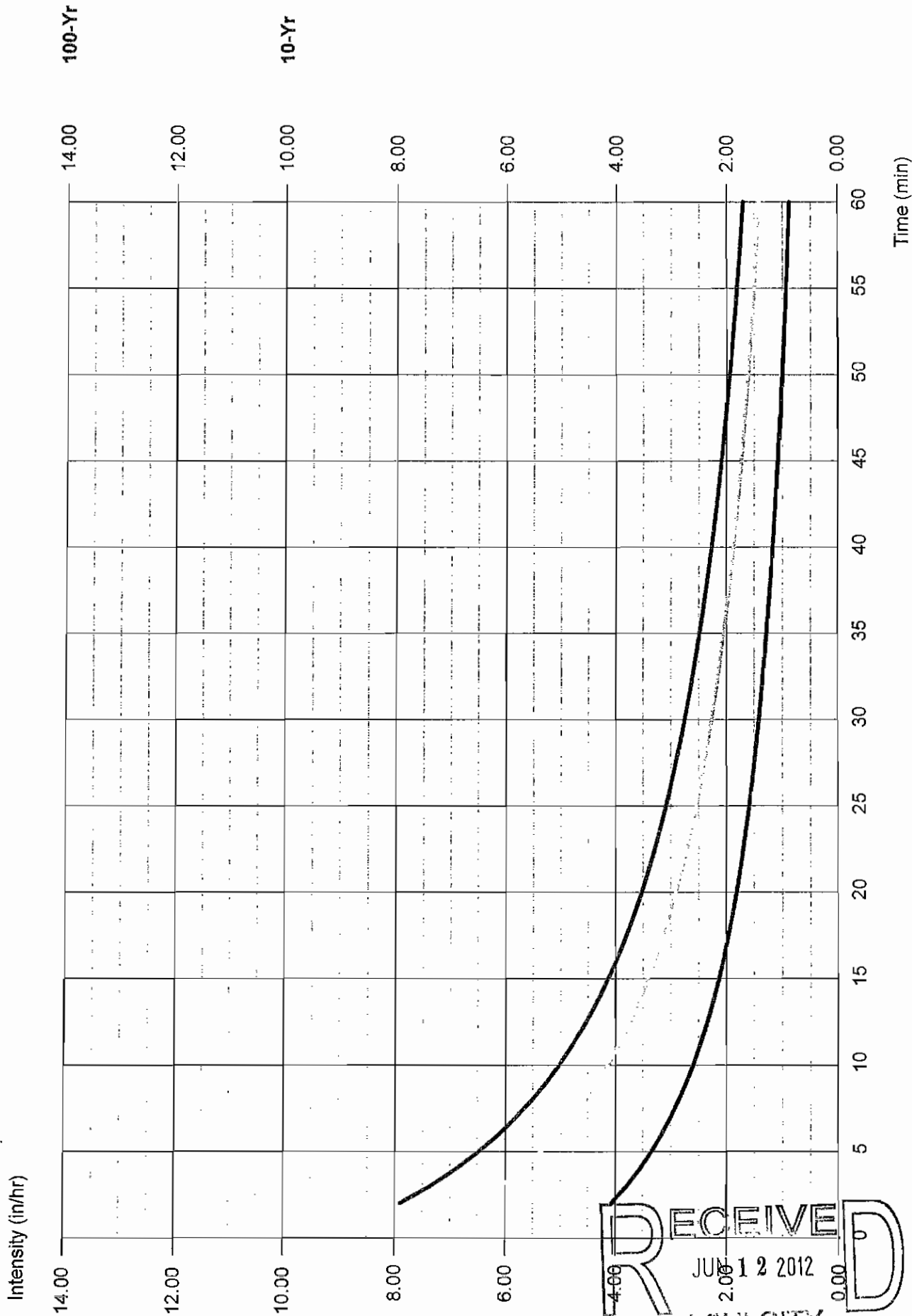
C

C

C

Hydrology IDF Curves

IDF file: .average.IDF



Friday, Apr 22, 2011

File name: lehitraverse.IDF

Return Period (Yrs)	Intensity Values (in/hr)											
	5 min	10	15	20	25	30	35	40	45	50	55	60
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10	3.34	2.60	2.14	1.82	1.59	1.42	1.28	1.17	1.08	1.00	0.93	0.88
25	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
50	5.35	4.14	3.41	2.91	2.55	2.27	2.05	1.88	1.73	1.61	1.50	1.41
100	6.48	5.03	4.13	3.53	3.09	2.75	2.48	2.27	2.09	1.94	1.81	1.70

Tc = time in minutes. Values may exceed 60.

Precip. file name: Lehitraverse.pcp

[illegible]

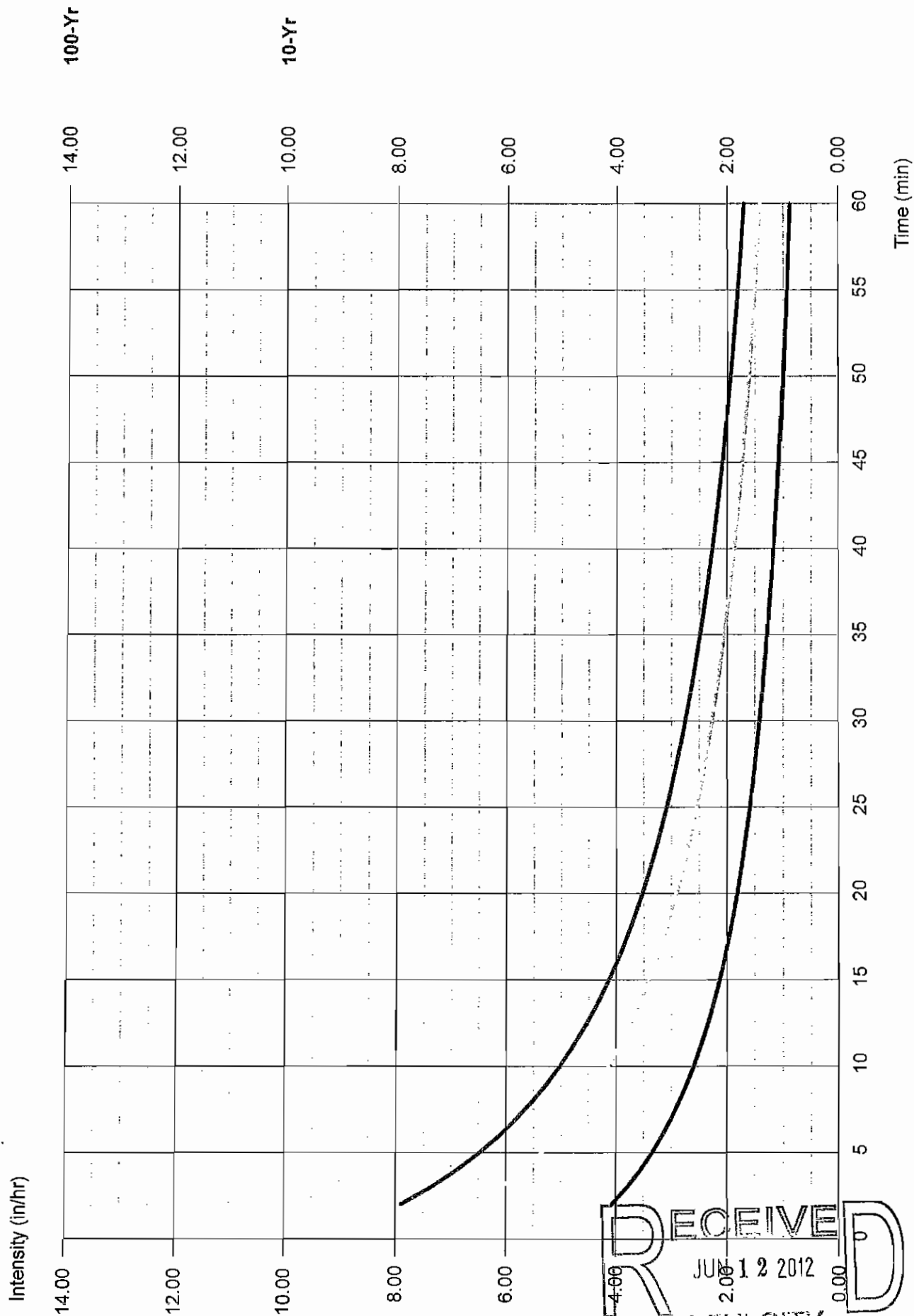
RAINFALL

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LEHI CITY

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JUN 12 2012
LEHI CITY

Friday, Apr 22, 2011

File name: lehitraverse.IDF

$$\text{Intensity} = B / (T_c + D)^E$$

Return Period (Yrs)	Intensity Values (in/hr)											
	5 min	10	15	20	25	30	35	40	45	50	55	60
1	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
3	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
5	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
10	3.34	2.60	2.14	1.82	1.59	1.42	1.28	1.17	1.08	1.00	0.93	0.88
25	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
50	5.35	4.14	3.41	2.91	2.55	2.27	2.05	1.88	1.73	1.61	1.50	1.41
100	6.48	5.03	4.13	3.53	3.09	2.75	2.48	2.27	2.09	1.94	1.81	1.70

Tc = time in minutes. Values may exceed 60.

Precip. file name: Lehitraverse.pcp

[illegible]



NOAA Atlas 14, Volume 1, Version 6
Location name: Lehi, Utah, US*
Coordinates: 40.4373, -111.8674
Elevation: 4978ft*
* source: Google Maps



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Malleria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Micheal Yekie, Tan Zhao, Geoffrey Bonnin, Daniel Brewin, Li-Chuan Chen, Tye Parzybnik, John Yarchean

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aeries](#)

PF tabular

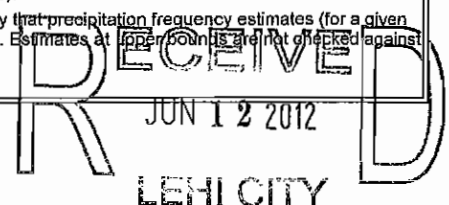
PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹										
Duration	Average recurrence interval(years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	0.128 (0.112-0.148)	0.162 (0.143-0.188)	0.223 (0.195-0.259)	0.279 (0.241-0.324)	0.366 (0.308-0.429)	0.447 (0.366-0.528)	0.541 (0.430-0.647)	0.652 (0.499-0.792)	0.830 (0.602-1.03)	0.992 (0.689-1.26)
10-min	0.195 (0.171-0.226)	0.247 (0.217-0.287)	0.339 (0.297-0.394)	0.424 (0.366-0.493)	0.557 (0.469-0.652)	0.681 (0.558-0.804)	0.824 (0.655-0.984)	0.993 (0.760-1.21)	1.26 (0.917-1.57)	1.51 (1.05-1.92)
15-min	0.242 (0.212-0.280)	0.306 (0.270-0.355)	0.421 (0.368-0.488)	0.526 (0.454-0.611)	0.690 (0.581-0.809)	0.844 (0.692-0.996)	1.02 (0.812-1.22)	1.23 (0.942-1.49)	1.57 (1.14-1.95)	1.87 (1.30-2.38)
30-min	0.325 (0.285-0.377)	0.413 (0.363-0.478)	0.567 (0.495-0.657)	0.708 (0.611-0.823)	0.929 (0.783-1.09)	1.14 (0.931-1.34)	1.38 (1.09-1.64)	1.66 (1.27-2.01)	2.11 (1.53-2.62)	2.52 (1.75-3.20)
60-min	0.403 (0.353-0.466)	0.511 (0.449-0.592)	0.701 (0.613-0.813)	0.876 (0.756-1.02)	1.15 (0.969-1.35)	1.41 (1.15-1.66)	1.70 (1.35-2.03)	2.05 (1.57-2.49)	2.61 (1.90-3.25)	3.12 (2.17-3.97)
2-hr	0.503 (0.456-0.571)	0.630 (0.566-0.712)	0.823 (0.735-0.932)	1.00 (0.887-1.14)	1.29 (1.12-1.48)	1.56 (1.31-1.79)	1.67 (1.53-2.18)	2.24 (1.76-2.66)	2.83 (2.11-3.46)	3.37 (2.40-4.21)
3-hr	0.582 (0.531-0.649)	0.720 (0.658-0.801)	0.912 (0.827-1.01)	1.09 (0.979-1.21)	1.37 (1.21-1.53)	1.61 (1.39-1.82)	1.91 (1.60-2.19)	2.26 (1.84-2.69)	2.85 (2.21-3.49)	3.38 (2.52-4.26)
6-hr	0.762 (0.706-0.829)	0.936 (0.866-1.02)	1.14 (1.05-1.25)	1.32 (1.22-1.45)	1.59 (1.44-1.75)	1.82 (1.61-2.01)	2.07 (1.81-2.32)	2.38 (2.03-2.71)	2.95 (2.44-3.53)	3.44 (2.77-4.30)
12-hr	0.967 (0.893-1.05)	1.18 (1.09-1.29)	1.43 (1.32-1.56)	1.64 (1.50-1.80)	1.95 (1.76-2.14)	2.20 (1.96-2.44)	2.46 (2.16-2.76)	2.76 (2.38-3.14)	3.23 (2.71-3.76)	3.62 (2.96-4.33)
24-hr	1.08 (1.01-1.16)	1.33 (1.24-1.43)	1.58 (1.48-1.70)	1.79 (1.68-1.92)	2.08 (1.94-2.23)	2.30 (2.13-2.46)	2.52 (2.33-2.79)	2.78 (2.53-3.17)	3.26 (2.78-3.79)	3.65 (2.99-4.37)
2-day	1.28 (1.20-1.37)	1.57 (1.47-1.68)	1.87 (1.75-2.00)	2.12 (1.98-2.26)	2.45 (2.29-2.62)	2.71 (2.52-2.89)	2.97 (2.75-3.17)	3.23 (2.97-3.46)	3.57 (3.26-3.86)	3.83 (3.48-4.42)
3-day	1.40 (1.30-1.50)	1.71 (1.59-1.84)	2.04 (1.90-2.20)	2.32 (2.16-2.49)	2.70 (2.51-2.90)	2.99 (2.77-3.22)	3.29 (3.03-3.54)	3.60 (3.29-3.88)	4.00 (3.63-4.35)	4.31 (3.89-4.83)
4-day	1.51 (1.40-1.64)	1.85 (1.72-2.01)	2.22 (2.06-2.39)	2.52 (2.34-2.72)	2.95 (2.72-3.18)	3.28 (3.02-3.54)	3.62 (3.32-3.92)	3.96 (3.61-4.30)	4.43 (4.00-4.83)	4.80 (4.30-5.25)
7-day	1.79 (1.65-1.94)	2.19 (2.03-2.38)	2.61 (2.42-2.83)	2.96 (2.74-3.20)	3.43 (3.17-3.71)	3.80 (3.50-4.10)	4.16 (3.82-4.50)	4.53 (4.14-4.91)	5.02 (4.54-5.46)	5.38 (4.85-5.88)
10-day	2.01 (1.86-2.17)	2.46 (2.28-2.66)	2.92 (2.72-3.15)	3.29 (3.06-3.54)	3.78 (3.50-4.08)	4.14 (3.82-4.45)	4.49 (4.14-4.84)	4.84 (4.45-5.22)	5.26 (4.83-5.72)	5.61 (5.10-6.09)
20-day	2.65 (2.45-2.85)	3.25 (3.00-3.50)	3.83 (3.55-4.13)	4.29 (3.98-4.61)	4.87 (4.50-5.23)	5.28 (4.89-5.68)	5.68 (5.25-6.11)	6.06 (5.58-6.52)	6.52 (5.99-7.03)	6.84 (6.26-7.40)
30-day	3.19 (2.95-3.43)	3.90 (3.62-4.20)	4.59 (4.26-4.94)	5.13 (4.76-5.51)	5.82 (5.40-6.25)	6.33 (5.85-6.80)	6.81 (6.29-7.34)	7.27 (6.70-7.85)	7.85 (7.20-8.50)	8.26 (7.55-8.97)
45-day	3.96 (3.69-4.26)	4.84 (4.51-5.21)	5.68 (5.30-6.10)	6.33 (5.90-6.79)	7.16 (6.67-7.67)	7.75 (7.21-8.30)	8.31 (7.72-8.91)	8.84 (8.19-9.49)	9.47 (8.76-10.2)	9.91 (9.13-10.7)
60-day	4.69 (4.37-5.04)	5.74 (5.34-6.17)	6.72 (6.26-7.20)	7.47 (6.97-8.01)	8.42 (7.84-9.03)	9.10 (8.46-9.75)	9.73 (9.04-10.4)	10.3 (9.57-11.1)	11.0 (10.2-11.9)	11.5 (10.6-12.4)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

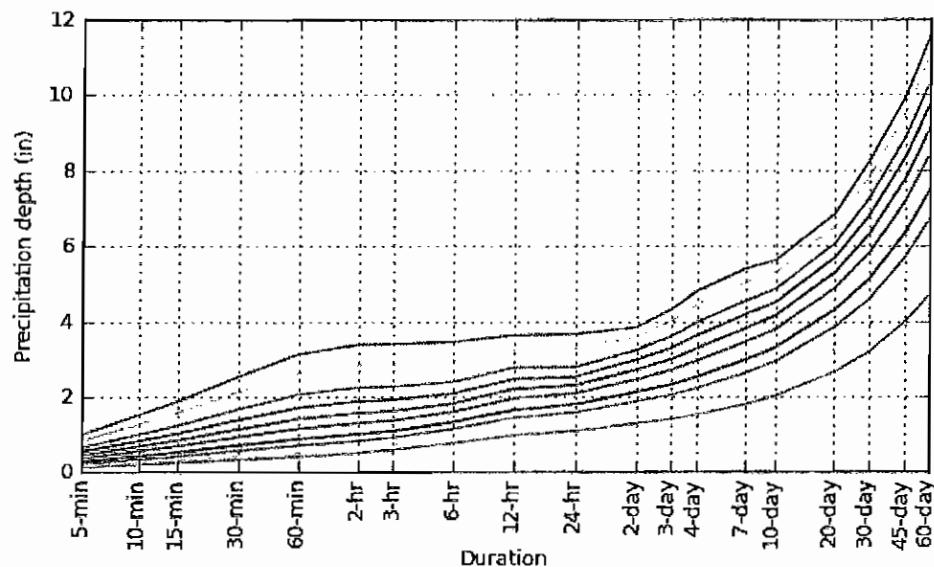
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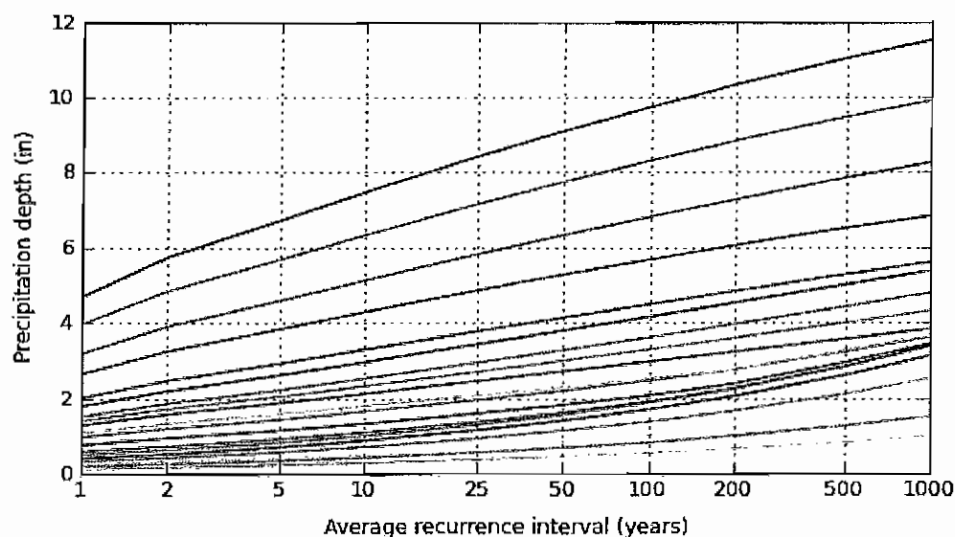
PF graphical

PDS-based depth-duration-frequency (DDF) curves

Coordinates: 40.4373, -111.8674



Average recurrence interval (years)
1
2
5
10
25
50
100
200
500
1000



Duration	
5-min	2-day
10-min	3-day
15-min	4-day
30-min	7-day
60-min	10-day
2-hr	20-day
3-hr	30-day
6-hr	45-day
12-hr	60-day
24-hr	

NOAA/NWS/OHD/HDSC

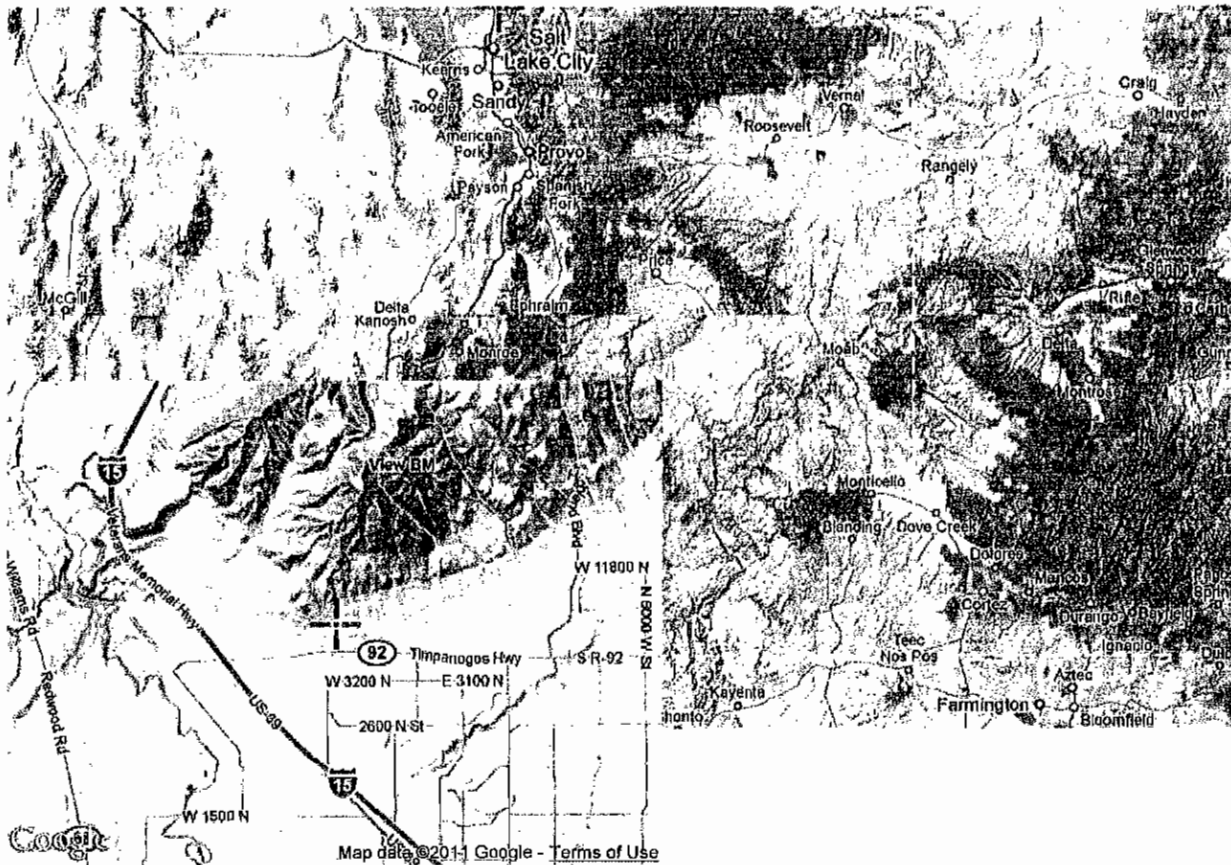
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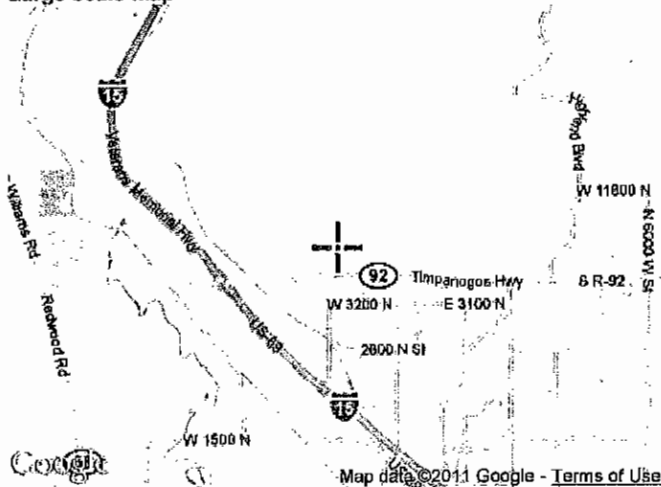
Maps & aeriels

Small scale terrain





Large scale map



Large scale aerial



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JUN 12 2012
LEHI CITY



NOAA Atlas 14, Volume 1, Version 5
 Location name: Lehi, Utah, US*
 Coordinates: 40.4373, -111.8674
 Elevation: 4978ft*
 * source: Google Maps



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dlotz, Sarah Holm, Lillian Hiner, Kazungu Maiteria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fanglin Yan, Michael Yokta, Tan Zhao, Geoffrey Bonnin, Daniel Brower, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aeriels](#)

PF tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour) ¹										
Duration	Average recurrence interval(years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	1.54 (1.34-1.78)	1.94 (1.72-2.26)	2.68 (2.34-3.11)	3.35 (2.89-3.89)	4.39 (3.70-5.15)	5.36 (4.39-6.34)	6.49 (5.16-7.76)	7.82 (5.99-9.50)	9.96 (7.22-12.4)	11.9 (8.27-15.1)
10-min	1.17 (1.03-1.36)	1.48 (1.30-1.72)	2.03 (1.78-2.36)	2.54 (2.20-2.96)	3.34 (2.81-3.91)	4.09 (3.35-4.82)	4.94 (3.93-5.90)	5.96 (4.56-7.23)	7.58 (5.50-9.43)	9.06 (6.29-11.5)
15-min	0.968 (0.848-1.12)	1.22 (1.08-1.42)	1.68 (1.47-1.95)	2.10 (1.82-2.44)	2.76 (2.32-3.24)	3.38 (2.77-3.98)	4.09 (3.25-4.88)	4.92 (3.77-5.98)	6.26 (4.55-7.79)	7.49 (5.20-9.52)
30-min	0.650 (0.570-0.754)	0.826 (0.726-0.956)	1.13 (0.990-1.31)	1.42 (1.22-1.65)	1.86 (1.57-2.18)	2.27 (1.86-2.68)	2.75 (2.19-3.28)	3.32 (2.54-4.03)	4.22 (3.06-5.25)	5.04 (3.50-6.41)
60-min	0.403 (0.353-0.466)	0.511 (0.449-0.592)	0.701 (0.613-0.813)	0.876 (0.756-1.02)	1.15 (0.969-1.35)	1.41 (1.15-1.66)	1.70 (1.35-2.03)	2.05 (1.57-2.49)	2.61 (1.90-3.25)	3.12 (2.17-3.97)
2-hr	0.252 (0.228-0.286)	0.315 (0.283-0.356)	0.412 (0.368-0.466)	0.501 (0.444-0.569)	0.646 (0.558-0.738)	0.779 (0.658-0.897)	0.936 (0.762-1.09)	1.12 (0.878-1.33)	1.42 (1.05-1.73)	1.69 (1.20-2.11)
3-hr	0.194 (0.177-0.216)	0.240 (0.219-0.267)	0.304 (0.275-0.338)	0.362 (0.326-0.404)	0.455 (0.401-0.510)	0.536 (0.463-0.607)	0.636 (0.534-0.730)	0.753 (0.613-0.896)	0.947 (0.736-1.16)	1.13 (0.839-1.42)
6-hr	0.127 (0.118-0.138)	0.156 (0.145-0.171)	0.191 (0.176-0.208)	0.221 (0.203-0.241)	0.266 (0.240-0.292)	0.303 (0.270-0.335)	0.346 (0.302-0.388)	0.398 (0.340-0.452)	0.492 (0.407-0.589)	0.575 (0.463-0.718)
12-hr	0.080 (0.074-0.087)	0.098 (0.091-0.107)	0.119 (0.109-0.130)	0.136 (0.125-0.149)	0.162 (0.146-0.178)	0.182 (0.163-0.202)	0.204 (0.179-0.229)	0.229 (0.197-0.260)	0.268 (0.225-0.312)	0.300 (0.246-0.359)
24-hr	0.045 (0.042-0.048)	0.055 (0.052-0.059)	0.066 (0.062-0.071)	0.075 (0.070-0.080)	0.087 (0.081-0.093)	0.096 (0.089-0.103)	0.105 (0.097-0.116)	0.116 (0.105-0.132)	0.136 (0.116-0.158)	0.152 (0.124-0.182)
2-day	0.027 (0.025-0.029)	0.033 (0.031-0.035)	0.039 (0.036-0.042)	0.044 (0.041-0.047)	0.051 (0.048-0.055)	0.056 (0.052-0.060)	0.062 (0.057-0.066)	0.067 (0.062-0.072)	0.074 (0.068-0.080)	0.080 (0.072-0.092)
3-day	0.019 (0.018-0.021)	0.024 (0.022-0.026)	0.028 (0.026-0.031)	0.032 (0.030-0.035)	0.037 (0.035-0.040)	0.042 (0.038-0.045)	0.046 (0.042-0.049)	0.050 (0.046-0.054)	0.056 (0.050-0.060)	0.060 (0.054-0.067)
4-day	0.016 (0.015-0.017)	0.019 (0.018-0.021)	0.023 (0.021-0.025)	0.026 (0.024-0.028)	0.031 (0.028-0.033)	0.034 (0.031-0.037)	0.038 (0.035-0.041)	0.041 (0.038-0.045)	0.046 (0.042-0.050)	0.050 (0.045-0.055)
7-day	0.011 (0.010-0.012)	0.013 (0.012-0.014)	0.016 (0.014-0.017)	0.018 (0.016-0.019)	0.020 (0.019-0.022)	0.023 (0.021-0.024)	0.025 (0.023-0.027)	0.027 (0.025-0.029)	0.030 (0.027-0.032)	0.032 (0.029-0.035)
10-day	0.008 (0.008-0.009)	0.010 (0.010-0.011)	0.012 (0.011-0.013)	0.014 (0.013-0.015)	0.016 (0.015-0.017)	0.017 (0.016-0.019)	0.019 (0.017-0.020)	0.020 (0.019-0.022)	0.022 (0.020-0.024)	0.023 (0.021-0.025)
20-day	0.006 (0.005-0.006)	0.007 (0.006-0.007)	0.008 (0.007-0.009)	0.009 (0.008-0.010)	0.010 (0.009-0.011)	0.011 (0.010-0.012)	0.012 (0.011-0.013)	0.013 (0.012-0.014)	0.014 (0.012-0.015)	0.014 (0.013-0.015)
30-day	0.004 (0.004-0.005)	0.005 (0.005-0.006)	0.006 (0.006-0.007)	0.007 (0.007-0.008)	0.008 (0.007-0.009)	0.009 (0.008-0.009)	0.009 (0.009-0.010)	0.010 (0.009-0.011)	0.011 (0.010-0.012)	0.011 (0.010-0.012)
45-day	0.004 (0.003-0.004)	0.004 (0.004-0.005)	0.005 (0.005-0.006)	0.006 (0.005-0.006)	0.007 (0.006-0.007)	0.007 (0.007-0.008)	0.008 (0.007-0.008)	0.008 (0.008-0.009)	0.009 (0.008-0.009)	0.009 (0.008-0.010)
60-day	0.003 (0.003-0.003)	0.004 (0.004-0.004)	0.005 (0.004-0.005)	0.005 (0.005-0.006)	0.006 (0.005-0.006)	0.006 (0.006-0.007)	0.007 (0.006-0.007)	0.007 (0.007-0.008)	0.008 (0.007-0.008)	0.008 (0.007-0.009)

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

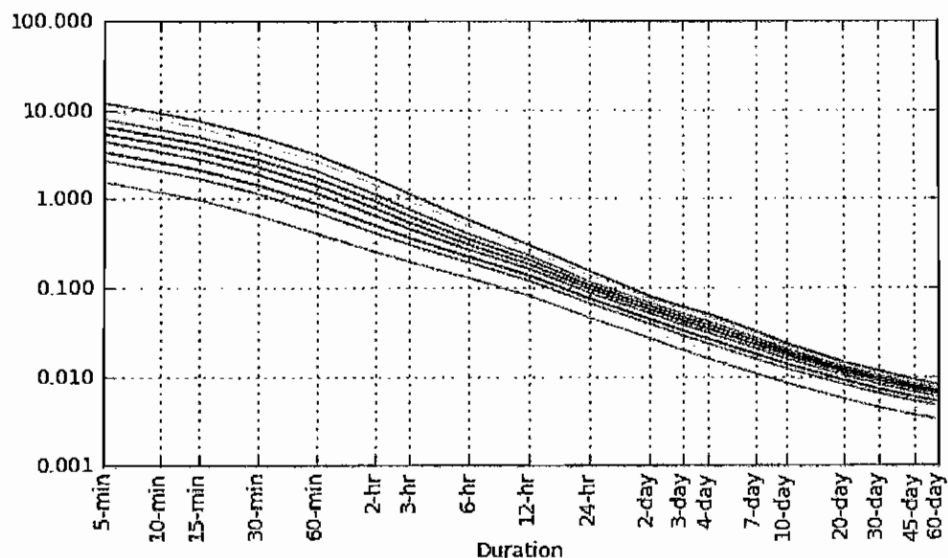
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

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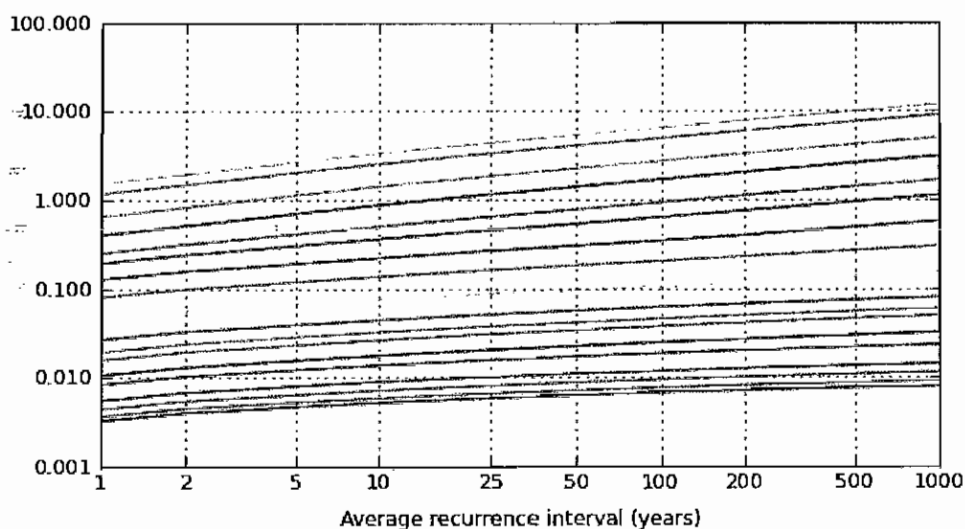
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PF graphical

PDS-based intensity-duration-frequency (IDF) curves
Coordinates: 40.4373, -111.8674



Average recurrence interval (years)
1
2
5
10
25
50
100
200
500
1000



Duration	
5-min	2-day
10-min	3-day
15-min	4-day
30-min	7-day
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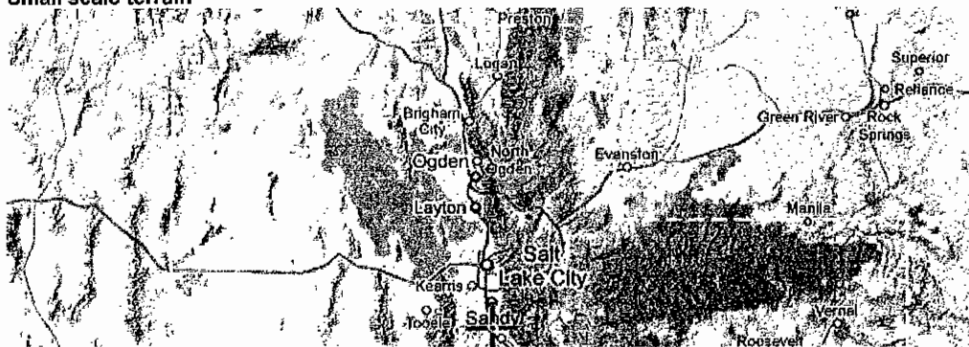
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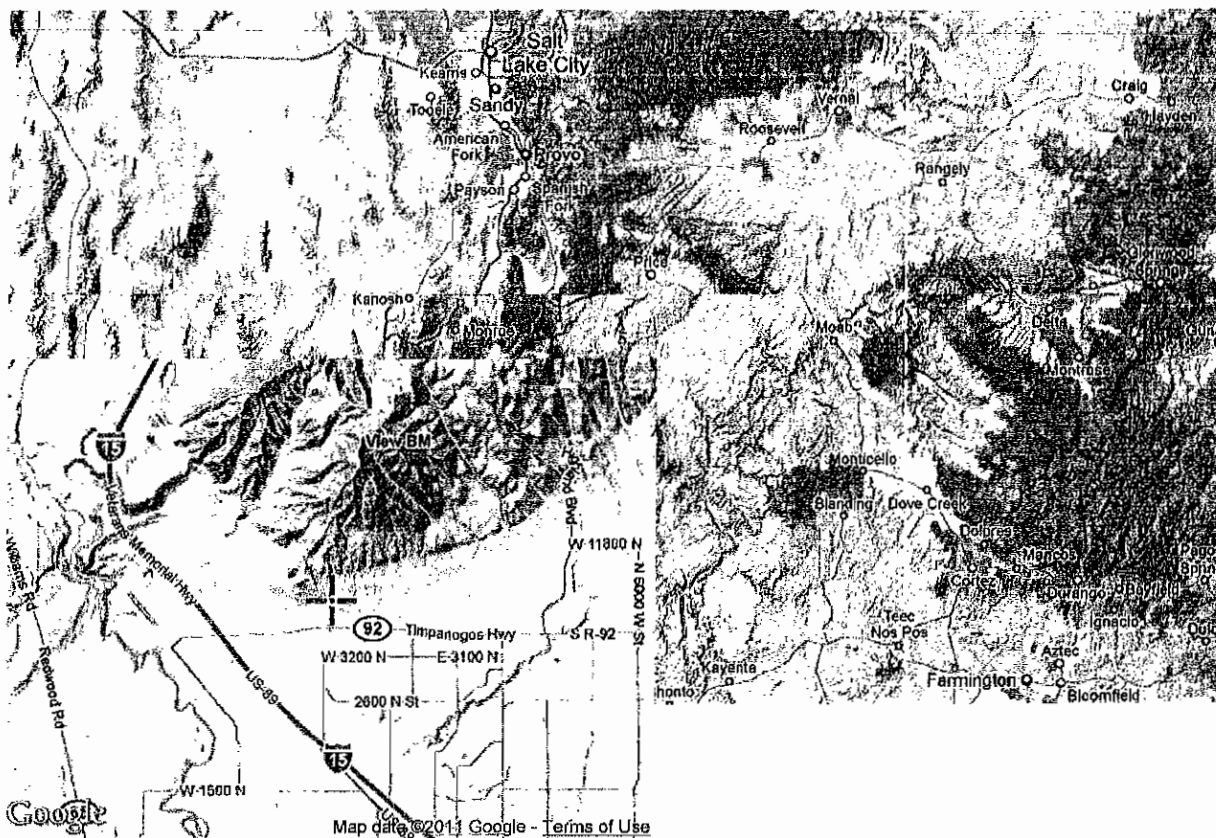
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Maps & aerals

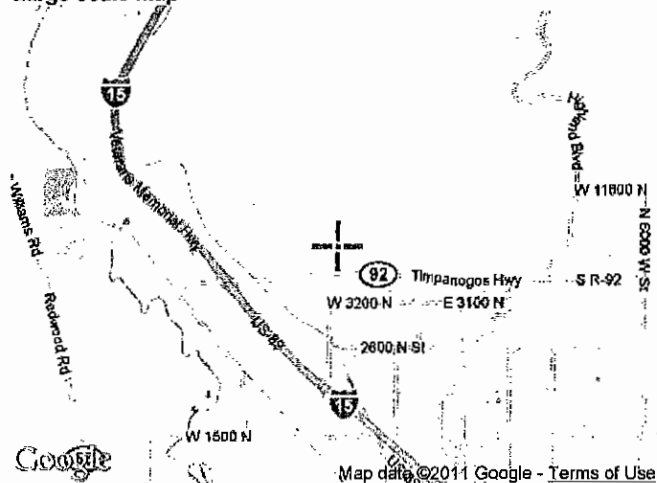
Small scale terrain



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LEHI CITY



Large scale map



Large scale aerial



LEHI CITY
AGREEMENT & UDOT
EXHIBITS

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AGREEMENT

For

LEHI CITY DETENTION & STORM DRAIN FACILITIES AT PILGRIM'S LANDING

Between

LEHI CITY and PILGRIM'S LANDING, LLC and
MOUNTAIN HOME DEVELOPMENT CORPORATION

WHEREAS, Lehi City owns an existing 8.10 acre foot detention basin (the "Traverse Mountain Detention Basin") on a 9.46 acre parcel located in the Traverse Mountain Development (Parcel No.: 53:257:0001) (the "Development Property");

WHEREAS, Lehi City owns and maintains an existing detention facility (the "Pilgrim's Landing Detention Basin") along the western edge of the Pilgrim's Landing, LLC property, and has already purchased an additional 1.15 acres of adjacent property from Pilgrim's Landing, LLC;

WHEREAS, Lehi City is currently in the process of designing and constructing a 72-inch storm drain and detention basin along and in property owned by Pilgrim's Landing, LLC;

WHEREAS, Lehi City desires to acquire additional land from Pilgrim's Landing, LLC to upgrade and increase the Pilgrim's Landing Detention Basin's capacity to serve the residents of Lehi City, drainage from I-15, SR-92, and Traverse Mountain Development (including replacement of the Traverse Mountain Detention Basin), and to provide a multi-use facility; and

WHEREAS, Mountain Home Development Corporation desires to acquire from Lehi City the Development Property for commercial development purposes, and Lehi City is willing to convey such property to Mountain Home Development Corporation on the terms and conditions set forth herein.

NOW THEREFORE, in consideration of the foregoing premises and the mutual promises contained herein, the Parties hereto agree as follows:

1. Pilgrim's Landing, LLC will sign a Special Warranty Deed to Lehi City for the property needed to increase the area of the Pilgrim's Landing Detention Basin to approximately 18.75 acres. (See attached Exhibit A.) The price of the sale will be \$2,890,000.00.
2. Lehi City will pay Pilgrim's Landing, LLC \$200,000.00 to be applied toward the total purchase price, reducing the amount owing to \$2,690,000.00. In consideration of Mountain Home Development Corporation being able to purchase the Development Property, it agrees to pay to Pilgrim's Landing, LLC the balance of the purchase price (\$2,690,000.00), to be evidenced by a Promissory Note from Mountain Home Development Corporation in favor of Pilgrim's Landing, LLC, secured by a first priority Trust Deed on the Development Property in favor of Pilgrim's Landing, LLC.

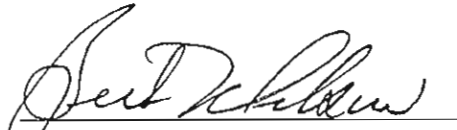


3. Lehi City will construct a detention basin on the property purchased from Pilgrim's Landing, LLC with a capacity of 17.1 acre feet, and upon completion thereof Lehi City will decommission the detention basin on the Development Property.
4. Lehi City will sign a Special Warranty Deed to Mountain Home Development Corporation for the 9.46 acre parcel (County Parcel No.: 53:257:0001, see attached Exhibit B) per the Area Plan Note #4, page 1 on the concept plan approved by Lehi City on November 18, 2008 which shall be used for commercial purposes only as generally described in the Area Plan.
5. Mountain Home Development Corporation will execute a promissory note and a first-position trust deed on the 9.46 acre parcel in favor of Pilgrim's Landing, LLC with the following terms:
 - a. The promissory note shall be in the principal amount of \$2,690,000.00, plus interest at the rate of 7% per annum.
 - b. Annual interest payments of \$188,300.00 shall be due on each anniversary date of the Promissory Note, and all unpaid principal and accrued interest shall be due on the 3rd anniversary of the Promissory Note.
 - c. The Trust Deed on the Development Property shall be in the amount of \$2,690,000.00, plus accrued interest, with a 3-year maturity date.
 - d. Mountain Home Development Corporation's obligations under the trust deed will be recourse only to the property encumbered by the trust deed.
 - e. If Pilgrim's Landing, LLC and/or its successors and assigns forecloses on the trust deed and acquires ownership of the 9.46 acre parcel, all owners of the parcel will hold the parcel subject to the Traverse Mountain Area Plan and CC&R's, all as in effect from time to time.
6. Lehi City will own and agrees to diligently proceed to build and maintain the new storm drain and detention facility to be built on the property purchased from Pilgrim's Landing, LLC.
7. Mountain Home Development Corporation will expand at its own cost the new storm basin to 37 acre feet in the future as capacity is needed.
8. Mountain Home Development Corporation will provide the trust deed in form and substance acceptable to Pilgrim's Landing, LLC in its sole discretion.
9. Lehi City will provide all legal documents for the Special Warranty Deeds in form and substance acceptable to the grantees of such Special Warranty Deeds.
10. The grantors of the Special Warranty Deeds shall provide at their cost an ALTA standard owner's policy insuring title to the subject properties, respectively, with only such exceptions as may be approved by the grantees.



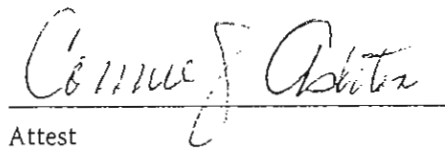
11. Lehi City, Pilgrim's Landing, LLC, and Mountain Home Development Corporation agree to close with Affiliated First Title Company, 321 East State Road, American Fork, UT 84003, Attention: Marnae Ballantyne.

Signed:


Lehi City

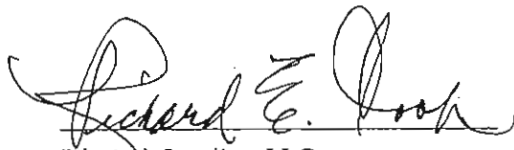
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Date

Lehi City Mayor
Title


Attest

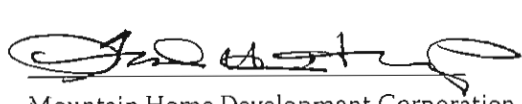
7/28/10
Date

City Recorder
Title


Pilgrim's Landing, LLC

7/28/10
Date

Manager
Title


Mountain Home Development Corporation
By Ted Heap, CEO

7/28/10
Date

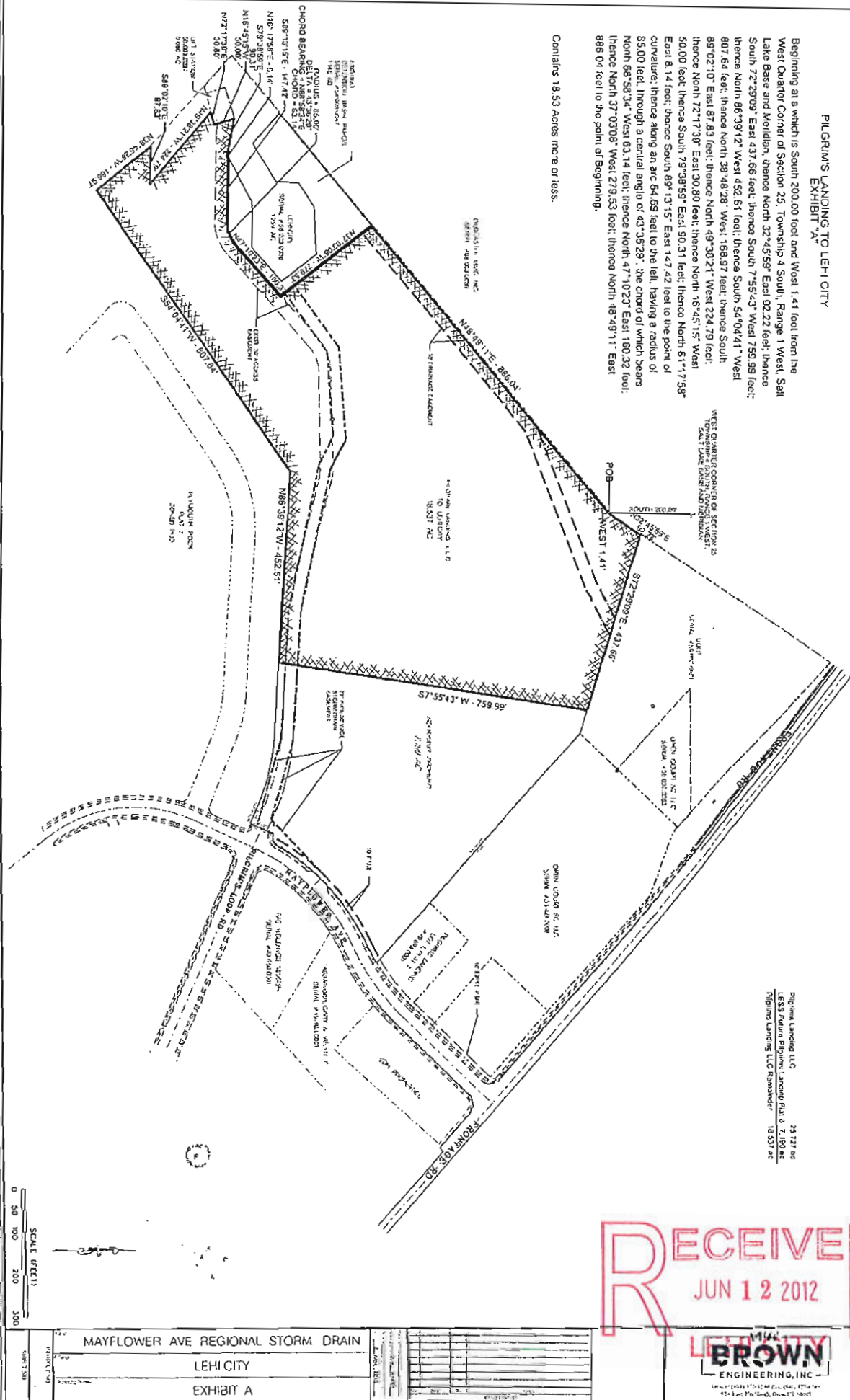
CEO
Title



PILGRIMS LANDING TO LEHI CITY
EXHIBIT "A"

Beginning at a which is South 200.00 feet and West 1.41 feet from the West Quarter Corner of Section 25, Township 4 South, Range 1 West, Salt Lake Base and Meridian, thence North 32°45'59" East 82.22 feet; thence South 72°29'09" East 437.66 feet; thence South 7°55'43" West 759.99 feet; thence North 86°39'12" West 452.61 feet; thence South 54°04'41" West 807.64 feet; thence North 38°48'28" West 158.97 feet; thence South 89°02'10" East 87.83 feet; thence North 49°30'21" West 224.79 feet; thence North 72°17'30" East 30.80 feet; thence North 16°45'15" West 50.00 feet; thence South 79°38'59" East 30.31 feet; thence North 61°17'58" East 8.14 feet; thence South 89°13'15" East 147.42 feet to the point of curvature; thence along an arc 64.69 feet to the left, having a radius of 85.00 feet, through a central angle of 43°36'29", the chord of which bears North 68°58'34" West 63.14 feet; thence North 47°10'23" East 180.32 feet; thence North 37°03'08" West 279.53 feet; thence North 48°49'11" East 886.04 feet to the point of Beginning.

Contains 18.53 Acres more or less.



Pilgrims Landing LLC
LESS Pilgrims Landing Plan B 2.189 ac
Pilgrims Landing LLC Remains 18.537 ac

25.727 ac

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LEHI CITY
BROWN
ENGINEERING, INC.

SCALE (FEET)
0 50 100 200 300

MAYFLOWER AVE REGIONAL STORM DRAIN	LEHI CITY	EXHIBIT A
DATE: 10/1/11	DRAWN: J. BROWN	CHECKED: J. BROWN
PROJECT NO: 11-001	CLIENT: LEHI CITY	LOCATION: PILGRIMS LANDING

Exhibit "B"

Lehi City to Traverse Mountain

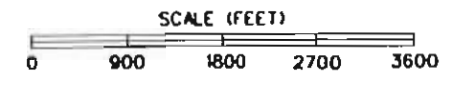
Lot 1, Plat A, Traverse Mountain Subdivision.

Area = 9.455 acres



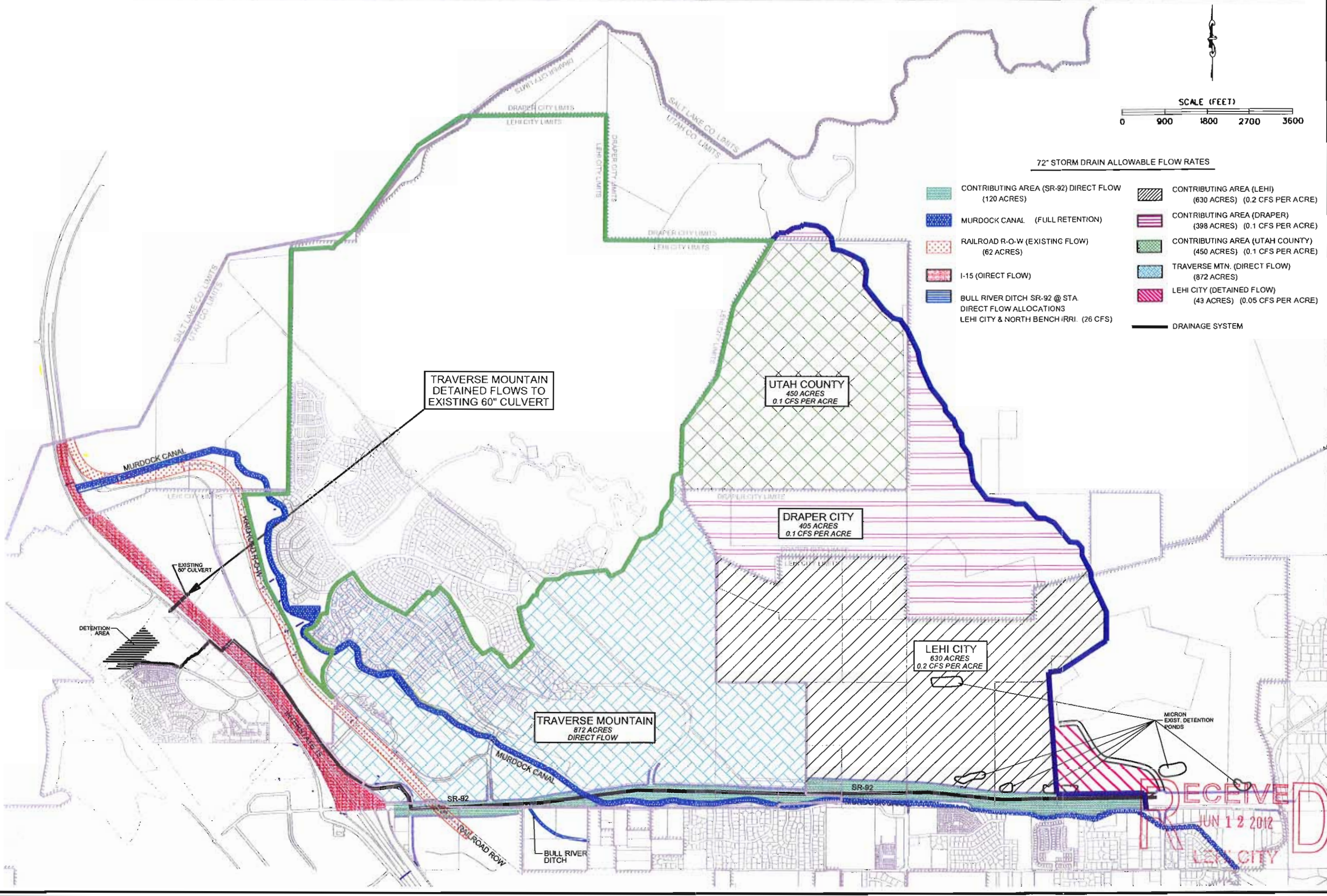
REVISIONS			
No.	Date	By	Name

Designed: J.A. BROWN	Checked: M.W. BROWN	Date: JANUARY 27, 2010
EXHIBIT "A"		
LEHI CITY ALLOWABLE FLOW RATE		
FEBRUARY 2011		
PROJECT NO.	2008-070	
SHEET NO.	1	



72" STORM DRAIN ALLOWABLE FLOW RATES

- | | |
|---|---|
| CONTRIBUTING AREA (SR-92) DIRECT FLOW
(120 ACRES) | CONTRIBUTING AREA (LEHI)
(630 ACRES) (0.2 CFS PER ACRE) |
| MURDOCK CANAL (FULL RETENTION) | CONTRIBUTING AREA (DRAPER)
(398 ACRES) (0.1 CFS PER ACRE) |
| RAILROAD R-O-W (EXISTING FLOW)
(62 ACRES) | CONTRIBUTING AREA (UTAH COUNTY)
(450 ACRES) (0.1 CFS PER ACRE) |
| I-15 (DIRECT FLOW) | TRAVERSE MTN. (DIRECT FLOW)
(872 ACRES) |
| BULL RIVER DITCH SR-92 @ STA.
DIRECT FLOW ALLOCATIONS
LEHI CITY & NORTH BENCH IRRIG. (26 CFS) | LEHI CITY (DETAINED FLOW)
(43 ACRES) (0.05 CFS PER ACRE) |
| | DRAINAGE SYSTEM |



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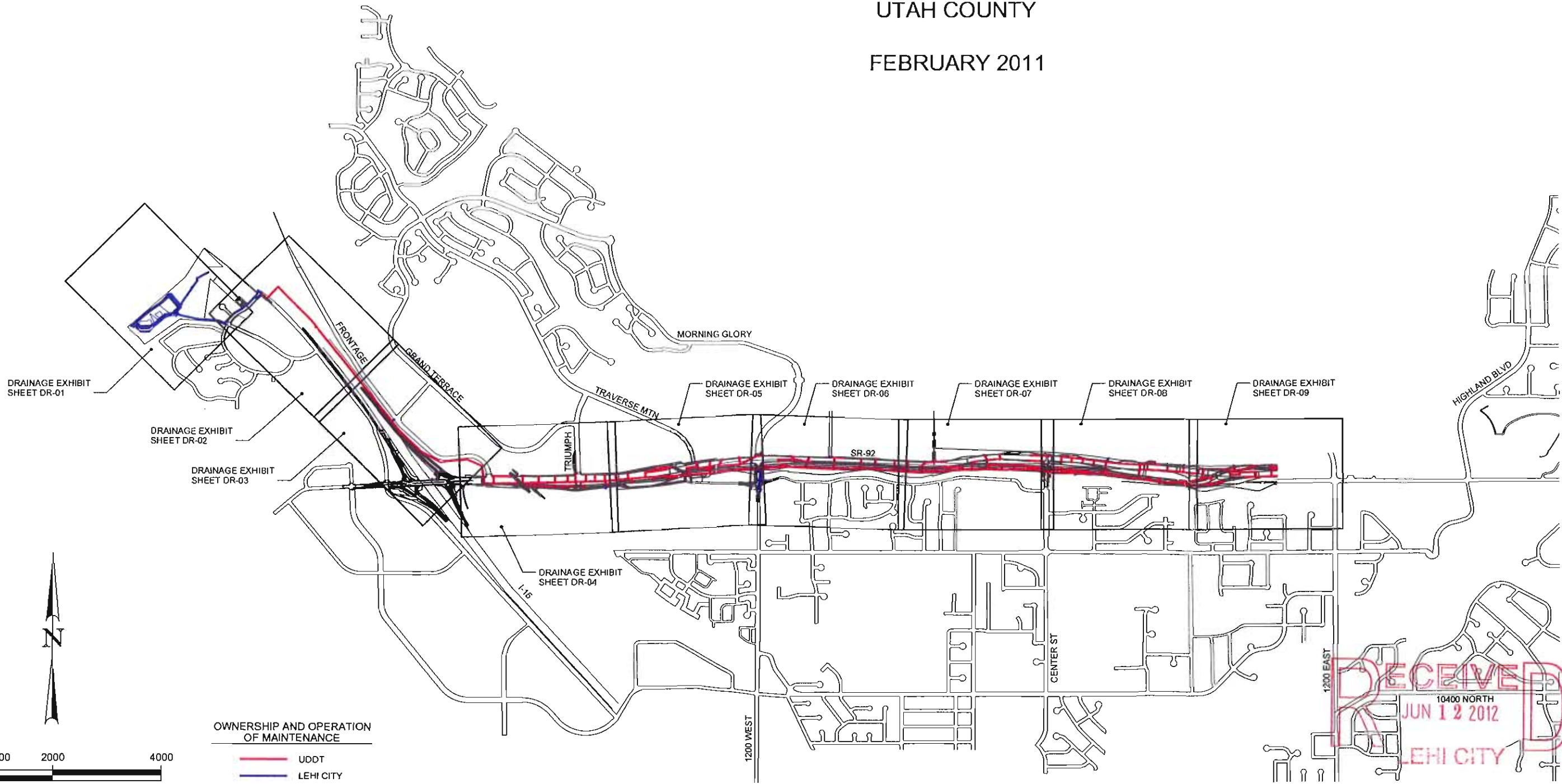
UTAH
DEPARTMENT OF TRANSPORTATION

DRAINAGE AGREEMENT EXHIBIT B

UTAH COUNTY ACCESS MANAGEMENT
SR-92, LEHI TO HIGHLAND

UTAH COUNTY

FEBRUARY 2011



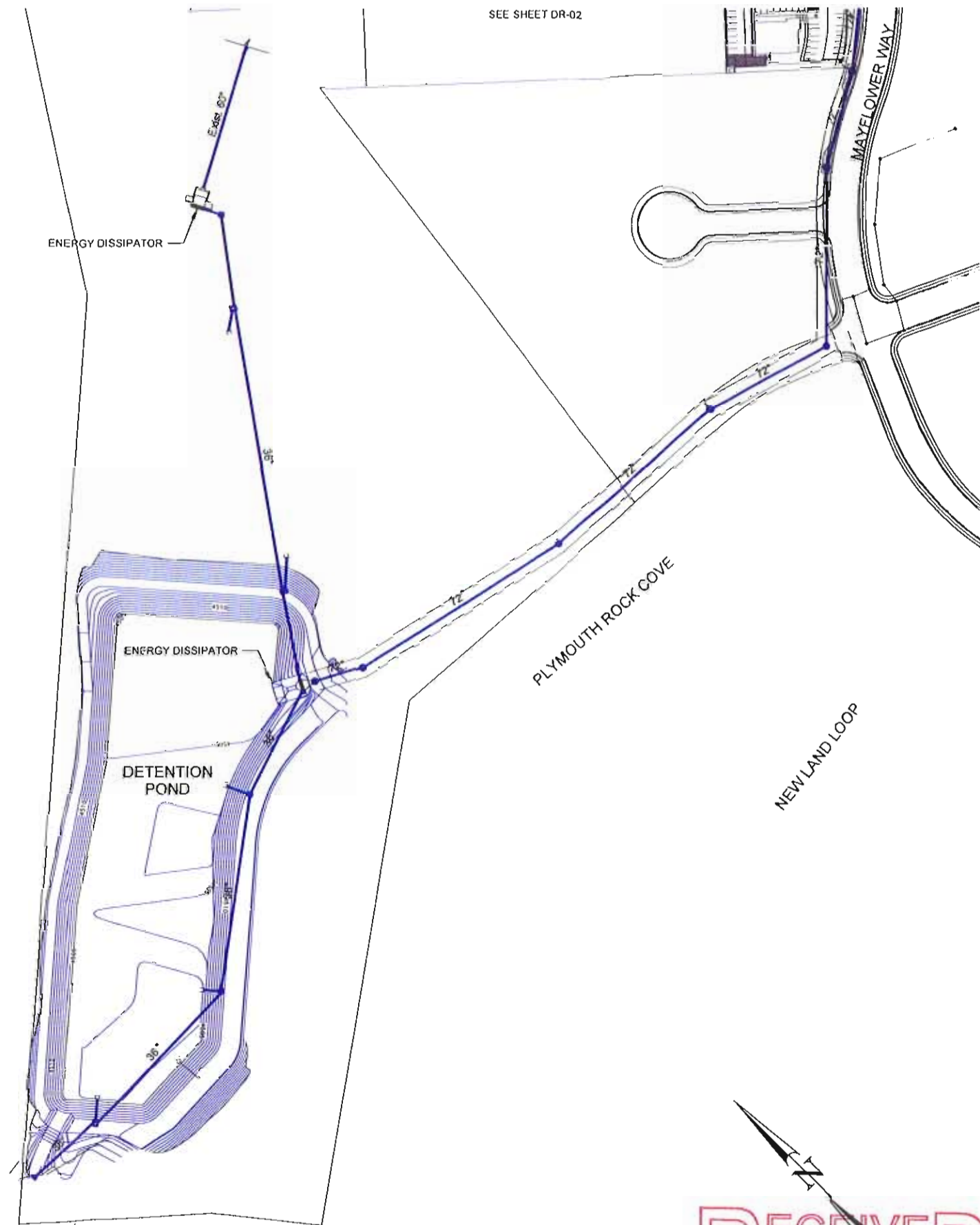
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OWNERSHIP AND OPERATION
OF MAINTENANCE

	UDOT
	LEHI CITY



SEE SHEET DR-02

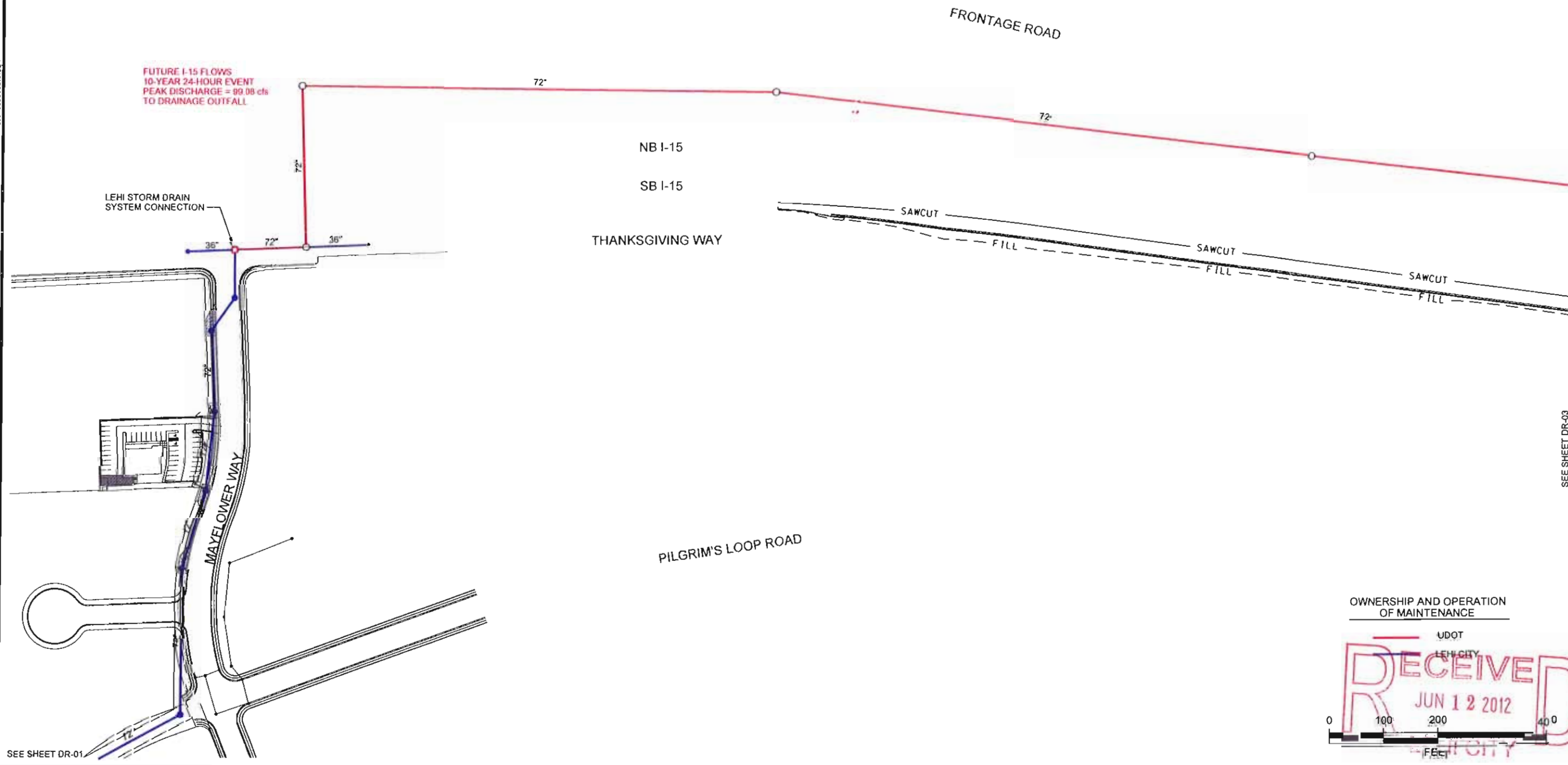


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PROJECT					

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LEHI CITY

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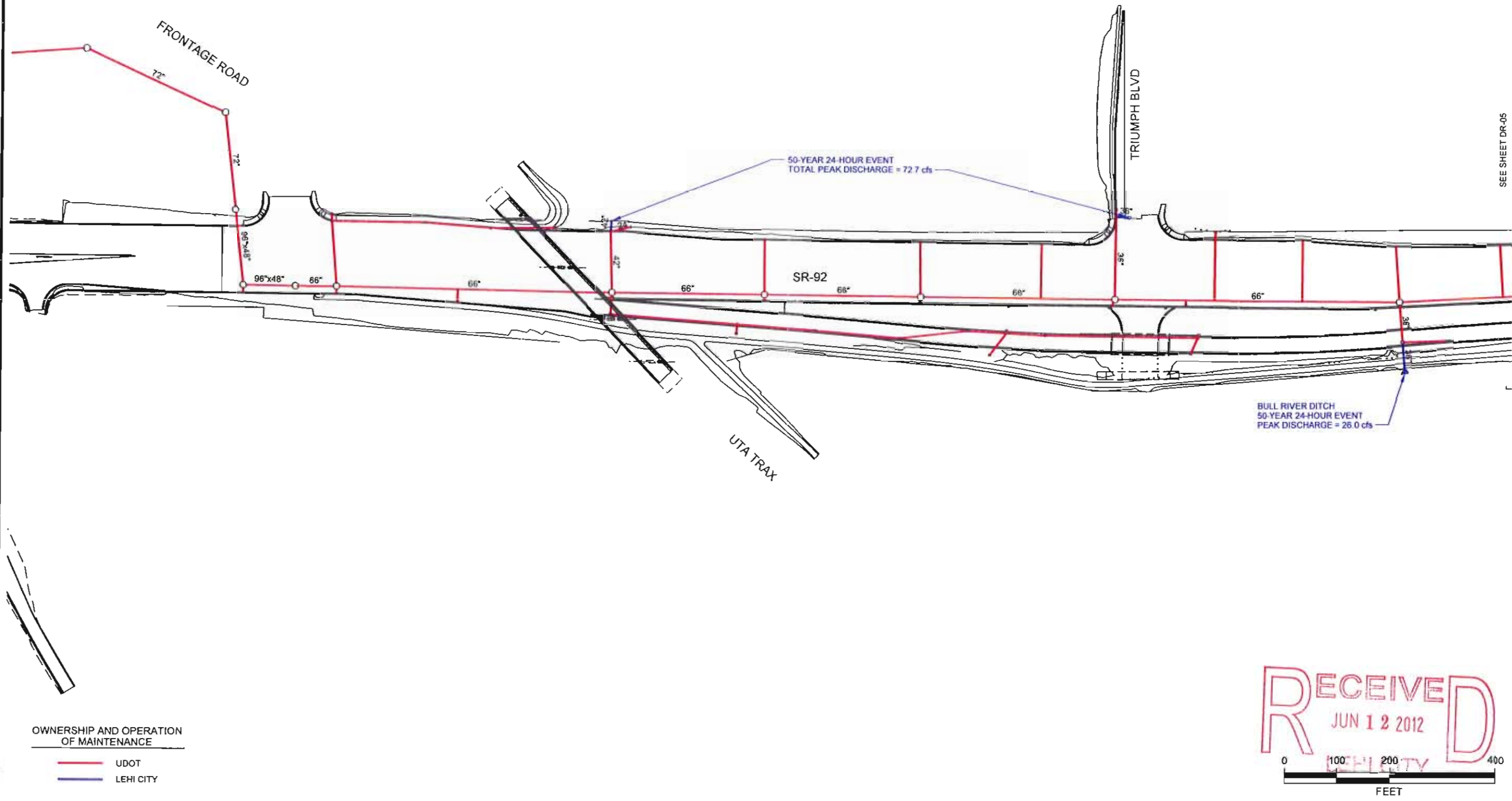
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DRAINAGE EXHIBIT		CHECKED BY	APPROVED		
		PROFESSIONAL ENGINEER	DATE		
		NO.	DATE	APPROVED BY	
				REMARKS	

SEE SHEET DR-01

SEE SHEET DR-03

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SEE SHEET DR-03



SEE SHEET DR-05

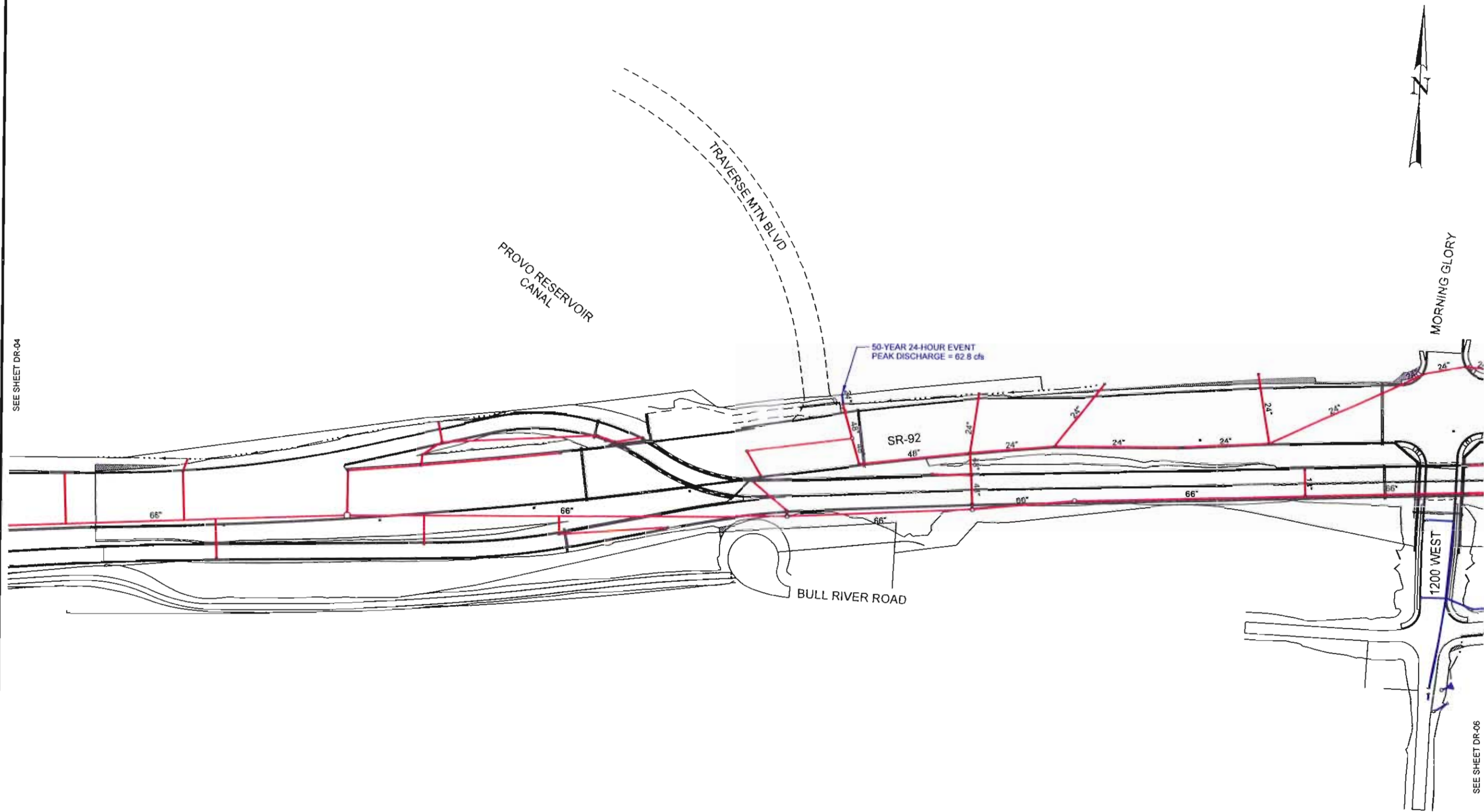


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OWNERSHIP AND OPERATION
OF MAINTENANCE

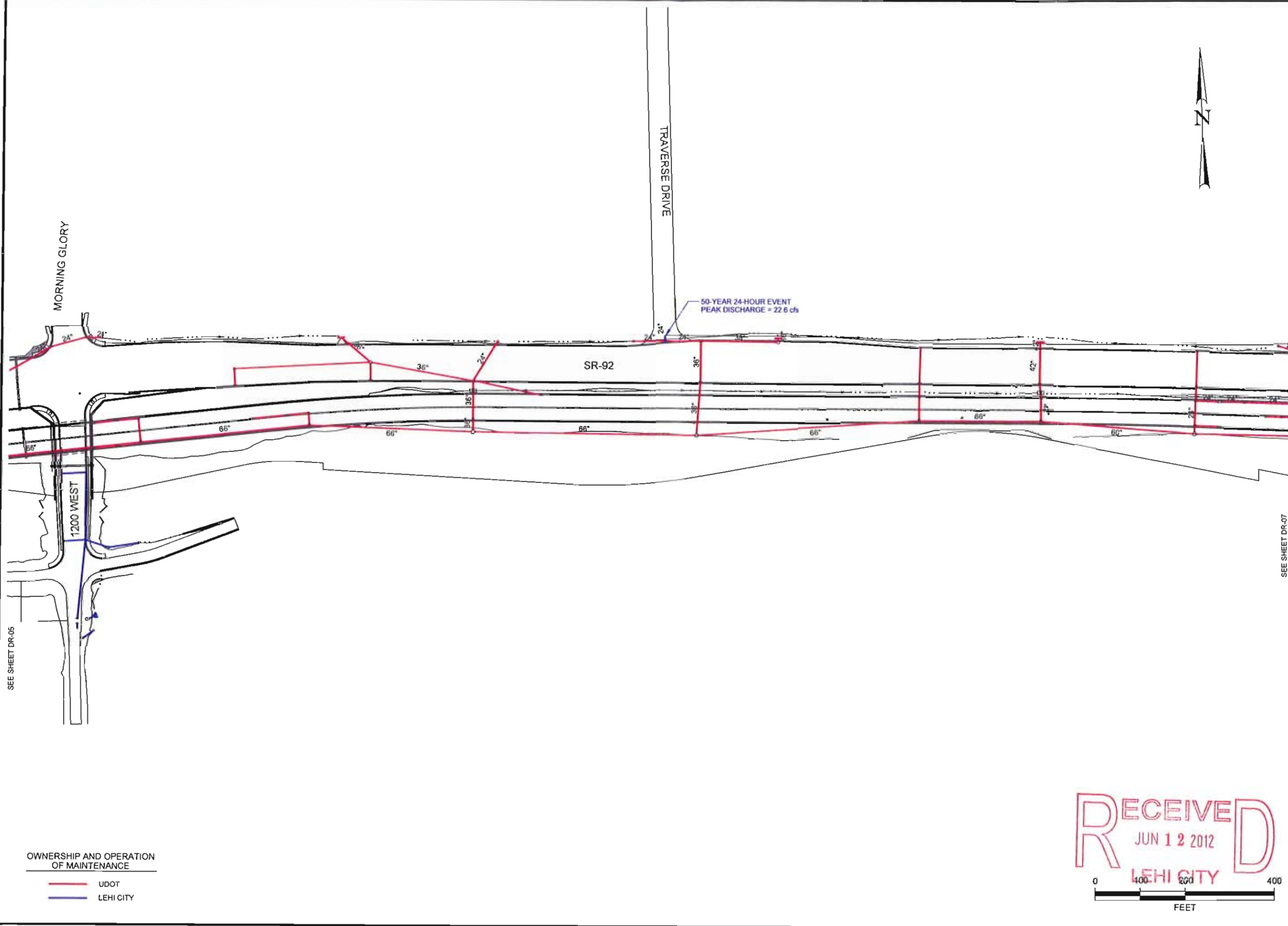
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LEHI CITY



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SEE SHEET DR-05

SEE SHEET DR-07

OWNERSHIP AND OPERATION
OF MAINTENANCE

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UTAH COUNTY ACCESS MANAGEMENT		UTAH DEPARTMENT OF TRANSPORTATION		REVISIONS	
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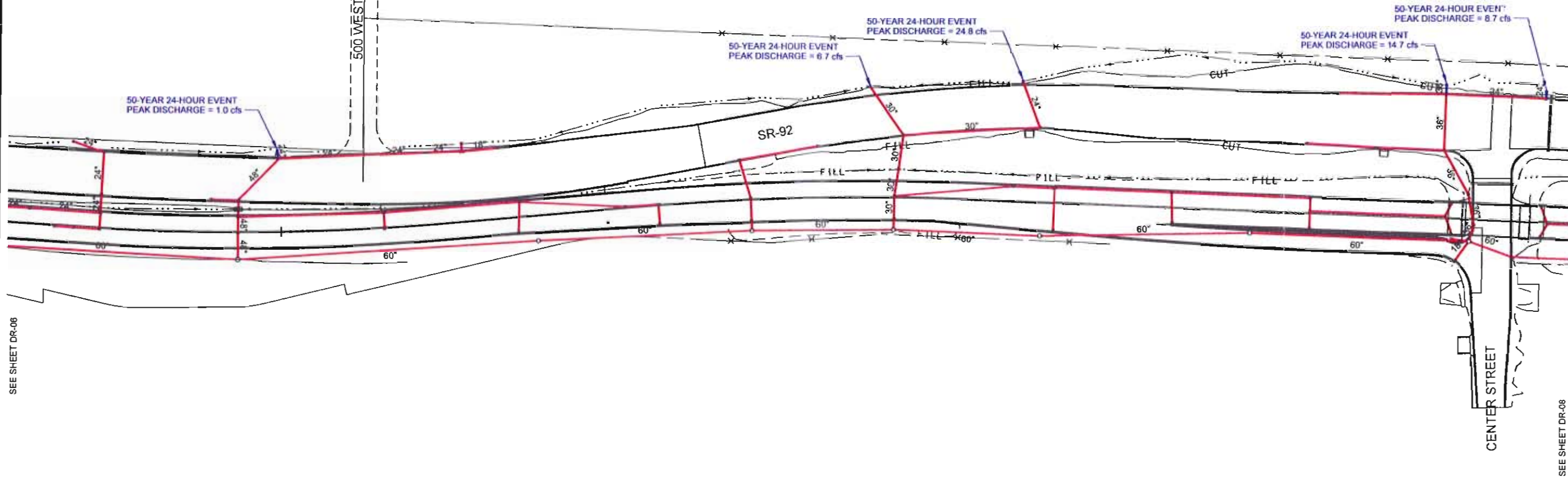
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SEE SHEET DR-06

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SEE SHEET DR-08

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UTAH COUNTY ACCESS MANAGEMENT		UTAH DEPARTMENT OF TRANSPORTATION		REVISIONS	
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SHEET NO. DR-07					

10 YEAR HEC-1

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* MAY 1991
* VERSION 4.0.1E
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* RUN DATE      TIME
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*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

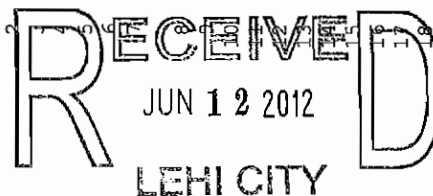
KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

PAGE 1

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LEHI CITY

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LINE

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HEC-1 INPUT

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293	KO	0							
294	BA	0.0660							
295	LS	0.0	61.27	0.0					
296	UD	0.0702							
297	KK	23R	CNAME	23C					
298	KO	0	0	0.0	0	22			
299	RD	1357.8	0.04276	0.013		CIRC	2.0	0.0	
300	KK	140B							
301	KO	0	0	0.0	0	22			
302	BA	0.0475							
303	LS	0.0	67.54	0.0					
304	UD	0.0616							
305	KK	24C	CNAME	24R					
306	KO	0	0	0.0	0	22			
307	HC	2							
308	KK	24R	CNAME	24C					
309	KO	0	0	0.0	0	22			
310	RD	3765.7	0.06856	0.013		CIRC	2.0	0.0	
311	KK	138B							
312	KO	0	0	0.0	0	22			
313	BA	0.1174							
314	LS	0.0	71.23	0.0					
315	UD	0.2069							
316	KK	18C	CNAME	18R					
317	KO	0	0	0.0	0	22			
318	HC	3							
319	KK	18R	CNAME	18C					
320	KO	0	0	0.0	0	22			
321	RD	3528.0	0.04879	0.013		TRAP	2.0	0.0	
322	KK	155B							
323	KO	0	0	0.0	0	22			
324	BA	0.0758							
325	LS	0.0	75.21	0.0					
326	UD	0.1458							
327	KK	149B							
328	KO	0	0	0.0	0	22			
329	BA	0.2020							
330	LS	0.0	80.17	0.0					
331	UD	0.2477							




```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
332      KK      4C      CNAME      4R      0      0      22
333      KO      0
334      HC      2
335      KK      4R      CNAME      4C
336      KO      0      0.0      0      22
337      RS      1      FLOW      0.0      0.0
      * 4C Volume
338      SV      0.00.2728530.5501420.8319091.118195 1.409041.7044872.0045762.3093492.618846
339      SV      2.93313.2521783.5760963.9049024.2386384.5773464.921066 5.269845.6237085.982713
      * 4C Elevation
340      SE      4811.04811.2104811.4214811.6314811.8424812.0524812.2634812.4734812.6844812.894
341      SE      4813.14813.3154813.5264813.7364813.9474814.1574814.3684814.5784814.789 4815.0
      * 4C Discharge
342      SQ      12.76313.3469013.9061714.4438114.9621415.4631015.9483316.4192316.8770017.32267
343      SQ      17.75718.1812818.7378822.8393729.3622537.5566847.1173257.86315 69.670582.44792
      * 4C Elevation
344      SE      4811.04811.2104811.4214811.6314811.8424812.0524812.2634812.4734812.6844812.894
345      SE      4813.14813.3154813.5264813.7364813.9474814.1574814.3684814.5784814.789 4815.0
346      KK      30B
347      KO      0
348      BA      0.1491
349      LS      0.0      74.12      0.0
350      UD      0.2306
351      KK      66B
352      KO      0
353      BA      0.0522
354      LS      0.0      72.0      0.0
355      UD      0.0556
356      KK      11C      CNAME      11R
357      KO      0      0.0      0      22
358      HC      4
359      KK      11R      CNAME      11C
360      KO      0      0.0      0      22
361      RN      11R
362      KK      241B
363      KO      0
364      BA      0.0949
365      LS      0.0      73.24      0.0
366      UD      0.1459
367      KK      10R      CNAME      10C
368      KO      0      0.0      0      22
369      RN      10R

```


[illegible]

RUNOFF SUMMARY

FLOW IN CUBIC FEET PER SECOND TIME IN HOURS, AREA IN SQUARE MILES									
OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD		BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE	
				6-HOUR	24-HOUR	72-HOUR			
+									
+	HYDROGRAPH AT	329B	7.	12.00	1.	0.	0.	0.05	
+	HYDROGRAPH AT	403B	4.	12.00	1.	0.	0.	0.02	
+	2 COMBINED AT	37C	11.	12.00	2.	1.	1.	0.07	
+	ROUTED TO	37R	5.	12.33	2.	1.	1.	0.07	4742.62
+									12.33
+	HYDROGRAPH AT	11B	0.	18.33	0.	0.	0.	0.12	
+	ROUTED TO	6R	0.	18.33	0.	0.	0.	0.12	
+	HYDROGRAPH AT	10B	14.	12.00	3.	1.	1.	0.16	
+	2 COMBINED AT	13C	14.	12.00	3.	1.	1.	0.28	
+	ROUTED TO	13R	2.	14.00	2.	1.	1.	0.28	4800.34
+									14.00
+	HYDROGRAPH AT	98B	1.	12.33	1.	0.	0.	0.11	
+	ROUTED TO	29R	1.	12.33	1.	0.	0.	0.11	
+	HYDROGRAPH AT	408B	2.	12.00	1.	0.	0.	0.08	
+	HYDROGRAPH AT	99B	19.	12.00	2.	1.	1.	0.06	
+	2 COMBINED AT	30C	21.	12.00	3.	1.	1.	0.25	
+	HYDROGRAPH AT	103B	4.	12.17	1.	0.	0.	0.01	
+	HYDROGRAPH AT	401B	18.	12.17	3.	1.	1.	0.14	



+	3 COMBINED AT	32C	37.	12.00	7.	3.	3.	0.40
+	HYDROGRAPH AT	101B	1.	12.33	1.	0.	0.	0.11
+	ROUTED TO	31R	1.	12.33	1.	0.	0.	0.11
+	HYDROGRAPH AT	83B	1.	17.83	1.	0.	0.	0.57
+	ROUTED TO	19R	1.	17.83	1.	0.	0.	0.57
+	HYDROGRAPH AT	86B	4.	12.00	1.	0.	0.	0.03
+	2 COMBINED AT	21C	4.	12.00	1.	0.	0.	0.59
+	HYDROGRAPH AT	85B	1.	12.50	1.	0.	0.	0.16
+	2 COMBINED AT	16C	5.	12.00	2.	1.	1.	0.75
+	HYDROGRAPH AT	81B	0.	17.83	0.	0.	0.	0.19
+	ROUTED TO	17R	0.	17.83	0.	0.	0.	0.19
+	HYDROGRAPH AT	84B	4.	12.00	1.	0.	0.	0.12
+	3 COMBINED AT	20C	9.	12.00	3.	1.	1.	1.06
+	HYDROGRAPH AT	79B	1.	12.00	0.	0.	0.	0.02
+	ROUTED TO	15R	1.	12.00	0.	0.	0.	0.02
+	HYDROGRAPH AT	78B	0.	13.50	0.	0.	0.	0.08
+	2 COMBINED AT	8C	1.	12.00	0.	0.	0.	0.09
+	HYDROGRAPH AT	87B	1.	12.00	1.	0.	0.	0.06
+	2 COMBINED AT	22C	2.	12.00	1.	0.	0.	0.16
+	HYDROGRAPH AT	77B	0.	12.83	0.	0.	0.	0.06

+	3 COMBINED AT	7C	11.	12.00	4.	2.	2.	1.27
+	HYDROGRAPH AT	177B	0.	12.33	0.	0.	0.	0.02
+	HYDROGRAPH AT	248B	2.	12.00	1.	0.	0.	0.08
+	HYDROGRAPH AT	176B	3.	12.00	0.	0.	0.	0.02
+	5 COMBINED AT	41C	16.	12.00	6.	2.	2.	1.51
+	HYDROGRAPH AT	286B	41.	12.00	7.	2.	2.	0.42
+	HYDROGRAPH AT	181B	8.	12.00	1.	0.	0.	0.03
+	3 COMBINED AT	43C	65.	12.00	14.	5.	5.	1.96
+	HYDROGRAPH AT	2B	18.	12.17	4.	1.	1.	0.08
+	ROUTED TO	38R	18.	12.17	4.	1.	1.	0.08
+	HYDROGRAPH AT	405B	3.	12.00	0.	0.	0.	0.01
+	HYDROGRAPH AT	288B	5.	12.00	1.	0.	0.	0.01
+	4 COMBINED AT	44C	83.	12.00	18.	6.	6.	2.06
+	HYDROGRAPH AT	415B	27.	12.00	3.	1.	1.	0.08
+	HYDROGRAPH AT	459B	42.	12.00	7.	2.	2.	0.18
+	4 COMBINED AT	3C	190.	12.00	36.	12.	12.	2.72
+	HYDROGRAPH AT	163B	21.	12.00	3.	1.	1.	0.06
+	HYDROGRAPH AT	7B	1.	12.00	0.	0.	0.	0.04
+	HYDROGRAPH AT	411B	11.	12.00	1.	0.	0.	0.03
+	4 COMBINED AT							



+		12C	224.	12.00	40.	14.	14.	2.86
	ROUTED TO							
+		12R	224.	12.00	40.	14.	14.	2.86
	HYDROGRAPH AT							
+		141B	8.	12.17	2.	1.	1.	0.16
	ROUTED TO							
+		25R	8.	12.17	2.	1.	1.	0.16
	HYDROGRAPH AT							
+		139B	0.	13.33	0.	0.	0.	0.07
	ROUTED TO							
+		23R	0.	13.33	0.	0.	0.	0.07
	HYDROGRAPH AT							
+		140B	2.	12.00	0.	0.	0.	0.05
	2 COMBINED AT							
+		24C	2.	12.00	1.	0.	0.	0.11
	ROUTED TO							
+		24R	2.	12.17	1.	0.	0.	0.11
	HYDROGRAPH AT							
+		138B	8.	12.17	2.	1.	1.	0.12
	3 COMBINED AT							
+		18C	18.	12.17	5.	2.	2.	0.39
	ROUTED TO							
+		18R	16.	12.17	5.	2.	2.	0.39
	HYDROGRAPH AT							
+		155B	11.	12.00	2.	1.	1.	0.08
	HYDROGRAPH AT							
+		149B	46.	12.17	8.	3.	3.	0.20
	2 COMBINED AT							
+		4C	57.	12.17	10.	3.	3.	0.28
	ROUTED TO							
+		4R	16.	12.83	14.	13.	13.	0.28
+							4812.09	12.83
	HYDROGRAPH AT							
+		30B	17.	12.17	3.	1.	1.	0.15
	HYDROGRAPH AT							
+		66B	7.	12.00	1.	0.	0.	0.05
	4 COMBINED AT							
+		11C	50.	12.17	23.	16.	16.	0.87
	ROUTED TO							
+		11R	50.	12.17	23.	16.	16.	0.87

+	HYDROGRAPH AT	241B	10.	12.17	2.	1.	1.	0.09	
+	ROUTED TO	10R	10.	12.17	2.	1.	1.	0.09	
+	HYDROGRAPH AT	151B	2.	12.00	0.	0.	0.	0.01	
+	HYDROGRAPH AT	150B	16.	12.00	2.	1.	1.	0.05	
+	2 COMBINED AT	35C	17.	12.00	2.	1.	1.	0.06	
+	ROUTED TO	35R	5.	0.17	5.	5.	5.	0.06	0.00
								4815.00	
+	HYDROGRAPH AT	143B	7.	12.00	1.	0.	0.	0.04	
+	HYDROGRAPH AT	402B	3.	12.00	0.	0.	0.	0.02	
+	2 COMBINED AT	33C	10.	12.00	1.	0.	0.	0.06	
+	ROUTED TO	33R	5.	0.17	5.	5.	5.	0.06	12.17
								4810.01	
+	HYDROGRAPH AT	407B	3.	12.00	0.	0.	0.	0.02	
+	HYDROGRAPH AT	406B	1.	12.00	0.	0.	0.	0.03	
+	HYDROGRAPH AT	358B	1.	12.00	0.	0.	0.	0.01	
+	2 COMBINED AT	54C	15.	12.00	11.	10.	10.	0.17	
+	HYDROGRAPH AT	344B	8.	12.00	1.	0.	0.	0.04	
+	HYDROGRAPH AT	363B	4.	12.00	1.	0.	0.	0.02	
+	2 COMBINED AT	9C	26.	12.00	12.	11.	11.	0.23	
+	ROUTED TO	9R	26.	12.00	12.	11.	11.	0.23	

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)



ISTAQ	ELEMENT	DT	PEAK (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	DT	INTERPOLATED TO			VOLUME
								COMPUTATION	INTERVAL	TIME TO PEAK	
25R	MANE	1.26	8.21	10.00	731.71	0.16	10.00	7.92	730.00	0.16	
FOR STORM = 1 STORM AREA (SQ MI) = 10.00 CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1336E+01 EXCESS=0.0000E+00 OUTFLOW=0.1334E+01 BASIN STORAGE=0.2259E-02 PERCENT ERROR= 0.0											
23R	MANE	3.29	0.24	10.00	806.43	0.04	10.00	0.24	810.00	0.04	
FOR STORM = 1 STORM AREA (SQ MI) = 10.00 CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1403E+00 EXCESS=0.0000E+00 OUTFLOW=0.1395E+00 BASIN STORAGE=0.7757E-03 PERCENT ERROR= 0.0											
24R	MANE	0.50	1.83	10.00	725.50	0.07	10.00	1.56	730.00	0.07	
FOR STORM = 1 STORM AREA (SQ MI) = 10.00 CONTINUITY SUMMARY (AC-FT) - INFLOW=0.4467E+00 EXCESS=0.0000E+00 OUTFLOW=0.4434E+00 BASIN STORAGE=0.3500E-02 PERCENT ERROR= 0.0											
18R	MANE	2.00	17.70	10.00	734.00	0.14	10.00	16.22	730.00	0.14	
FOR STORM = 1 STORM AREA (SQ MI) = 10.00 CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2969E+01 EXCESS=0.0000E+00 OUTFLOW=0.2956E+01 BASIN STORAGE=0.2097E-01 PERCENT ERROR= -0.2											

*** NORMAL END OF HEC-1 ***

50 YEAR HEC-1

RECEIVED
JUN 12 2012
LEHI CITY

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*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* MAY 1991
* VERSION 4.0.1E
*
* RUN DATE      TIME
*
*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
*
*****

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X X X X' X XX
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X X X X' X X XXX
X X XXXXXXX XXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
 THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

LINE	ID	1	2	3	4	5	6	7	8	9	10	
1	ID	HEC-1 Analysis using WMS										
2	ID	50 year developed flow										
3	ID	MAY 2012										
4	IT	10	07	MAY	09	0	130					
5	IO	5										
6	IN	6	07	MAY	09	0						
7	JD	2.3	10.0									
	* typeII-24hour											
8	PC	0.0	0.001	0.002	0.0031	0.0041	0.0051	0.0062	0.0073	0.0083	0.0094	
9	PC	0.0105	0.0116	0.0127	0.0138	0.015	0.0161	0.0173	0.0185	0.0196	0.0208	
10	PC	0.022	0.0232	0.0244	0.0256	0.0269	0.0281	0.0294	0.0307	0.0319	0.0332	
11	PC	0.0345	0.0358	0.0371	0.0384	0.0398	0.0411	0.0425	0.0439	0.0452	0.0466	



HEC-1 INPUT

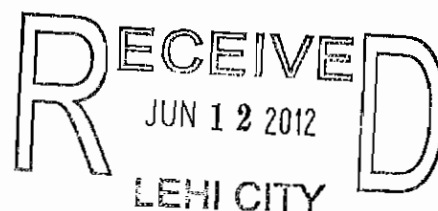
LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10	37R	CNAME	37C	37C Volume
46	KK	0	0	0.0	22
47	KO	0	0	0.0	22
48	RS	1	FLOW	0.0	0.0
49	SV	0.00.1266630.253327	0.379990.5066530.633316	0.759980.8866431.0133061	1.39969
50	SV	1.26661.3932961.5199591.6466221.7732861.8999492.0266122.1532752.2799392.406602			
51	SE	4742.04742.4214742.8424743.2634743.6844744.1054744.5264744.9474745.3684745.789			
52	SE	4746.24746.6314747.0524747.4734747.8944748.3154748.7364749.1574749.578			4750.0
53	SQ	0.02.197453	8.3679616.4140423.1448215.9029218.6881421.1090223.2794925.26417		
54	SQ	27.10328.8264930.4517731.9946033.4663734.8761036.2310137.5370538.7991540.02147			
55	SE	4742.04742.4214742.8424743.2634743.6844744.1054744.5264744.9474745.3684745.789			
56	SE	4746.24746.6314747.0524747.4734747.8944748.3154748.7364749.1574749.578			4750.0
57	KK	11B			
58	KO	0	0	0.0	22
59	BA	0.1161			
60	LS	0.0	57.0	0.0	
61	UD	0.0767			
62	KK	6R	CNAME	6C	
63	KO	0	0	0.0	22
64	RN	6R			
65	KK	10B			
66	KO	0	0	0.0	22
67	BA	0.1616			
68	LS	0.0	71.74	0.0	
69	UD	0.1283			
70	KK	13C	CNAME	13R	
71	KO	0	0	0.0	22
72	HC	2			
73	KK	13R	CNAME	13C	
74	KO	0	0	0.0	22
75	RS	1	FLOW	0.0	0.0
76	SV	0.00.9742581.9639382.969202	3.990215.0271236.0801017.1493058.2348969.337034		
77	SV	10.45511.5915912.7443313.9142715.1015516.3063517.5288218.7691220.0274121.30386			
78	SE	4800.04800.5264801.0524801.5784802.1054802.6314803.1574803.6844804.2104804.736			
79	SE	4805.24805.7894806.3154806.8424807.3684807.8944808.4214808.9474809.473			4810.0

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80	* 13C Discharge	
81	SQ	0.03.42952912.3279421.8209515.9029219.3218222.2207724.7829127.1039229.24128
	SQ	31.23233.1045734.8761036.5618938.1733239.7194241.2075542.6437844.0331945.38008
	* 13C Elevation	
82	SE	4800.04800.5264801.0524801.5784802.1054802.6314803.1574803.6844804.2104804.736
83	SE	4805.24805.7894806.3154806.8424807.3684807.8944808.4214808.9474809.473 4810.0

ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

LINE	ID.....1.....2.....3.....4.....5.
84	KK 98B
85	KO 0
86	BA 0.1097
87	LS 0.0
88	UD 0.0812
89	KK 29R CNAME 29C
90	KO 0
91	RN 29R
92	KK 408B
93	KO 0
94	BA 0.0830
95	LS 0.0
96	UD 0.1008
97	KK 99B
98	KO 0
99	BA 0.0594
100	LS 0.0
101	UD 0.0694
102	KK 30C CNAME 30R
103	KO 0
104	HC 3
105	KK 103B
106	KO 0
107	BA 0.0102
108	LS 0.0
109	UD 0.1933
110	KK 401B
111	KO 0
112	BA 0.1360
113	LS 0.0
114	UD 0.1917
115	KK 32C CNAME 32R
116	KO 0
117	HC 3
118	KK 101B
119	KO 0
120	BA 0.1138

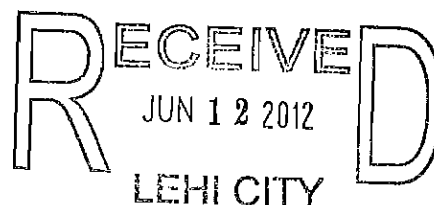


121	LS	0.0	64.94	0.0		
122	UD	0.1459				
123	KK	31R	CNAME	31C		
124	KO	0	0	0.0	0	22
125	RN	31R				

163	KK	20C	CNAME	20R	0	22
164	KQ	0	0	0.0		
165	HC	3				

ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

LINE	ID.....1.....2.....3.....4.....5.
166	KK 79B
167	KO 0
168	BA 0.0165
169	LS 0.0
170	UD 0.0556
171	KK 15R CNAME
172	KO 0
173	RN 15R
174	KK 78B
175	KO 0
176	BA 0.0764
177	LS 0.0
178	UD 0.0556
179	KK 8C
180	KO 0
181	HC 2
182	KK 87B
183	KO 0
184	BA 0.0637
185	LS 0.0
186	UD 0.0556
187	KK 22C CNAME
188	KO 0
189	HC 2
190	KK 77B
191	KO 0
192	BA 0.0564
193	LS 0.0
194	UD 0.0556
195	KK 7C CNAME
196	KO 0
197	HC 3
198	KK 177B
199	KO 0
200	BA 0.0215
201	LS 0.0
202	UD 0.0320



203	KK	246B				
204	KO	0	0	0.0	0	22
205	BA	0.0832				
206	LS	0.0	66.07	0.0		
207	UD	0.0813				

HEC-1 INPUT

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10	176B	0	0.0	0	22
208	KK	176B	0	0.0	0	22
209	KO	0				
210	BA	0.0174				
211	LS	0.0	75.39	0.0		
212	UD	0.1412				
213	KK	41C	CNAME	41R		
214	KO	0	0	0.0	0	22
215	HC	5				
216	KK	286B				
217	KO	0	0	0.0	1	22
218	BA	0.4184				
219	LS	0.0	70.78	0.0		
220	UD	0.0268				
221	KK	181B				
222	KO	0	0	0.0	1	22
223	BA	0.0313				
224	LS	0.0	77.05	0.0		
225	UD	0.0991				
226	KK	43C	CNAME	43R		
227	KO	0	0	0.0	0	22
228	HC	3				
229	KK	2B				
230	KO	0	0	0.0	1	22
231	BA	0.0817				
232	LS	0.0	81.16	0.0		
233	UD	0.3103				
234	KK	38R	CNAME	38C		
235	KO	0	0	0.0	0	22
236	RN	38R				
237	KK	405B				
238	KO	0	0	0.0	1	22
239	BA	0.0092				
240	LS	0.0	80.21	0.0		
241	UD	0.0730				
242	KK	288B				
243	KO	0	0	0.0	1	22
244	BA	0.0149				



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LS	0.0	78.34	0.0	
UD	0.0664			
KK	44C	CNAME	44R	
KO	0	0	0.0	22
HC	4		0	

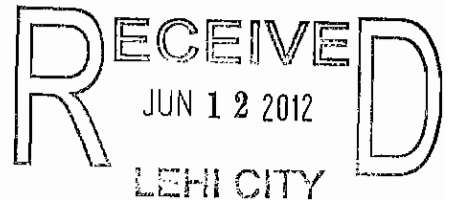
287	LS	0.0	69.57	0.0				
288	UD	0.1866						
289	KK	25R	CNAME	25C				
290	KO	0	0	0.0				
291	RD	1297.6	0.07153	0.013	0	22	0.0	0.0
						CIRC	2.0	

HEC-1 INPUT

ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

LINE

292	KK	139B	0	0.0	0	22			
293	KO	0							
294	BA	0.0660							
295	LS	0.0	61.27	0.0					
296	UD	0.0702							
297	KK	23R	CNAME	23C					
298	KO	0	0	0.0	0	22			
299	RD	1357.8	0.04276	0.013		CIRC	2.0	0.0	
300	KK	140B							
301	KO	0		0.0	0	22			
302	BA	0.0475							
303	LS	0.0	67.54	0.0					
304	UD	0.0616							
305	KK	24C	CNAME	24R					
306	KO	0	0	0.0	0	22			
307	HC	2							
308	KK	24R	CNAME	24C					
309	KO	0	0	0.0	0	22			
310	RD	3765.7	0.06856	0.013		CIRC	2.0	0.0	
311	KK	138B							
312	KO	0		0.0	0	22			
313	BA	0.1174							
314	LS	0.0	71.23	0.0					
315	UD	0.2069							
316	KK	18C	CNAME	18R					
317	KO	0	0	0.0	0	22			
318	HC	3							
319	KK	18R	CNAME	18C					
320	KO	0	0	0.0	0	22			
321	RD	3528.0	0.04879	0.013		TRAP	2.0	0.0	
322	KK	155B							
323	KO	0		0.0	0	22			
324	BA	0.0758							
325	LS	0.0	75.21	0.0					
326	UD	0.1458							
327	KK	149B							



328	KO	0	0	0.0	0	22
329	BA	0.2020				
330	LS	0.0	80.17	0.0		
331	UD	0.2477				

HEC-1 INPUT

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
332	KK 4C CNAME 4R 0 0.0 0 22
333	KO 0 0 0.0 0 22
334	HC 2
335	KK 4R CNAME 4C 0 0.0 0 22
336	KO 0 0 0.0 0 22
337	RS 1 FLOW 0.0 0.0
338	* 4C Volume
339	SV 0.00.2728530.5501420.8319091.118195 1.409041.7044872.0045762.3093492.618846
340	SV 2.93313.2521783.5760963.9049024.2386384.5773464.921066 5.269845.6237085.982713
341	* 4C Elevation
342	SE 4811.04811.2104811.4214811.6314811.8424812.0524812.2634812.4734812.6844812.894
343	SE 4813.14813.3154813.5264813.7364813.9474814.1574814.3684814.5784814.789 4815.0
344	* 4C Discharge
345	SQ 12.76313.3469013.9061714.4438114.9621415.4631015.9483316.4192316.8770017.32267
346	SQ 17.75718.1812818.7378822.8393729.3622537.5566847.1173257.86315 69.670582.44792
347	* 4C Elevation
348	SE 4811.04811.2104811.4214811.6314811.8424812.0524812.2634812.4734812.6844812.894
349	SE 4813.14813.3154813.5264813.7364813.9474814.1574814.3684814.5784814.789 4815.0
350	KK 30B 0 0.0 0 22
351	KO 0 0 0.0 0 22
352	BA 0.1491 74.12 0.0
353	LS 0.0 72.0 0.0
354	UD 0.2306
355	KK 66B 0 0.0 0 22
356	KO 0 0 0.0 0 22
357	BA 0.0522 72.0 0.0
358	LS 0.0 72.0 0.0
359	UD 0.0556
360	KK 11C CNAME 11R 0 0.0 0 22
361	KO 0 0 0.0 0 22
362	HC 4
363	KK 11R CNAME 11C 0 0.0 0 22
364	KO 0 0 0.0 0 22
365	RN 11R
366	KK 241B 0 0.0 0 22
	KO 0 0 0.0 0 22
	BA 0.0949 73.24 0.0
	LS 0.0 73.24 0.0
	UD 0.1459



367	KK	10R	CNAME	10C	
368	KC	0	0	0.0	0
369	KN	10R			22

HEC-1 INPUT

ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

LINE

370	KK	151B																		
371	KO	0																		
372	BA	0.0132																		
373	LS	0.0	72.23	0.0																
374	UD	0.0337																		
375	KK	150B																		
376	KO	0																		
377	BA	0.0461																		
378	LS	0.0	79.46	0.0																
379	UD	0.0407																		
380	KK	35C	CNAME	35R																
381	KO	0	0	0.0																
382	HC	2																		
383	KK	35R	CNAME	35C																
384	KO	0	0	0.0																
385	RS	1	FLOW	0.0																
386	SV	1.0	2.0	3.0	4.0	5.0	6.0	7.0	8.0	9.0	10.0									
387	SE	4815.0	4816.0	4817.0	4818.0	4819.0	4820.0	4821.0	4822.0	4823.0	4824.0									
388	SQ	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0									
389	SE	4815.0	4816.0	4817.0	4818.0	4819.0	4820.0	4821.0	4822.0	4823.0	4824.0									
390	KK	143B																		
391	KO	0	0	0.0																
392	BA	0.0414																		
393	LS	0.0	74.0	0.0																
394	UD	0.0120																		
395	KK	402B																		
396	KO	0	0	0.0																
397	BA	0.0153																		
398	LS	0.0	74.0	0.0																
399	UD	0.0514																		
400	KK	33C	CNAME	33R																
401	KO	0	0	0.0																
402	HC	2																		
403	KK	33R	CNAME	33C																

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404	KO	0	0	0.0	0	22			
405	RS	1	FLOW	0.0	0.0				
	* 33C Volume								
406	SV	0.0	1.0	2.0	3.0	4.0	5.0	6.0	7.0 8.0 9.0
	* 33C Elevation								
407	SE	4810.0	4811.0	4812.0	4813.0	4814.0	4815.0	4816.0	4817.0 4818.0 4819.0
	* 33C Discharge								
408	SQ	5.0	5.0	5.0	5.0	5.0	5.0	5.0	5.0 5.0
	* 33C Elevation								

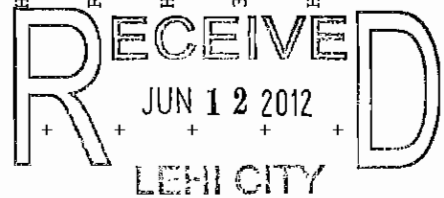
HEC-1 INPUT

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10	4810.0	4811.0	4812.0	4813.0	4814.0	4815.0	4816.0	4817.0	4818.0	4819.0
409	SE	4810.0	4811.0	4812.0	4813.0	4814.0	4815.0	4816.0	4817.0	4818.0	4819.0
410	KK 407B	0	0	0.0	0	22					
411	KO	0									
412	BA 0.0182										
413	LS 0.0	74.0	0.0								
414	UD 0.0532										
415	KK 406B	0	0	0.0	0	22					
416	KO	0									
417	BA 0.0256										
418	LS 0.0	68.46	0.0								
419	UD 0.0717										
420	KK 358B	0	0	0.0	0	22					
421	KO	0									
422	BA 0.0053										
423	LS 0.0	72.0	0.0								
424	UD 0.0822										
425	KK 54C	CNAME	54R								
426	KO	0	0.0	0	0	22					
427	HC	5									
428	KK 344B	0	0	0.0	0	22					
429	KO	0									
430	BA 0.0449										
431	LS 0.0	73.99	0.0								
432	UD 0.0895										
433	KK 363B	0	0	0.0	0	22					
434	KO	0									
435	BA 0.0208										
436	LS 0.0	75.76	0.0								
437	UD 0.1262										
438	KK 9C	CNAME	9R								
439	KO	0	0.0	0	0	22					
440	HC	3									
441	KK 9R	CNAME	9C								
442	KO	0	0.0	0	0	22					
443	RN 9R										
444	ZZ										

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RUNOFF SUMMARY							
FLOW IN CUBIC FEET PER SECOND							
TIME IN HOURS, AREA IN SQUARE MILES							
OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA
				6-HOUR	24-HOUR	72-HOUR	MAXIMUM STAGE
							TIME OF MAX STAGE
+							
	HYDROGRAPH AT						
+	329B	17.	12.00	2.	1.	1.	0.05
	HYDROGRAPH AT						
+	403B	9.	12.00	1.	0.	0.	0.02
	2 COMBINED AT						
+	37C	26.	12.00	3.	1.	1.	0.07
	ROUTED TO						
+	37R	15.	12.17	3.	1.	1.	0.07
+							4743.20
	HYDROGRAPH AT						12.17
+	11B	1.	12.50	1.	0.	0.	0.12
	ROUTED TO						
+	6R	1.	12.50	1.	0.	0.	0.12
	HYDROGRAPH AT						
+	10B	40.	12.00	6.	2.	2.	0.16
	2 COMBINED AT						
+	13C	40.	12.00	7.	2.	2.	0.28
	ROUTED TO						
+	13R	7.	13.00	5.	2.	2.	0.28
+							4800.75
	HYDROGRAPH AT						13.00
+	98B	12.	12.00	2.	1.	1.	0.11
	ROUTED TO						
+	29R	12.	12.00	2.	1.	1.	0.11
	HYDROGRAPH AT						
+	408B	11.	12.00	2.	1.	1.	0.08
	HYDROGRAPH AT						
+	99B	34.	12.00	4.	1.	1.	0.06
	3 COMBINED AT						

+		30C	57.	12.00	8.	3.	3.	0.25
	HYDROGRAPH AT							
+		103B	6.	12.17	1.	0.	0.	0.01
	HYDROGRAPH AT							
+		401B	39.	12.17	7.	2.	2.	0.14
	3 COMBINED AT							
+		32C	96.	12.00	15.	5.	5.	0.40
	HYDROGRAPH AT							
+		101B	9.	12.17	2.	1.	1.	0.11
	ROUTED TO							
+		31R	9.	12.17	2.	1.	1.	0.11
	HYDROGRAPH AT							
+		83B	7.	12.33	4.	2.	2.	0.57
	ROUTED TO							
+		19R	7.	12.33	4.	2.	2.	0.57
	HYDROGRAPH AT							
+		86B	10.	12.00	1.	0.	0.	0.03
	2 COMBINED AT							
+		21C	13.	12.00	5.	2.	2.	0.59
	HYDROGRAPH AT							
+		85B	13.	12.00	3.	1.	1.	0.16
	2 COMBINED AT							
+		16C	26.	12.00	8.	3.	3.	0.75
	HYDROGRAPH AT							
+		81B	2.	12.33	1.	1.	1.	0.19
	ROUTED TO							
+		17R	2.	12.33	1.	1.	1.	0.19
	HYDROGRAPH AT							
+		84B	21.	12.00	3.	1.	1.	0.12
	3 COMBINED AT							
+		20C	48.	12.00	12.	4.	4.	1.06
	HYDROGRAPH AT							
+		79B	4.	12.00	0.	0.	0.	0.02



+	ROUTED TO	15R	4.	12.00	0.	0.	0.	0.02
+	HYDROGRAPH AT	78B	3.	12.00	1.	0.	0.	0.08
+	2 COMBINED AT	8C	6.	12.00	1.	0.	0.	0.09
+	HYDROGRAPH AT	87B	10.	12.00	1.	0.	0.	0.06
+	2 COMBINED AT	22C	16.	12.00	3.	1.	1.	0.16
+	HYDROGRAPH AT	77B	3.	12.00	1.	0.	0.	0.06
+	3 COMBINED AT	7C	67.	12.00	16.	6.	6.	1.27
+	HYDROGRAPH AT	177B	2.	12.00	0.	0.	0.	0.02
+	HYDROGRAPH AT	248B	12.	12.00	2.	1.	1.	0.08
+	HYDROGRAPH AT	176B	6.	12.00	1.	0.	0.	0.02
+	5 COMBINED AT	41C	96.	12.00	21.	7.	7.	1.51
+	HYDROGRAPH AT	286B	119.	12.00	15.	5.	5.	0.42
+	HYDROGRAPH AT	181B	15.	12.00	2.	1.	1.	0.03
+	3 COMBINED AT	43C	230.	12.00	37.	13.	13.	1.96
+	HYDROGRAPH AT	2B	32.	12.17	6.	2.	2.	0.08
+	ROUTED TO	38R	32.	12.17	6.	2.	2.	0.08
+	HYDROGRAPH AT	405B	6.	12.00	1.	0.	0.	0.01

+	HYDROGRAPH AT	288B	8.	12.00	1.	0.	0.	0.01
+	4 COMBINED AT	44C	265.	12.00	45.	15.	15.	2.06
+	HYDROGRAPH AT	415B	49.	12.00	5.	2.	2.	0.08
+	HYDROGRAPH AT	459B	80.	12.00	12.	4.	4.	0.18
+	4 COMBINED AT	3C	489.	12.00	78.	26.	26.	2.72
+	HYDROGRAPH AT	163B	37.	12.00	4.	1.	1.	0.06
+	HYDROGRAPH AT	7B	7.	12.00	1.	0.	0.	0.04
+	HYDROGRAPH AT	411B	20.	12.00	2.	1.	1.	0.03
+	4 COMBINED AT	12C	553.	12.00	86.	29.	29.	2.86
+	ROUTED TO	12R	553.	12.00	86.	29.	29.	2.86
+	HYDROGRAPH AT	141B	26.	12.17	5.	2.	2.	0.16
+	ROUTED TO	25R	26.	12.17	5.	2.	2.	0.16
+	HYDROGRAPH AT	139B	3.	12.00	1.	0.	0.	0.07
+	ROUTED TO	23R	2.	12.17	1.	0.	0.	0.07
+	HYDROGRAPH AT	140B	9.	12.00	1.	0.	0.	0.05
+	2 COMBINED AT	24C	11.	12.00	2.	1.	1.	0.11
+	ROUTED TO							

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+		24R	8.	12.17	2.	1.	1.	0.11	
+		138B	23.	12.17	4.	1.	1.	0.12	
+		18C	57.	12.17	11.	4.	4.	0.39	
+		18R	55.	12.17	11.	4.	4.	0.39	
+		155B	25.	12.00	4.	1.	1.	0.08	
+		149B	85.	12.17	14.	5.	5.	0.20	
+		4C	106.	12.17	18.	6.	6.	0.28	
+		4R	21.	13.00	17.	14.	14.	0.28	
+									4813.64
									13.00
+		30B	38.	12.17	7.	2.	2.	0.15	
+		66B	17.	12.00	2.	1.	1.	0.05	
+		11C	117.	12.17	37.	21.	21.	0.87	
+		11R	117.	12.17	37.	21.	21.	0.87	
+		241B	25.	12.00	4.	1.	1.	0.09	
+		10R	25.	12.00	4.	1.	1.	0.09	
+		151B	4.	12.00	1.	0.	0.	0.01	
+		150B	28.	12.00	3.	1.	1.	0.05	
+		35C	33.	12.00	4.	1.	1.	0.06	

+	ROUTED TO	35R	5.	0.17	5.	5.	5.	0.06	4815.00	0.00
+										
+	HYDROGRAPH AT	143B	16.	12.00	2.	1.	1.	0.04		
+	HYDROGRAPH AT	402B	6.	12.00	1.	0.	0.	0.02		
+	2 COMBINED AT	33C	23.	12.00	3.	1.	1.	0.06		
+	ROUTED TO	33R	5.	0.17	5.	5.	5.	0.06	4810.30	12.50
+										
+	HYDROGRAPH AT	407B	7.	12.00	1.	0.	0.	0.02		
+	HYDROGRAPH AT	406B	5.	12.00	1.	0.	0.	0.03		
+	HYDROGRAPH AT	358B	2.	12.00	0.	0.	0.	0.01		
+	5 COMBINED AT	54C	24.	12.00	12.	11.	11.	0.17		
+	HYDROGRAPH AT	344B	17.	12.00	2.	1.	1.	0.04		
+	HYDROGRAPH AT	363B	8.	12.00	1.	0.	0.	0.02		
+	3 COMBINED AT	9C	50.	12.00	15.	12.	12.	0.23		
+	ROUTED TO	9R	50.	12.00	15.	12.	12.	0.23		

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

DT	PEAK	TIME TO PEAK	VOLUME	DT	PEAK	COMPUTATION INTERVAL TIME TO PEAK	VOLUME
(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)

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FOR STORM = 1 STORM AREA (SQ MI) = 10.00
 25R MANE 1.00 25.99 0.35 10.00 25.72 730.00 0.35

 CONTINUITY SUMMARY (AC-FT) - INFLOW=0.2960E+01 EXCESS=0.0000E+00 OUTFLOW=0.2957E+01 BASIN STORAGE=0.3543E-02 PERCENT ERROR= 0.0

 FOR STORM = 1 STORM AREA (SQ MI) = 10.00
 23R MANE 0.50 2.68 0.14 10.00 2.21 730.00 0.14

 CONTINUITY SUMMARY (AC-FT) - INFLOW=0.5098E+00 EXCESS=0.0000E+00 OUTFLOW=0.5084E+00 BASIN STORAGE=0.1490E-02 PERCENT ERROR= 0.0

 FOR STORM = 1 STORM AREA (SQ MI) = 10.00
 24R MANE 1.00 10.99 0.20 10.00 8.20 730.00 0.21

 CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1245E+01 EXCESS=0.0000E+00 OUTFLOW=0.1240E+01 BASIN STORAGE=0.6146E-02 PERCENT ERROR= 0.0

 FOR STORM = 1 STORM AREA (SQ MI) = 10.00
 18R MANE 1.50 56.03 0.32 10.00 54.90 730.00 0.32

 CONTINUITY SUMMARY (AC-FT) - INFLOW=0.6707E+01 EXCESS=0.0000E+00 OUTFLOW=0.6693E+01 BASIN STORAGE=0.2973E-01 PERCENT ERROR= -0.2

*** NORMAL END OF HEC-1 ***

100 YEAR HEC-1

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LEHI CITY

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*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* MAY 1991
* VERSION 4.0.1E
*
* RUN DATE TIME
*
*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
*
*****

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X X X X X XX
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XXXXXX XXXX XXXX X
X X X X X X
X X X X X X
X X XXXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

PAGE 1

HEC-1 INPUT

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

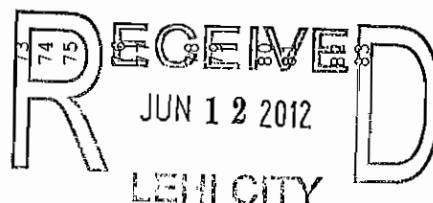
LINE	ID	1	2	3	4	5	6	7	8	9	10
1	HEC-1 Analysis using WMS										
2	ID 100 year developed flow										
3	ID MAY 2012										
4	IT 10 07MAY09	0	130								
5	IO 5										
6	IN 6 07MAY09	0									
7	JD 2.52 10.0										
8	* typeII-24hour										
9	PC 0.0 0.001	0.002	0.0031	0.0041	0.0051	0.0062	0.0073	0.0083	0.0094		
10	PC 0.0105 0.0116	0.0127	0.0138	0.015	0.0161	0.0173	0.0185	0.0196	0.0208		
11	PC 0.022 0.0232	0.0244	0.0256	0.0269	0.0281	0.0294	0.0307	0.0319	0.0332		
12	PC 0.0345 0.0358	0.0371	0.0384	0.0398	0.0411	0.0425	0.0439	0.0452	0.0466		
13	PC 0.048 0.0494	0.0508	0.0523	0.0538	0.0553	0.0568	0.0583	0.0598	0.0614		
14	PC 0.063 0.0646	0.0662	0.0679	0.0696	0.0712	0.073	0.0747	0.0764	0.0782		
15	PC 0.08 0.0818	0.0836	0.0855	0.0874	0.0892	0.0912	0.0931	0.095	0.097		
16	PC 0.099 0.101	0.103	0.1051	0.1072	0.1093	0.1114	0.1135	0.1156	0.1178		
17	PC 0.12 0.1223	0.1246	0.1271	0.1296	0.1323	0.135	0.1379	0.1408	0.1439		
18	PC 0.147 0.1502	0.1534	0.1566	0.1598	0.163	0.1663	0.1697	0.1733	0.1771		
19	PC 0.181 0.1851	0.1895	0.1941	0.1989	0.204	0.2094	0.2152	0.2214	0.228		
20	PC 0.235 0.2427	0.2513	0.2609	0.2715	0.283	0.3068	0.3544	0.4308	0.5679		
	PC 0.663 0.682	0.6986	0.713	0.7252	0.735	0.7434	0.7514	0.7588	0.7656		



ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

LINE

46	KK	37R	CNAME	37C					
47	KO	0	0	0.0	0	22			
48	RS	1	FLOW	0.0	0.0				
49	* 37C Volume								
50	SV	0.00.1266630.253327	0.379990.5066530.633316	0.759980.8866431.0133061.139969					
51	SV	1.26661.3932961.5199591.6466221.7732861.8999492.0266122.1532752.2799392.406602							
52	* 37C Elevation								
53	SE	4742.04742.4214742.8424743.2634743.6844744.1054744.5264744.9474745.3684745.789							
54	SE	4746.24746.6314747.0524747.4734747.8944748.3154748.7364749.1574749.578							
55	* 37C Discharge								
56	SQ	0.02.197453	8.3679616.4140423.1448215.9029218.6881421.1090223.2794925.26417						
57	SQ	27.10328.8264930.4517731.9946033.4663734.8761036.2310137.5370538.7991540.02147							
58	* 37C Elevation								
59	SE	4742.04742.4214742.8424743.2634743.6844744.1054744.5264744.9474745.3684745.789							
60	SE	4746.24746.6314747.0524747.4734747.8944748.3154748.7364749.1574749.578							
61	* 11B								
62	KK	11B	0	0.0	0	22			
63	BA	0.1161							
64	LS	0.0	57.0	0.0					
65	UD	0.0767							
66	* 6C								
67	KK	6R	CNAME	6C					
68	KO	0	0	0.0	0	22			
69	RN	6R							
70	* 10B								
71	KK	10B	0	0.0	0	22			
72	KO	0							
73	BA	0.1616							
74	LS	0.0	71.74	0.0					
75	UD	0.1283							
76	* 13C								
77	KK	13C	CNAME	13R					
78	KO	0	0	0.0	0	22			
79	HC	2							
80	* 13C Volume								
81	SV	0.00.9742581.9639382.969202	3.990215.0271236.0801017.1493058.2348969.337034						
82	SV	10.45511.5915912.7443313.9142715.1015516.3063517.5288218.7691220.0274121.30386							
83	* 13C Elevation								
84	SE	4800.04800.5264801.0524801.5784802.1054802.6314803.1574803.6844804.2104804.736							
85	SE	4805.24805.7894806.3154806.8424807.3684807.8944808.4214808.9474809.473							
86	* 13C Discharge								
87	SQ	0.03.42952912.3279421.8209515.9029219.3218222.2207724.7829127.1039229.24128							
88	SQ	31.23233.1045734.8761036.5618938.1733239.7194241.2075542.6437844.0331945.38008							
89	* 13C Elevation								
90	SE	4800.04800.5264801.0524801.5784802.1054802.6314803.1574803.6844804.2104804.736							
91	SE	4805.24805.7894806.3154806.8424807.3684807.8944808.4214808.9474809.473							



HEC-1 INPUT

[illegible]

LINE	ID	1	2	3	4	5	6	7	8	9	10	11
250	KK	415B										
251	KO	0	0	0.0	1	22						
252	BA	0.0771										
253	LS	0.0	80.26	0.0								
254	UD	0.0921										
255	KK	459B										
256	KO	0	0	0.0	1	22						
257	BA	0.1803										
258	LS	0.0	79.85	0.0								
259	UD	0.1662										
260	KK	3C	CNAME	3R								
261	KO	0	0	0.0	0	22						
262	HC	4										
263	KK	163B										
264	KO	0	0	0.0	1	22						
265	BA	0.0618										
266	LS	0.0	80.62	0.0								
267	UD	0.1138										
268	KK	7B										
269	KO	0	0	0.0	1	22						
270	BA	0.0408										
271	LS	0.0	67.23	0.0								
272	UD	0.0556										
273	KK	411B										
274	KO	0	0	0.0	1	22						
275	BA	0.0331										
276	LS	0.0	79.74	0.0								
277	UD	0.0892										
278	KK	12C	CNAME	12R								
279	KO	0	0	0.0	0	22						
280	HC	4										
281	KK	12R	CNAME	12C								
282	KO	0	0	0.0	0	22						
283	RN	12R										
284	KK	141B										
285	KO	0	0	0.0	1	22						
286	BA	0.1600										
287	LS	0.0	69.57	0.0								
288	UD	0.1866										
289	KK	25R	CNAME	25C								
290	KO	0	0	0.0	0	22						
291	RD	1297.6	0.07153	0.013		CIRC	2.0					0.0

HEC-1 INPUT

ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

LINE

292	KK	139B	0	0.0	0	22			
293	BA	0.0660							
294	LS	0.0	61.27	0.0					
295	UD	0.0702							
296									
297	KK	23R	CNAME	23C					
298	KO	0	0	0.0	0	22			
299	RD	1357.8	0.04276	0.013		CIRC	2.0	0.0	
300	KK	140B							
301	KO	0	0	0.0	0	22			
302	BA	0.0475							
303	LS	0.0	67.54	0.0					
304	UD	0.0616							
305	KK	24C	CNAME	24R					
306	KO	0	0	0.0	0	22			
307	HC	2							
308	KK	24R	CNAME	24C					
309	KO	0	0	0.0	0	22			
310	RD	3765.7	0.06856	0.013		CIRC	2.0	0.0	
311	KK	138B							
312	KO	0	0	0.0	0	22			
313	BA	0.1174							
314	LS	0.0	71.23	0.0					
315	UD	0.2069							
316	KK	18C	CNAME	18R					
317	KO	0	0	0.0	0	22			
318	HC	3							
319	KK	18R	CNAME	18C					
320	KO	0	0	0.0	0	22			
321	RD	3528.0	0.04879	0.013		TRAP	2.0	0.0	
322	KK	155B							
323	KO	0	0	0.0	0	22			
324	BA	0.0758							
325	LS	0.0	75.21	0.0					
326	UD	0.1458							
327	KK	149B							
328	KO	0	0	0.0	0	22			
329	BA	0.2020							
330	LS	0.0	80.17	0.0					
331	UD	0.2477							



LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
332	KK 4C CNAME 4R 0 0 22
333	KO 0
334	HC 2
335	KK 4R CNAME 4C
336	KO 0 0 0 22
337	RS 1 FLOW 0.0 0.0
	* 4C Volume
338	SV 0.00.2728530.5501420.8319091.118195 1.409041.7044872.0045762.3093492.618846
339	SV 2.93313.2521783.5760963.9049024.2386384.5773464.921066 5.269845.6237085.982713
	* 4C Elevation
340	SE 4811.04811.2104811.4214811.6314811.8424812.0524812.2634812.4734812.6844812.894
341	SE 4813.14813.3154813.5264813.7364813.9474814.1574814.3684814.5784814.789 4815.0
	* 4C Discharge
342	SQ 12.76313.3469013.9061714.4438114.9621415.4631015.9483316.4192316.8770017.32267
343	SQ 17.75718.1812818.7378822.8393729.3622537.5566847.1173257.86315 69.670582.44792
	* 4C Elevation
344	SE 4811.04811.2104811.4214811.6314811.8424812.0524812.2634812.4734812.6844812.894
345	SE 4813.14813.3154813.5264813.7364813.9474814.1574814.3684814.5784814.789 4815.0
346	KK 30B
347	KO 0 0 0 22
348	BA 0.1491
349	LS 0 0 74.12 0.0
350	UD 0.2306
351	KK 66B
352	KO 0 0 0 22
353	BA 0.0522
354	LS 0 0 72.0 0.0
355	UD 0.0556
356	KK 11C CNAME 11R
357	KO 0 0 0 22
358	HC 4
359	KK 11R CNAME 11C
360	KO 0 0 0 22
361	RN 11R
362	KK 241B
363	KO 0 0 0 22
364	BA 0.0949
365	LS 0 0 73.24 0.0
366	UD 0.1459
367	KK 10R CNAME 10C
368	KO 0 0 0 22
369	RN 10R

HEC-1 INPUT

ID.....	1.....	2.....	3.....	4.....	5.....	6.....	7.....	8.....	9.....	10.....
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LINE

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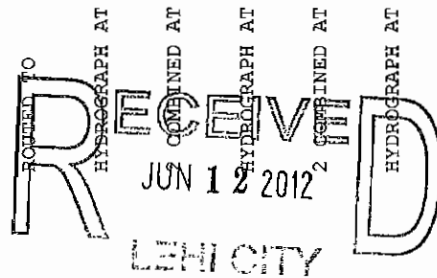
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HEC-1 INPUT

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
409	SE 4810.0 4811.0 4812.0 4813.0 4814.0 4815.0 4816.0 4817.0 4818.0 4819.0
410	KK 407B
411	KO 0
412	BA 0.0182
413	LS 0.0 74.0 0.0
414	UD 0.0532
415	KK 406B
416	KO 0
417	BA 0.0256
418	LS 0.0 68.46 0.0
419	UD 0.0717
420	KK 358B
421	KO 0
422	BA 0.0053
423	LS 0.0 72.0 0.0
424	UD 0.0822
425	KK 54C CNAME 54R
426	KO 0 0.0
427	HC 5
428	KK 344B
429	KO 0
430	BA 0.0449
431	LS 0.0 73.99 0.0
432	UD 0.0895
433	KK 363B
434	KO 0
435	BA 0.0208
436	LS 0.0 75.76 0.0
437	UD 0.1262
438	KK 9C CNAME 9R
439	KO 0 0.0
440	HC 3
441	KK 9R CNAME 9C
442	KO 0 0.0
443	RN 9R
444	ZZ

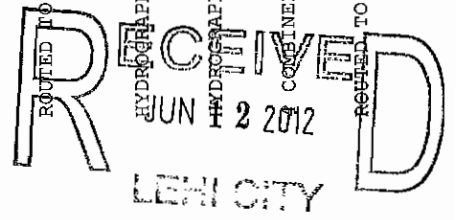
RECEIVED
JUN 12 2012
LEHI CITY

+	32C	128.	12.00	19.	6.	6.	0.40
	HYDROGRAPH AT						
+	101B	14.	12.17	3.	1.	1.	0.11
	ROUTED TO						
+	31R	14.	12.17	3.	1.	1.	0.11
	HYDROGRAPH AT						
+	83B	17.	12.00	7.	2.	2.	0.57
	ROUTED TO						
+	19R	17.	12.00	7.	2.	2.	0.57
	HYDROGRAPH AT						
+	86B	13.	12.00	1.	0.	0.	0.03
	2 COMBINED AT						
+	21C	29.	12.00	8.	3.	3.	0.59
	HYDROGRAPH AT						
+	85B	23.	12.00	4.	1.	1.	0.16
	2 COMBINED AT						
+	16C	52.	12.00	12.	4.	4.	0.75
	HYDROGRAPH AT						
+	81B	5.	12.00	2.	1.	1.	0.19
	ROUTED TO						
+	17R	5.	12.00	2.	1.	1.	0.19
	HYDROGRAPH AT						
+	84B	30.	12.00	4.	1.	1.	0.12
	3 COMBINED AT						
+	20C	88.	12.00	18.	6.	6.	1.06
	HYDROGRAPH AT						
+	79B	5.	12.00	1.	0.	0.	0.02
	ROUTED TO						
+	15R	5.	12.00	1.	0.	0.	0.02
	HYDROGRAPH AT						
+	78B	6.	12.00	1.	0.	0.	0.08
	2 COMBINED AT						
+	8C	11.	12.00	2.	1.	1.	0.09
	HYDROGRAPH AT						
+	87B	15.	12.00	2.	1.	1.	0.06
	2 COMBINED AT						
+	22C	26.	12.00	4.	1.	1.	0.16
	HYDROGRAPH AT						
+	77B	6.	12.00	1.	0.	0.	0.06



+	3 COMBINED AT	7C	120.	12.00	23.	8.	8.	1.27
+	HYDROGRAPH AT	177B	4.	12.00	1.	0.	0.	0.02
+	HYDROGRAPH AT	248B	18.	12.00	2.	1.	1.	0.08
+	HYDROGRAPH AT	176B	8.	12.00	1.	0.	0.	0.02
+	5 COMBINED AT	41C	163.	12.00	30.	10.	10.	1.51
+	HYDROGRAPH AT	286B	160.	12.00	19.	6.	6.	0.42
+	HYDROGRAPH AT	181B	19.	12.00	2.	1.	1.	0.03
+	3 COMBINED AT	43C	341.	12.00	51.	17.	17.	1.96
+	HYDROGRAPH AT	2B	39.	12.17	7.	2.	2.	0.08
+	ROUTED TO	38R	39.	12.17	7.	2.	2.	0.08
+	HYDROGRAPH AT	405B	7.	12.00	1.	0.	0.	0.01
+	HYDROGRAPH AT	288B	10.	12.00	1.	0.	0.	0.01
+	4 COMBINED AT	44C	384.	12.00	60.	20.	20.	2.06
+	HYDROGRAPH AT	415B	59.	12.00	7.	2.	2.	0.08
+	HYDROGRAPH AT	459B	98.	12.00	15.	5.	5.	0.18
+	4 COMBINED AT	3C	668.	12.00	100.	33.	33.	2.72
+	HYDROGRAPH AT	163B	44.	12.00	5.	2.	2.	0.06
+	HYDROGRAPH AT	7B	10.	12.00	1.	0.	0.	0.04
+	HYDROGRAPH AT	411B	25.	12.00	3.	1.	1.	0.03
+	4 COMBINED AT	12C	747.	12.00	110.	36.	36.	2.86

+	ROUTED TO	12R	747.	12.00	110.	36.	36.	2.86
+	HYDROGRAPH AT	141B	36.	12.17	6.	2.	2.	0.16
+	ROUTED TO	25R	35.	12.17	6.	2.	2.	0.16
+	HYDROGRAPH AT	139B	6.	12.00	1.	0.	0.	0.07
+	ROUTED TO	23R	5.	12.00	1.	0.	0.	0.07
+	HYDROGRAPH AT	140B	13.	12.00	2.	1.	1.	0.05
+	2 COMBINED AT	24C	18.	12.00	3.	1.	1.	0.11
+	ROUTED TO	24R	13.	12.00	3.	1.	1.	0.11
+	HYDROGRAPH AT	138B	31.	12.17	5.	2.	2.	0.12
+	3 COMBINED AT	18C	79.	12.17	15.	5.	5.	0.39
+	ROUTED TO	18R	77.	12.17	15.	5.	5.	0.39
+	HYDROGRAPH AT	155B	32.	12.00	5.	2.	2.	0.08
+	HYDROGRAPH AT	149B	103.	12.17	17.	5.	5.	0.20
+	2 COMBINED AT	4C	129.	12.17	22.	7.	7.	0.28
+	ROUTED TO	4R	35.	12.67	20.	15.	15.	0.28
+	HYDROGRAPH AT	30B	49.	12.17	9.	3.	3.	0.15
+	HYDROGRAPH AT	66B	22.	12.00	3.	1.	1.	0.05
+	COMBINED AT	11C	154.	12.17	45.	23.	23.	0.87
+	ROUTED TO	11R	154.	12.17	45.	23.	23.	0.87
								4814.08
								12.67

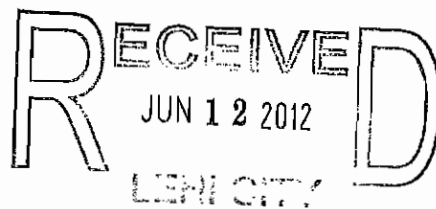


	HYDROGRAPH AT	241B	33.	12.00	5.	2.	2.	0.09	
+									
+	ROUTED TO	10R	33.	12.00	5.	2.	2.	0.09	
+	HYDROGRAPH AT	151B	6.	12.00	1.	0.	0.	0.01	
+	HYDROGRAPH AT	150B	34.	12.00	4.	1.	1.	0.05	
+	2 COMBINED AT	35C	40.	12.00	4.	1.	1.	0.06	
+	ROUTED TO	35R	5.	0.17	5.	5.	5.	0.06	4815.00
+									0.00
+	HYDROGRAPH AT	143B	21.	12.00	2.	1.	1.	0.04	
+	HYDROGRAPH AT	402B	8.	12.00	1.	0.	0.	0.02	
+	2 COMBINED AT	33C	29.	12.00	3.	1.	1.	0.06	
+	ROUTED TO	33R	5.	0.17	5.	5.	5.	0.06	4810.49
+									12.50
+	HYDROGRAPH AT	407B	9.	12.00	1.	0.	0.	0.02	
+	HYDROGRAPH AT	406B	8.	12.00	1.	0.	0.	0.03	
+	HYDROGRAPH AT	358B	2.	12.00	0.	0.	0.	0.01	
+	5 COMBINED AT	54C	29.	12.00	12.	11.	11.	0.17	
+	HYDROGRAPH AT	344B	22.	12.00	3.	1.	1.	0.04	
+	HYDROGRAPH AT	363B	10.	12.00	1.	0.	0.	0.02	
+	3 COMBINED AT	9C	61.	12.00	16.	12.	12.	0.23	
+	ROUTED TO	9R	61.	12.00	16.	12.	12.	0.23	
1									

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)
INTERPOLATED TO

ISTAQ	ELEMENT	DT	PEAK	TIME TO PEAK	VOLUME	DT	COMPUTATION PEAK	INTERVAL TIME TO PEAK	VOLUME
		(MIN)	(CFS)	(MIN)	(IN)	(MIN)	(CFS)	(MIN)	(IN)
FOR STORM = 1 STORM AREA (SQ MI) = 10.00									
25R	MANE	0.94	35.56	730.30	0.45	10.00	35.38	730.00	0.45
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.3804E+01 EXCESS=0.0000E+00 OUTFLOW=0.3801E+01 BASIN STORAGE=0.4098E-02 PERCENT ERROR= 0.0									
FOR STORM = 1 STORM AREA (SQ MI) = 10.00									
23R	MANE	0.50	5.82	722.00	0.21	10.00	4.93	720.00	0.21
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.7282E+00 EXCESS=0.0000E+00 OUTFLOW=0.7265E+00 BASIN STORAGE=0.1807E-02 PERCENT ERROR= 0.0									
FOR STORM = 1 STORM AREA (SQ MI) = 10.00									
24R	MANE	1.00	17.38	723.00	0.28	10.00	12.90	720.00	0.28
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.1692E+01 EXCESS=0.0000E+00 OUTFLOW=0.1686E+01 BASIN STORAGE=0.7309E-02 PERCENT ERROR= 0.0									
FOR STORM = 1 STORM AREA (SQ MI) = 10.00									
18R	MANE	1.54	77.93	731.22	0.41	10.00	76.86	730.00	0.42
CONTINUITY SUMMARY (AC-FT) - INFLOW=0.8656E+01 EXCESS=0.0000E+00 OUTFLOW=0.8640E+01 BASIN STORAGE=0.3327E-01 PERCENT ERROR= -0.2									

*** NORMAL END OF HEC-1 ***



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